

Upshot of Chemical Species and Nonlinear Thermal Radiation on Oldroyd-B Nanofluid Flow Past a Bi-directional Stretched Surface with Heat Generation/Absorption in a Porous Media*

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Abstract A three-dimensional mathematical model is developed to examine the flow of nonlinear thermal radiation Oldroyd-B nanofluid past a bidirectional linearly stretched surface in a porous medium. The flow is induced by temperature dependent thermal conductivity, chemical reaction and convective heat and mass conditions. Novel characteristics of Brownian motion and thermophoresis are accompanied by magnetohydrodynamic and heat generation/absorption. Self-similar transformations are employed to convert the system of nonlinear partial differential equations to a system of ordinary differential equations with high nonlinearity and are solved by strong analytic technique named as Homotopy Analysis method (HAM). Effects of varied arising parameters on involved distributions are reflected through graphical illustrations. From this study, it is perceived that strong magnetic field hinders the fluid's motion and leads to rise in temperature that eventually lowers heat transfer rate from the surface. Further, decrease in heat transfer rate is also observed for enhanced values of thermal radiation parameter. To validate our results, a comparison with already published paper in limiting case is also given and results are found in excellent concurrence; hence reliable results are being presented.

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Key words: nonlinear thermal radiation, heat generation/absorption, chemical reaction, convective heat and mass conditions, porous media

Nomenclature

B_0	Magnetic field	Rd	Radiation parameter
c, d	Constants	Re	Reynolds number
C	Concentration of fluid	Sh_x	Sherwood number
C_w	Concentration at wall	T	Temperature of fluid
C_∞	Ambient concentration	T_w	Temperature at wall
C_p	Specific heat	T_∞	Ambient temperature
D_B	Brownian diffusion coefficient	(u, v, w)	Velocity components
D_T	Thermophoretic diffusion coefficient	(x, y, w)	Coordinate axes
f, g	Dimensionless velocities	β_1	Thermal Deborah number
h_1	Convective heat transfer coefficient	β_2	Solutal Deborah number
h_2	Convective mass transfer coefficient	δ	Chemical reaction parameter
k	Variable thermal conductivity	δ_1	Relaxation Biot number
k^*	Coefficient of mean absorption	δ_2	Retardation Biot number
k_p	Permeability parameter	λ	Ratio of stretching rate
k_r	Chemical reaction rate	λ_1	Relaxation time
k_∞	Fluid free stream conductivity	λ_2	Retardation time
k_w	Thermal conductivity at wall	ν	Kinematic viscosity
Le	Lewis number	ρ	Density of fluid
M	Hartmann number	σ	Electric conductivity

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Nb	Brownian motion parameter	θ	Dimensionless temperature
Nt	Thermophoresis parameter	ϕ	Dimensionless concentration
Pm	Permeability parameter	ϵ	Thermal conductivity parameter
Q	Heat generation/absorption parameter	μ	Dynamic viscosity
q_r	Radiative heat flux	τ	Heat capacity ratio
Q^*	Heat generation/absorption coefficient	σ^*	Stefan-Boltzmann constant
Nu_x	Nusselt number	η	Dimensionless variable
Pr	Prandtl number	θ_w	Temperature ratio

1 Introduction

Heat and mass transfer is the most studied subject in today's research because of its abundant efficacy in science and industry. The processes of reheating and freezing have vast usage in industry. In manufacturing processes, it is necessary to keep heat transfer phenomenon live in manufacturing of final refined product. Due to such interesting applications, scientists and researchers are captivated to reassess the potential of heat transfer. Choi and Eastman^[1] were the pioneer who introduced the concept of great nanofluids to meet requirements of the industry. Geothermal industry, floor heating, polymer industry and processes like lubrication, manufacturing, chemical are some applications of nanofluids. A nanofluid is an amalgamation of nano sized metallic particles (like Cu, T₁O₂, Ag, etc.) and base fluid (like water, kerosene, ethylene glycol, oils). Usually, thermal conductivity of nanoparticle is more than the base liquid. However, mixture of both has obviously enhanced thermal conductivity. The pioneering work of Choi and Eastman was followed a study by Wang and Mujumdar^[2] who tried to improve the convective characteristics of base fluid by insertion of metallic and nonmetallic nanoparticles. Then Eastman *et al.*^[3] examined that mixture of ethylene glycol and suspended copper nanoparticles augments the thermal conductivity of the base fluid by 40%. In continuation to previous study,^[3] Eastman *et al.*^[4] explored another important result that thermal conductivity of nanofluid is also affected by the nanoparticle's shape and size. This concept was supported by an experiment by Murshed *et al.*^[5] who investigated that an amalgamation of spherical shaped nanoparticles (with size more than 40 nm) and Titanium oxide (base fluid) produces 33% more thermal conductivity than that of ordinary base fluid. In very a recent exploration, Pryazhnikov *et al.*^[6] studied that thermal conductivity of nanofluid is also affected by nanoparticle's material and density. Sandeep and Reddy^[7] discussed the heat transfer phenomenon of Cu-water nanofluid past two varied geometries accompanied by nonlinear radiation effects. Zaib *et al.*^[8] discussed the flow of Carreau nanofluid with effects of nonlinear thermal radiation, activation energy and binary chemical reaction past a nonlinear stretched surface. Nayak *et al.*^[9] reported numerical treatment of

three-dimensional nanofluid free convective flow with thermal radiation and magnetohydro dynamic with shooting technique. Kasaeian *et al.*^[10] described heat transfer of nanofluids flow in a porous medium. Some more studies highlighting different aspects of nanofluids may be found at Refs. [11–20] and many therein.

