

**HEAT TRANSFER ANALYSIS OF  
JOHNSON-SEGALMAN FLUID IN A TAPERED  
ASYMMETRIC CHANNEL**



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## **Dedication**

Dedicated to my Beloved Parents and Respected Supervisor

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All praises to **Almighty Allah**, the creator of all the creatures in the universe, who has created us in the structure of human beings as the best creature. Many thanks to Him, who created us as a muslim and blessed us with knowledge to differentiate between right and wrong. Many many thanks to Him as he blessed us with the Holy Prophet, **Hazrat Muhammad (Sallallahu Alaihay Wa'alihi wasalam)** for Whom the whole universe is created. He (Sallallahu Alaihay Wa'alihi wasalam) brought us out of darkness and enlightened the way to heaven.

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## **Abstract**

This study presents a theoretical thermal analysis for the peristaltic transportation of electrically conducting Johnson-Segalman liquid through a two-dimensional asymmetric tapered following the propagation of sinusoidal wave trains with dissimilar phases. The impact of viscous dissipation is also deliberated in the modeling. Mathematical modeling is carried out by making use of lubrication approximation theory. The fundamental equations of the Johnson Segalman fluid are solved by regular perturbation technique and the expressions for velocity, energy and stream functions are attained. The impact of various embedded parameters on the flow fields is illustrated graphically and discussed in detail. The significant outcomes of the current analysis are that the liquid velocity declined with the higher values of magnetic parameter and enhances with Johnson-Segalman liquid parameter. Pressure rise improves in the augmented pumping portion with the magnetic parameter.

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## LIST OF SYMBOLS

$d$	channel half-width
$k'$	non-uniform parameter
$c$	wave speed
$\widehat{u}, \widehat{v}$	laboratory frame velocity components
$t$	Time
$T_0, T_1$	temperature at upper and lower wall
$a_1, a_2$	amplitude of wave at upper and lower wall
$u, v$	wave frame velocity components
$x, y$	space coordinates in wave frame
$p$	Pressure
$m$	Relaxation time
$\mu, \eta$	dynamic viscosities
$\lambda$	Wavelength
$B_0$	strength of magnetic field
$B_r$	Brinkman number
$e$	slip parameter
Pr	Prandtl number
$\Delta p$	pressure rise
$\widehat{Q}$	time average of the flux
$M$	magnetic number
$c_p$	specific heat
$Ec$	Eckert Number
Re	Reynold's number
$\sigma^*$	Stefan - Boltzmann constant

$\widehat{D}, \widehat{W}$	symmetric and skew-symmetric
$\psi$	dimensionless stream function
$\tau$	Cauchy stress tensor
$\delta$	Wavenumber
$\rho$	fluid density
$\xi$	thermal conductivity constant
$q_r$	radiative heat flux
$\beta$	velocity slip parameter
$We$	Weissenberg number
$k^*$	mean absorption coefficient
$\phi$	Phase difference
$\sigma$	Electrical Conductivity

#### **Abbreviations**

JS	Johnson-Segalman
PT	Peristaltic transport
NF	Newtonian fluid
NNF	Non-Newtonian fluid
PDE	Partial differential equation
ODE	Ordinary differentials equation

# CHAPTER 1

## INTRODUCTION

### 1.1 Overview

This chapter is intended to provide basic fluid mechanics ideas as well as definitions of numerous dimensionless numbers and equations in order to explain the flow analysis presented in this study.

### 1.2 Fluid

When a shearing stress is applied to a fluid, the individual particles, no matter how small, deform constantly.

### 1.3 Fluid Rheology

The term "rheology" refers to the study of fluid movements and deformation in response to stress. Shear stress has a very small impact on fluids that flow incompressible. Real fluid is defined as a fluid with at least some viscosity. The truth is that every fluid found or existing in the environment is classified as a real fluid. For instance, water. Real fluid can be further divided into the following categories:

#### 1.3.1 Newtonian fluids (NF)

The relation between strain and stress rate is linear in an NF. NF are those that follow Newton's law of viscosity. According to this rule, shear stress is directly but inversely related to deformation rate.

Mathematically,

$$\tau \propto \frac{\partial u}{\partial y},$$
$$\tau = \mu \frac{\partial u}{\partial y}, \quad (1.1)$$

where  $\mu$  is the dynamic viscosity of the liquid, which is constant for NF at a given temperature and pressure. Examples of NF are air and water.