Characteristics of viscoelasticity is key to many complex natured fluids like polymer melts, colloidal suspensions and polymer solutions. Applications like blow molding, inkjet printing and extrusion involve such fluids. Viscoelastic characteristics like energy dissipation, hydraulic resistance, transport efficiency etc. affect many flows.^[21] Pioneering work of Maxwell^[22] featured a rate type mathematical model to assess viscoelasticity in fluids. While doing so, he overlooked the incompressibility feature of the fluid. This gap is fulfilled by Oldroyd's model^[23] that portrays a factual depiction of nonlinear fluids. Amongst the proposed mathematical models by Oldroyd, Oldroyd-B model was much praised and admired model that interpret the both relaxation and retardation times' characteristics. This fluid model reduces to Maxwell fluid model in absence of retardation time term. Later, Lai^[24] analyzed the stability of Oldroyd-B fluid down an inclined plane. This effort was followed by Thien^[25] who discussed numerical and analytical solutions of Oldroyd-B fluid flow around a coaxial disk. Thien also highlighted stagnation point Oldroyd-B fluid flow^[26] and instability of cone and plate.^[27] Then Tan^[28] extended Stokes's first problem to Oldroyd-B fluid flow with semi permeable surface using sine transform to find exact solution. Exploring a new dimension, Fetecau *et al.*^[29] found exact solutions of oscillating flows of Oldroyd-B fluid in oscillating circular cylinders. Pioneering work in three dimensional geometry was explored by Hayat *et al.*^[30] who examined similar solution of three dimensional Oldroyd-B fluid flow past a bidirectional stretched surface. Boundary layer flow of an Oldroyd-B fluid over the continuously linearly stretching sheet is studied by Hayat *et al.*^[31] They have examined the effects of mixed convection and stagnation point flow of thermally stratified fluid by using the homotopy analysis method. Waqar *et al.*^[32] addressed analytically about the bidirectional flow of an Oldroyd-B nanofluid with heat generation/absorption over the stretching sheet.

They concluded that local Nusselt number decreases for the higher values of heat generation parameter. Later on Hayat *et al.*^[33] investigated about the electrically conducting Oldroyd-B nanofluid flow over the multidimensional stretching sheet with the zero nanoparticle mass flux condition employed on the boundary. They also applied normal magnetic field and found that velocity reduces for the higher magnetic strength. Zhang *et al.*^[34] analyzed analytically the unsteady thin film flow of an Oldroyd-B nanofluid for the heat transfer over the stretching sheet. Poly vinyl alcohol-water is used as a base fluid with Ag and Cu as nanoparticles. Besides this, a good number of recent explorations highlighting various aspects involving three dimensional flows of Oldroyd-B fluid may be found in the literature.^[35–38] However, after the invent of nanofluids, researchers started to explore new fronts with the amalgamation of Oldroyd-B fluid and nanofluids. First step in this direction was taken by Nadeem *et al.*^[39] who studied flow of Oldroyd-B nanofluid flow past a linearly stretched surface numerically. Moving a step further, three dimensional nanofluid Oldroyd-B fluid past a stretched surface was deliberated by Khan *et al.*^[39] Then Hayat *et al.*^[40] studied three dimensional Oldroyd-B nanofluid with effects of magneto hydrodynamic and zero mass flux condition. Shehzad *et al.*^[41] first time studied combination of linear thermal radiation with three dimensional Oldroyd-B nanofluid flow and magneto hydrodynamic. Last attempt in this regard is recently done by Hayat *et al.*^[42] who found analytical solution of three-dimensional Oldroyd-B nanofluid flow with heat generation/absorption.

From the above literature survey, it is revealed that the problem of three-dimensional Oldroyd-B magneto nanofluid flow with impact of nonlinear thermal radiation and chemical reaction in a porous media is still a scarce. Additional effects of heat generation/absorption, temperature dependent thermal conductivity and convective heat and mass conditions are added features to the uniqueness

of the present effort. No attempt so far has been made to solve such an important mathematical model. We being the pioneer have solved this problem using renowned Homotopy Analysis method.^[43–48] Graphical illustrations are given to portray the impact of varied parameters versus velocity profile, heat and mass transfer rates. To authenticate our results, a comparison with previous study in limiting case is also given.

2 Mathematical Formulation

Consider the flow of three-dimensional Oldroyd-B nanofluid past a bidirectional stretched surface in the presence of nonlinear thermal radiation in a porous media. Flow analysis is performed in attendance of thermophoresis and Brownian motion. Additional effects of heat generation, chemical reaction and variable thermal conductivity are also taken into account. Fluid flow occupies the region $z > 0$, however, stretched surface coincides with the plane $z = 0$. Fluid is made electrically conducting in the presence of uniform magnetic field of strength B_0 . Here, induced magnetic field is ignored due to our assumption of small Reynolds number. The velocity components $u = cx$ and $v = dy$ (with c and d are constants) are along x and y -directions. Also, T_w is the constant surface temperature and T_∞ is the ambient temperature with $T_w > T_\infty$ (see Fig. 1). The pertinent boundary layer equations are^[33,49]

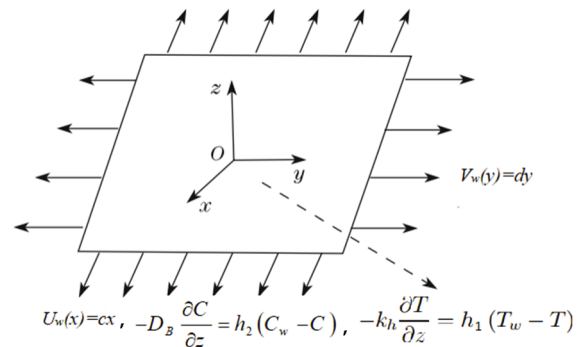


Fig. 1 Geometry of the flow problem.

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0, \quad (1)$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} + \lambda_1 \left(u^2 \frac{\partial^2 u}{\partial x^2} + v^2 \frac{\partial^2 u}{\partial y^2} + w^2 \frac{\partial^2 u}{\partial z^2} + 2uv \frac{\partial^2 u}{\partial x \partial y} + 2vw \frac{\partial^2 u}{\partial y \partial z} + 2uw \frac{\partial^2 u}{\partial x \partial z} \right) = \nu \left[\frac{\partial^2 u}{\partial z^2} + \lambda_2 \left(u \frac{\partial^3 u}{\partial x \partial z^2} + v \frac{\partial^3 u}{\partial y \partial z^2} + w \frac{\partial^3 u}{\partial z^3} - \frac{\partial u}{\partial x} \frac{\partial^2 u}{\partial z^2} - \frac{\partial u}{\partial y} \frac{\partial^2 v}{\partial z^2} - \frac{\partial u}{\partial z} \frac{\partial^2 w}{\partial z^2} \right) \right] - \frac{\sigma B_0^2}{\rho} \left(u + \lambda_1 w \frac{\partial u}{\partial z} \right) - \frac{\nu}{k_p} u, \quad (2)$$

$$u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} + \lambda_1 \left(u^2 \frac{\partial^2 v}{\partial x^2} + v^2 \frac{\partial^2 v}{\partial y^2} + w^2 \frac{\partial^2 v}{\partial z^2} + 2uv \frac{\partial^2 v}{\partial x \partial y} + 2vw \frac{\partial^2 v}{\partial y \partial z} + 2uw \frac{\partial^2 v}{\partial x \partial z} \right) = \nu \left[\frac{\partial^2 v}{\partial z^2} + \lambda_2 \left(u \frac{\partial^3 v}{\partial x \partial z^2} + v \frac{\partial^3 v}{\partial y \partial z^2} + w \frac{\partial^3 v}{\partial z^3} - \frac{\partial v}{\partial x} \frac{\partial^2 u}{\partial z^2} - \frac{\partial v}{\partial y} \frac{\partial^2 v}{\partial z^2} - \frac{\partial v}{\partial z} \frac{\partial^2 w}{\partial z^2} \right) \right] - \frac{\sigma B_0^2}{\rho} \left(v + \lambda_1 w \frac{\partial v}{\partial z} \right) - \frac{\nu}{k_p} v, \quad (3)$$

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z} = \frac{1}{\rho C_p} \frac{\partial}{\partial z} \left(k \frac{\partial T}{\partial z} \right) + \tau \left[D_B \frac{\partial T}{\partial z} \frac{\partial C}{\partial z} + \frac{D_T}{T_\infty} \left(\frac{\partial T}{\partial z} \right)^2 \right] - \frac{1}{\rho C_p} \frac{\partial q_r}{\partial z} + \frac{Q^*}{\rho C_p} (T - T_\infty), \quad (4)$$

$$u \frac{\partial C}{\partial x} + v \frac{\partial C}{\partial y} + w \frac{\partial C}{\partial z} = D_B \frac{\partial^2 C}{\partial z^2} + \frac{D_T}{T_\infty} \frac{\partial^2 T}{\partial z^2} - k_r (C - C_\infty), \quad (5)$$

with (u, v, w) are the velocities along (x, y, z) directions respectively.

In view of Rosseland's approximation, the value of heat flux is given by

$$q_r = -\frac{4\sigma^*}{3k^*} \frac{\partial T^4}{\partial z} = -\frac{16\sigma^*}{3k^*} T^3 \frac{\partial T}{\partial z}. \quad (6)$$

The model equations (1)–(5) are supported by the boundary conditions

$$\begin{aligned} u = cx, \quad v = dy, \quad w = 0, \quad -k_h \frac{\partial T}{\partial z} &= h_1(T_w - T), \\ -D_B \frac{\partial C}{\partial z} &= h_2(C_w - C), \quad \text{at } z = 0, \\ u \rightarrow 0, \quad v \rightarrow 0, \quad T \rightarrow T_\infty, \quad C \rightarrow C_\infty &\text{ as } z \rightarrow \infty. \end{aligned} \quad (7)$$

Taking into account the succeeding transformations

$$\begin{aligned} u = U_w(x) = cx f'(\eta), \quad v = V_w(y) = cy g'(\eta), \\ w = -\sqrt{c\nu}(f(\eta) + g(\eta)), \quad \theta(\eta) = \frac{T - T_\infty}{T_w - T_\infty}, \\ \eta = \sqrt{\frac{c}{\nu}} z, \quad \theta(\eta) = \frac{C - C_\infty}{C_w - C_\infty}. \end{aligned} \quad (8)$$

Here, η is similarity variable. The variable thermal conductivity^[50] is given by $k = k_\infty(1 + \epsilon\theta(\eta))$, where $\epsilon = (k_w - k_\infty)/k_\infty$ with k_∞ and k_w are the fluid free stream conductivity and the thermal conductivity at wall respectively. Also, using the relation $T = T_\infty((\theta_w - 1)\theta(\eta) + 1)$, $\theta_w = T_w/T_\infty$ with above transformations, requirement of Eq. (1) is fulfilled inevitably, however, Eqs. (2)–(5) and Eq. (7) take the form

$$f'''' + (M^2\beta_1 + 1)(f + g)f'' - f'^2 - (M^2 + Pm)f' + \beta_1(2(f + g)f'f'' - (f + g)^2f''') + \beta_2((f'' + g'')f'' - (f + g)f''''') = 0, \quad (9)$$

$$g'''' + (M^2\beta_1 + 1)(f + g)g'' - g'^2 - (M^2 + Pm)g' + \beta_1(2(f + g)g'g'' - (f + g)^2g''') + \beta_2((f'' + g'')g'' - (f + g)g''''') = 0, \quad (10)$$

$$(1 + \epsilon\theta)\theta'' + \epsilon\theta'^2 + Pr(f + g)\theta' + PrNb\left(\theta'\phi' + \frac{Nt}{Nb}\theta'^2\right) + \frac{4}{3}Rd((\theta_w - 1)\theta + 1)^3\theta'' + 4Rd((\theta_w - 1)\theta + 1)^2\theta'^2 + PrQ\theta = 0, \quad (11)$$

$$\phi'' + PrLe(f + g)\phi' + \frac{Nt}{Nb}\theta'' - PrLe\delta\phi = 0, \quad (12)$$

$$f(0) = 0, \quad f'(0) = 1, \quad g(0) = 0, \quad g'(0) = \lambda, \quad \theta'(0) = -\delta_1(1 - \theta(0)), \quad \phi'(0) = -\delta_2(1 - \phi(0)), \quad (13)$$

$$f'(\infty) \rightarrow 0, \quad f''(\infty) \rightarrow 0, \quad g'(\infty) \rightarrow 0, \quad g''(\infty) \rightarrow 0, \quad \phi(\infty) \rightarrow 0, \quad \theta(\infty) \rightarrow 0. \quad (14)$$

The values of above mentioned non-dimensionalized parameters are given below:

$$\begin{aligned} Pr = \frac{\mu C_p}{k}, \quad M = \frac{\sigma B_0^2}{\rho c}, \quad \delta_1 = \frac{h_1}{k} \sqrt{\frac{\nu}{c}}, \quad \delta_2 = \frac{h_2}{D_B} \sqrt{\frac{\nu}{c}}, \quad \beta_1 = \lambda_1 c, \quad Rd = \frac{4\sigma^* T_\infty^3}{kk^*}, \quad \delta = \frac{k_r}{c}, \\ \beta_2 = \lambda_2 c, \quad Ec = \frac{c^2 x^2}{(T_w - T_\infty)C_p}, \quad \lambda = \frac{d}{c}, \quad Nb = \frac{\tau D_B (C_f - C_\infty)}{\nu}, \quad Pm = \frac{\mu}{k_p c}, \quad Q = \frac{Q^* \nu}{\rho C_p}, \\ Le = \frac{\alpha}{D_B}, \quad \lambda = \frac{d}{c}, \quad Nb = \frac{\tau D_B (C_f - C_\infty)}{\nu}, \quad Nt = \frac{\tau D_T (T_f - T_\infty)}{T_\infty \nu}, \quad L = \frac{y}{x}. \end{aligned} \quad (15)$$

The heat and mass transfer rates i.e., local Nusselt and Sherwood numbers in dimensional form are given by

$$Nu_z = \frac{xq_w}{k(T_w - T_\infty)}, \quad Sh_z = \frac{xj_w}{D_B(T_w - T_\infty)}, \quad (16)$$

where

$$q_w = -k \left(\frac{\partial T}{\partial z} \right) + q_r \Big|_{z=0}, \quad q_w = -D_B \left(\frac{\partial C}{\partial z} \right) \Big|_{z=0}. \quad (17)$$

Dimensionless form of these numbers are

$$\begin{aligned} Nu_z Re_z^{-1/2} &= -\left(1 + \frac{4}{3}Rd((\theta_w - 1)\theta(0) + 1)^3\right)\theta'(0), \\ Sh_z Re_z^{-1/2} &= -\phi'(0). \end{aligned} \quad (18)$$

3 Homotopic Solutions

The initial guesses $(f_0, g_0, \theta_0, \phi_0)$ and linear operators $(\mathcal{L}_f, \mathcal{L}_g, \mathcal{L}_\theta, \mathcal{L}_\phi)$ required for Homotopy Analysis method

are defined as:

$$\begin{aligned} f_0(\eta) = (1 - \exp(-\eta)), \quad g_0(\eta) = \lambda(1 - \exp(-\eta)), \\ \theta_0(\eta) = \frac{\delta_1 \exp(-\eta)}{1 + \delta_1}, \quad \phi_0(\eta) = \frac{\delta_2 \exp(-\eta)}{1 + \delta_2}, \end{aligned} \quad (19)$$

$$\begin{aligned} \mathcal{L}_f(\eta) = \frac{d^3 f}{d\eta^3} - \frac{df}{d\eta}, \quad \mathcal{L}_g(\eta) = \frac{d^3 g}{d\eta^3} - \frac{dg}{d\eta}, \\ \mathcal{L}_\theta(\eta) = \frac{d^2 \theta}{d\eta^2} - \theta, \quad \mathcal{L}_\phi(\eta) = \frac{d^2 \phi}{d\eta^2} - \phi, \end{aligned} \quad (20)$$

with the following properties

$$\begin{aligned} \mathcal{L}_f[C_1 + C_2 \exp(\eta) + C_3 \exp(-\eta)] &= 0, \\ \mathcal{L}_g[C_4 + C_5 \exp(\eta) + C_6 \exp(-\eta)] &= 0, \\ \mathcal{L}_\theta[C_7 \exp(\eta) + C_8 \exp(-\eta)] &= 0, \\ \mathcal{L}_\phi[C_9 \exp(\eta) + C_{10} \exp(-\eta)] &= 0, \end{aligned} \quad (21)$$

where C_i ($i = 1-10$), the arbitrary constants, through the

boundary conditions have the values

$$\begin{aligned}
 C_2 = C_5 = C_7 = C_9 = 0, \quad C_3 &= \left. \frac{\partial f_m^*(\eta)}{\partial \eta} \right|_{\eta=0}, \\
 C_1 = -C_3 - f_m^*(0), \quad C_6 &= \left. \frac{\partial g_m^*(\eta)}{\partial \eta} \right|_{\eta=0}, \\
 C_4 = -C_6 - g_m^*(0), \quad C_8 &= \frac{1}{1 + \delta_1} \left(\left. \frac{\partial \theta_m^*(\eta)}{\partial \eta} \right|_{\eta=0} - \delta \theta_m^*(0) \right), \\
 C_{10} = \frac{1}{1 + \delta_2} \left(\left. \frac{\partial \phi_m^*(\eta)}{\partial \eta} \right|_{\eta=0} - \delta_2 \phi_m^*(0) \right). \quad (22)
 \end{aligned}$$

3.1 Convergence Analysis

To determine the region of convergence for series solutions, the importance of auxiliary parameters ($\hbar_f, \hbar_g, \hbar_\theta, \hbar_\phi$) can not be denied. Figure 2 is illustrated to identify the same regions. Tolerable ranges of parameters \hbar_f ,

\hbar_g, \hbar_θ , and \hbar_ϕ are $-1.7 \leq \hbar_f \leq -0.7, -1.6 \leq \hbar_g \leq -0.4, -1.4 \leq \hbar_\theta \leq -0.5$, and $-1.4 \leq \hbar_\phi \leq -0.5$ respectively. The values of these parameters are in complete alignment to those numerical values found in Table 1.

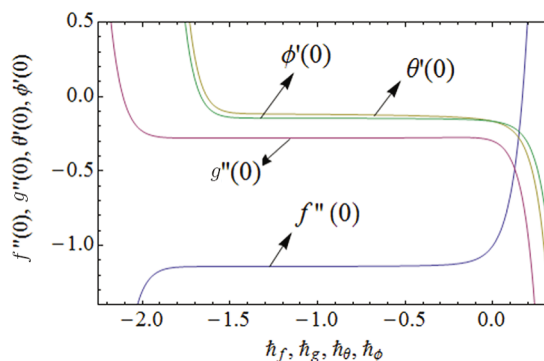


Fig. 2 \hbar -curve of f, g, θ , and ϕ .

Table 1 Convergence of series solutions for different order of approximations when $\beta_1 = 0.2, \beta_2 = 0.2, M = 0.4, \epsilon = 0.3, \lambda = 0.3, Nt = 0.2, Nb = 0.7, Rd = 0.4, \theta_w = 1.3, Le = 0.7, Pr = 0.7, \delta_1 = 0.4, \delta_2 = 0.6, \delta = 0.2, Pm = 0.1, Q = 0.1$.

Order of approximations	$-f''(0)$	$-g''(0)$	$-\theta'(0)$	$-\phi'(0)$
1	1.099 07	0.271 76	0.149 92	0.157 14
5	1.134 71	0.276 55	0.133 18	0.149 90
10	1.139 61	0.278 62	0.125 29	0.147 39
15	1.140 98	0.279 35	0.120 97	0.146 28
20	1.141 59	0.279 69	0.118 08	0.145 64
25	1.141 91	0.279 88	0.115 96	0.145 22
30	1.142 12	0.279 99	0.114 30	0.144 93
35	1.142 14	0.280 03	0.114 00	0.144 83
40	1.142 14	0.280 03	0.113 93	0.144 82

4 Results and Discussion

This section is outlined to examine the impact of varied involved parameters on all distributions via several graphs that arise in the mathematical model. Figures 3 and 4 are drawn to show the influence of relaxation and retardation times i.e., β_1 and β_2 on velocity fields $f'(\eta)$ and $g'(\eta)$ respectively. It is witnessed that $f'(\eta)$ and $g'(\eta)$ are decreasing and increasing functions of β_1 and β_2 respectively. This is due to the fact that higher values of β_1 boosts the viscous force that hinders the movement of fluid's motion and eventually decays in velocity profile is seen. An opposite trend in case of β_2 is seen where growth in velocity field is observed for large values of β_2 . Here, strength of viscous force is weakened because of higher values of β_2 and eventually an enhanced velocity distribution is perceived. Figures 5 and 6 epitomize the impact of Biot numbers δ_1 and δ_2 on temperature and concentration fields respectively. Both δ_1 and δ_2 have direct proportion to their respective heat and mass transfer coefficients. Augmented values of δ_1 and δ_2 are because of more heat and mass transfer resistance inside the body in comparison to the surface that results in enhanced temperature and concentration distributions. Figure 7 elucidates the impact of temperature dependent thermal conductivity parameter ϵ on temperature distribution. It is noticed that increasing values of ϵ amplify the temperature field. As we know that higher temperature is because of increased values of thermal conductivity. In Fig. 8, effect of heat generation/absorption parameter Q on temperature distribution is displayed. It is perceived that mounting values of Q lead to increase in the temperature profile. Higher values of Q means more heat is transferred to the fluid that ultimately results in higher temperature and sturdier boundary layer thickness. Figures 9 and 10 are portrayed to depict the effect of stretching ratio parameter λ on both velocities $f'(\eta)$ and $g'(\eta)$ respectively. It is seen

that higher value of λ is in direct and indirect relation to stretched rates along y - and x -directions respectively. So, velocity field $g'(\eta)$ along y -direction increases and velocity field $f'(\eta)$ along x -direction decreases.

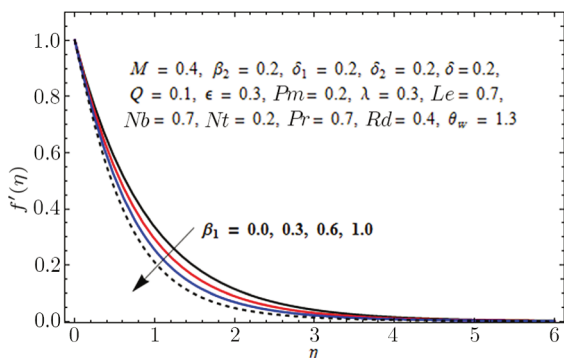


Fig. 3 Graph of β_1 versus $f'(\eta)$.

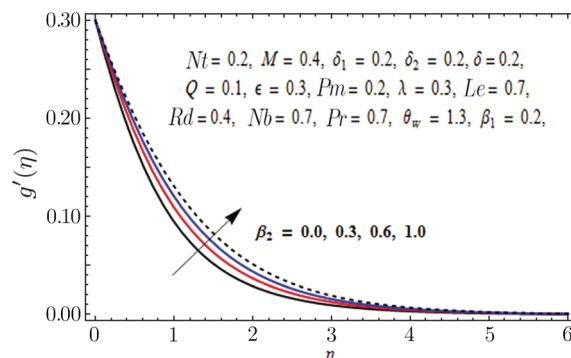


Fig. 4 Graph of β_2 versus $g'(\eta)$.

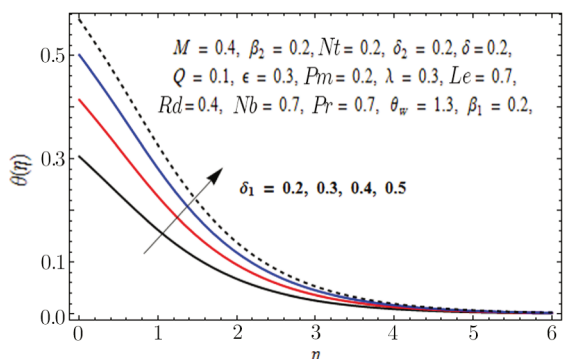


Fig. 5 Graph of δ_1 versus $\theta(\eta)$.

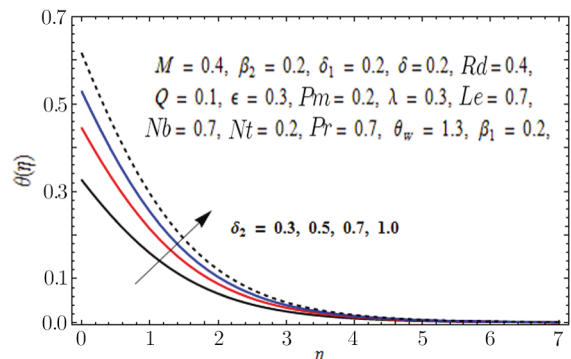


Fig. 6 Graph of δ_2 versus $\phi(\eta)$.

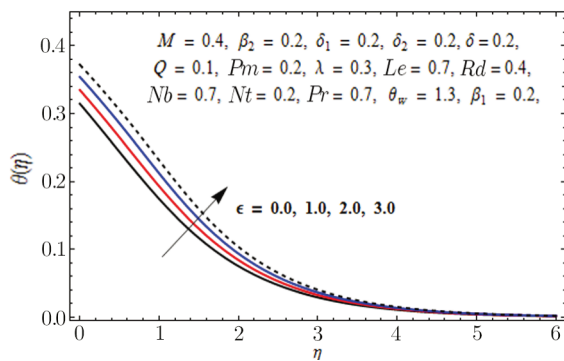


Fig. 7 Graph of ϵ versus $\theta(\eta)$.

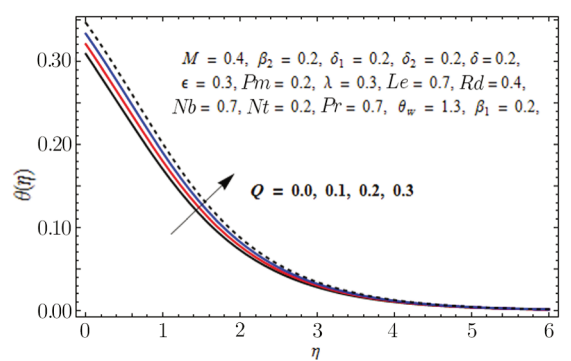


Fig. 8 Graph of Q versus $\theta(\eta)$.

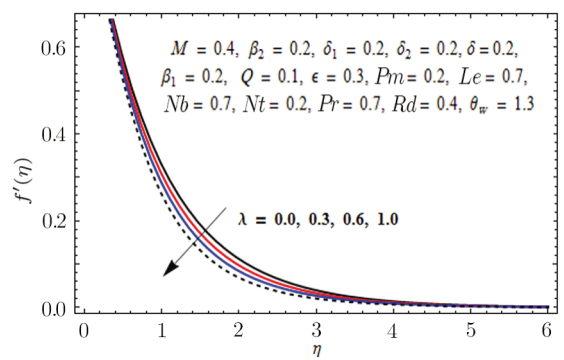


Fig. 9 Graph of λ versus $f'(\eta)$.

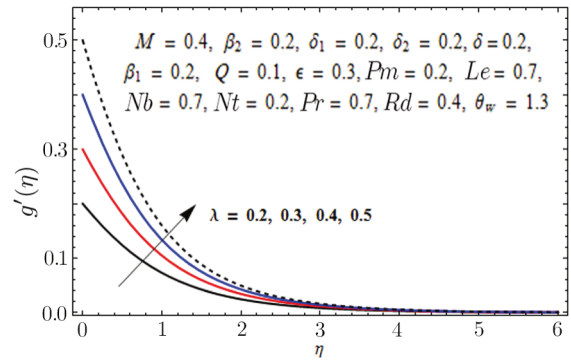


Fig. 10 Graph of λ versus $g'(\eta)$.

In Fig. 11, impact of radiation parameter Rd on temperature distribution is presented. It is examined that temperature field is mounted function of Rd . It is due to the fact that enhancement in thermal radiation parameter results in diminution in mean absorption coefficient that eventually boosts the divergence of the radiative heat flux and increase in fluid's temperature is witnessed. Figure 12 is drawn to show the impact of Lewis number Le on concentration

distribution. As we know that Lewis number is the quotient of thermal diffusivity to mass diffusivity. Increase in Le means high thermal diffusivity which is responsible for decrement in concentration distribution. Figures 13 and 14 are illustrated to depict the influence of Hartmann number M on velocities in both x - and y -directions respectively. It is seen that both velocities decrease with increase in values of M . This is because of the resistance offered by the Lorentz force. Hence, decrease in both velocities is experimented. Figure 15 is portrayed to depict the effect of temperature ratio parameter θ_w on temperature field. Augmented values of θ_w enhance the fluid's thermal state, which is accountable for increased temperature. In Fig. 16, effect of Brownian motion parameter Nb on temperature profile is portrayed. It is examined that temperature field is increasing function of Nb . Actually, rise in values of means Nb more collision of particles and eventually rise in temperature field is witnessed. Figure 17 is drawn to illustrate the impact of thermophoresis parameter Nt on concentration profile. Decrease in concentration profile is seen for increasing values of Nt . Nanoparticles are attracted towards the cold surface with increase in values of Nt that lowers the nanoparticle concentration. To check the influence of Prandtl number Pr on temperature and concentration distributions, Figs. 18 and 19 are graphed.

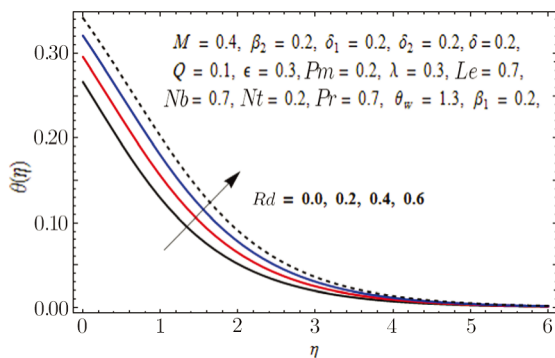


Fig. 11 Graph of Rd versus $\theta(\eta)$.

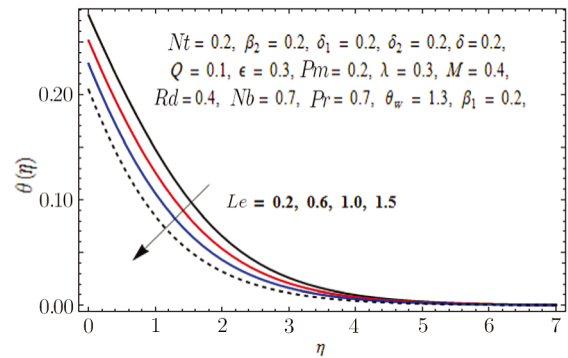


Fig. 12 Graph of Le versus $\phi(\eta)$.

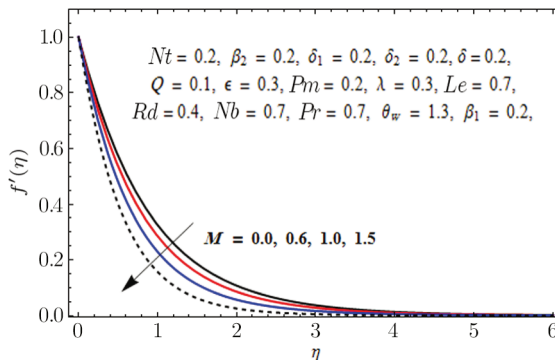


Fig. 13 Graph of M versus $f'(\eta)$.

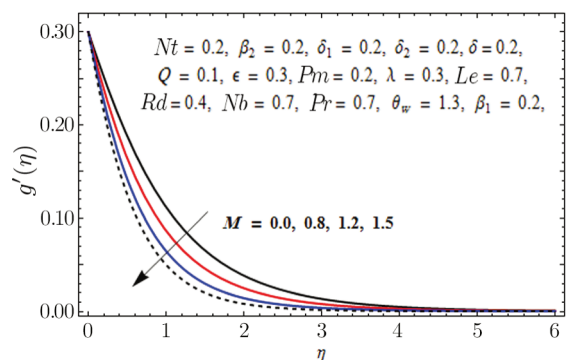


Fig. 14 Graph of M versus $g'(\eta)$.

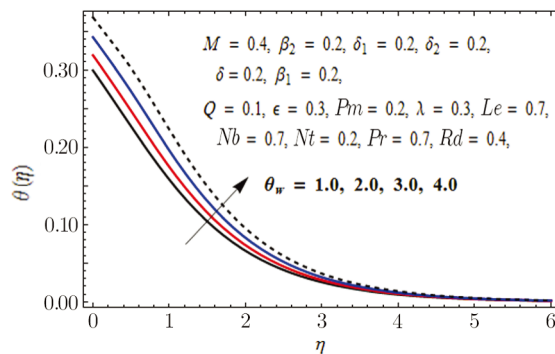


Fig. 15 Graph of θ_w versus $\theta(\eta)$.

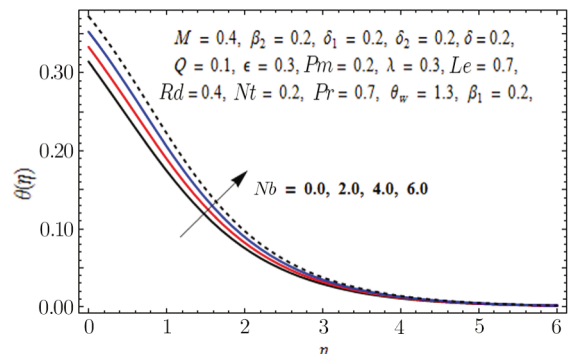


Fig. 16 Graph of Nb versus $\theta(\eta)$.

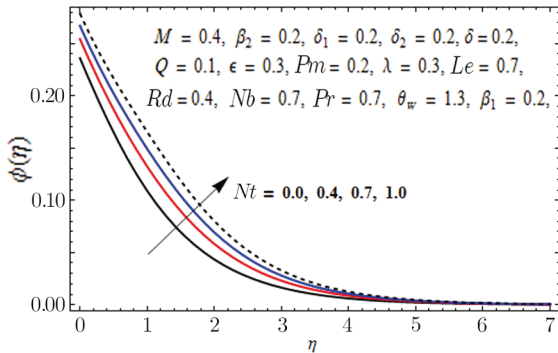


Fig. 17 Graph of Nt versus $\phi(\eta)$.

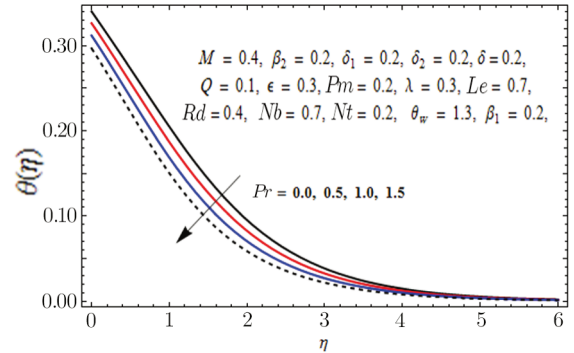


Fig. 18 Graph of Pr versus $\theta(\eta)$.

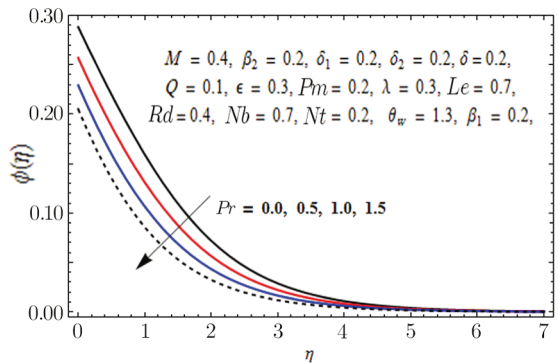


Fig. 19 Graph of Pr versus $\phi(\eta)$.

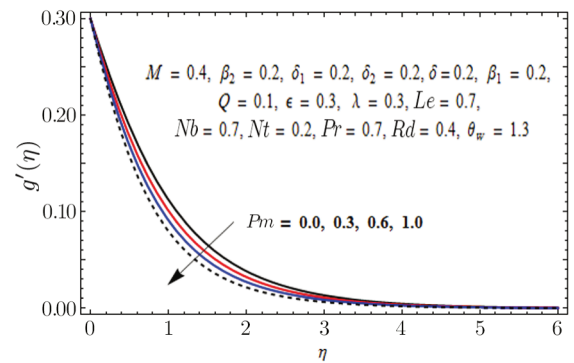


Fig. 20 Graph of Pm versus $g'(\eta)$.

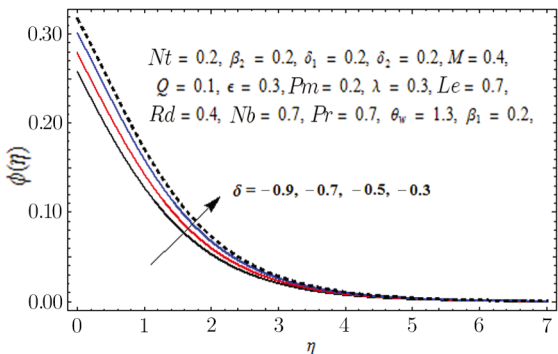


Fig. 21 Graph of $\delta < 0$ versus $\phi(\eta)$.

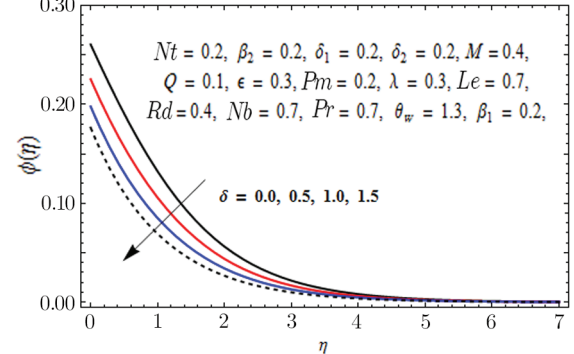


Fig. 22 Graph of $\delta > 0$ versus $\phi(\eta)$.

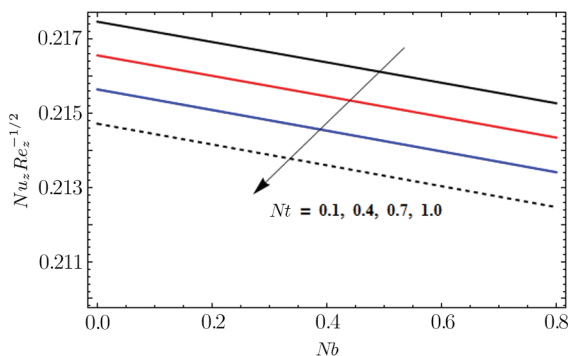


Fig. 23 Influence of Nb and Nt on $Nu_z Re_z^{-1/2}$.

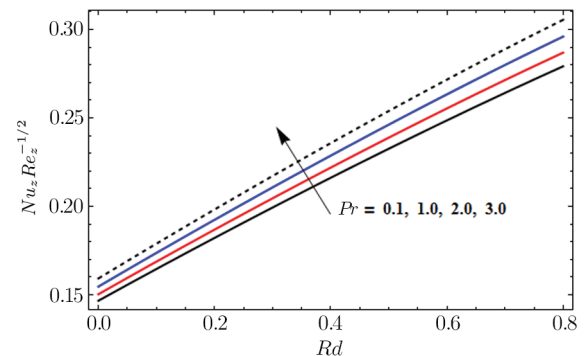


Fig. 24 Influence of Pr and Rd on $Nu_z Re_z^{-1/2}$.

It is experimented that Prandtl number is the proportion of momentum diffusivity to thermal diffusivity. Higher values of momentum diffusivity correspond to feeble thermal diffusivity in case of Prandtl number and we encounter weaker boundary layer thicknesses in case of both temperature and concentration profiles. Figure 20 is drawn to exhibit the effects of permeability parameter Pm on velocity profile along y -axis. It is seen that porous medium offers resistance to the fluid flow and as a result velocity of the fluid is decreased. Effect of chemical reaction parameter in both cases generative ($\delta < 0$) and destructive ($\delta > 0$) on concentration profile is presented in Figs. 21 and 22

respectively. Opposite behavior in both cases is witnessed. Disruption in chemical reaction for generative case ($\delta < 0$) does not create much disorder. However, in case of destructive ($\delta > 0$), disruption is higher due to comparatively substantial molecular motion.

Table 2 Values of local Nusselt number $-\theta'(0)$ in comparison to Hayat *et al.*^[50] for different values of parameters β_1 , β_2 , Pr and γ in absence of nanofluid, nonlinear thermal radiation, variable thermal conductivity, porous medium, chemical reaction, convective mass condition.

β_1	β_2	Pr	γ	$-\theta'(0)$			
				Ref. [50]		Present	
				$\lambda = 0.0$	$\lambda = 0.5$	$\lambda = 0.0$	$\lambda = 0.5$
0.0	0.4	1.0	0.8	0.347 59	0.396 58	0.347 59	0.396 58
0.5	0.4	1.0	0.8	0.336 51	0.382 28	0.336 51	0.382 28
1.0	0.4	1.0	0.8	0.326 36	0.369 97	0.326 36	0.369 97
0.4	0.0	1.0	0.8	0.326 13	0.367 61	0.326 13	0.367 61
0.4	0.5	1.0	0.8	0.340 94	0.387 93	0.340 94	0.387 93
0.4	1.0	1.0	0.8	0.349 63	0.395 52	0.349 63	0.395 52
0.4	0.4	0.5	0.8	0.248 39	0.292 21	0.248 39	0.292 21
0.4	0.4	0.8	0.8	0.309 16	0.355 06	0.309 16	0.355 06
0.4	0.4	1.3	0.8	0.373 00	0.419 32	0.373 00	0.419 32
0.4	0.4	1.0	0.3	0.198 56	0.213 65	0.198 56	0.213 65
0.4	0.4	1.0	0.6	0.296 77	0.331 87	0.296 77	0.331 87
0.4	0.4	1.0	1.0	0.369 93	0.426 14	0.369 93	0.426 14

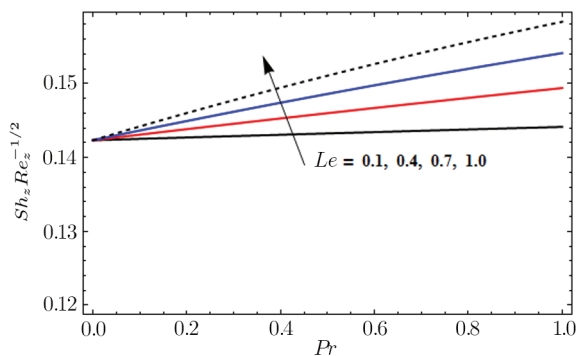


Fig. 25 Influence of Pr and Le on $Sh_z Re_z^{-1/2}$.

Figures 23 and 24 show that Nusselt number increase and decrease for gradual increasing values of Pr , Rd and Nt , Nb respectively. In Fig. 25, we see that Sherwood number increase and decrease for Le and Pr respectively.

Table 2 depicts an excellent agreement of numerically calculated local Nusselt number in limiting case (in absence of nanofluid, nonlinear thermal radiation, variable thermal conductivity, porous medium, chemical reaction, convective mass condition) to those values obtained Hayat *et al.*^[50]

5 Conclusions

In this communication three-dimensional Oldroyd-B

fluid flow in attendance of variable thermal conductivity and nonlinear thermal radiation is studied. Additional effects of chemical reaction, porous medium and magneto hydrodynamics are also taken into account. Flow analysis is performed in the presence Brownian motion and thermophoresis with convective heat and mass conditions. The salient characteristics of this investigation are appended below:

- Increasing values of radiation parameter boosts the temperature of fluid.
- Convective heat and mass transfer support the temperature and concentration profiles respectively.
- Higher values of variable thermal conductivity augments the fluid's temperature.
- Sherwood number increases with higher values of Prandtl and Lewis numbers.
- Velocities along x - and y -axes decrease with increase in values of Hartmann number.
- Temperature is increased with higher values of Brownian motion.
- Opposite behavior in case of generative and destructive chemical reaction on concentration field is witnessed.
- Decrease in velocity of fluid flow is observed for increasing values of permeability parameter.

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