**1.3.2 Non-Newtonian fluid (NNF)**

Any liquid in which relation between shear stress and the rate of deformation is direct but not linearly proportional to the rate of deformation is referred to as NNF.

Mathematically,

$$\tau = k \left( \frac{\partial u}{\partial y} \right)^n, \tag{1.2}$$

where  $n$  signifies the flow actions index and  $k$  indicates the consistency index.

**1.4 Peristaltic flow**

Peristalsis is a series of wave-like muscular cramps that migrate to the food separate processing station in the digestive tracks. The Peristalsis process begins in the esophagus when a bolus meal is consumed.

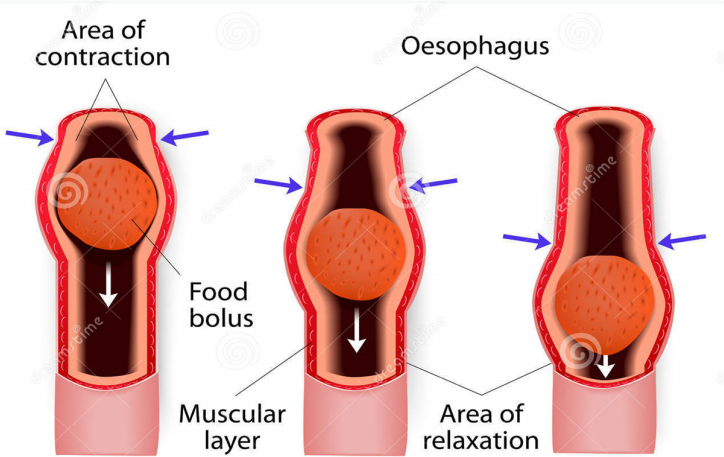


Figure 1. 1: Peristalsis mechanism

**1.4.1 Flowing Regions**

Peristaltic movement is discretized interested in four kinds of movement areas or quadrants known as unfavorable pressure if pressure increase ( $\Delta P > 0$ ) and favorable

pressure gradient if pressure rise ( $\Delta P < 0$ ). These zones are defined by the pressure variation with the time mean flow rate.

**i. Peristaltic pumping**

The stream rate is positive in this case ( $Q > 0$ ), However, the increase in pressure is unfavorable ( $\Delta p > 0$ ).

**ii. Retrograde pumping**

The stream rate is inefficient. ( $Q < 0$ ), and the pressure rise is adverse ( $\Delta p > 0$ ).

**iii. Co-pumping**

Co-pumping depicts a movement in which the time mean flow is negative with ( $\Delta P < 0$ )

**iv. Enhanced pumping**

The stream rate is positive ( $Q < 0$ ) in this scenario, yet the pressure rise is neither unfavorable nor beneficial. In other terms  $\Delta p = 0$ .

### **1.4.2 Trapping phenomenon**

A fundamental physical fact of peristalsis is trapping. It is based on the streamline's contours. A bolus of fluid may occasionally be contained in closed streamlines, creating a circulating area, instead of flowing in the direction of the peristaltic wall. The trapped bolus illustrates the peristalsis flow trapping phenomenon by moving with the wave in the flow.

### **1.5 Dimensionless numbers**

This segment is intended to provide an explanation and definition of some of the basic parameters involved in fluid flow



**i. Reynolds number**

It is a non-dimensional quantity that can be used in fluid dynamics to predict fluid flow regimes in a range of flow patterns. In fluid mechanics, it can be used for a variety of purposes. It is denoted by the letter  $Re$ , and written as

$$Re = \frac{\rho c d}{\mu}, \quad (1.3)$$

where  $\rho, c, d$  and  $\mu$  are density, width, and dynamic viscosity respectively.

**ii. Wave number**

The wavelength to channel width ratio is known as the wave number. The Greek letter  $\delta$  is used to represent it.

$$\delta = \frac{d}{\lambda}, \quad (1.4)$$

where  $d$  and  $\lambda$  are width of channel and wavelength

**iii. Weissenberg Number**

In viscoelastic flow analysis,  $We$  is a dimensionless number.

$$We = \frac{m c}{d}, \quad (1.5)$$

where  $m$  is relaxation time parameter.

**iv. Brinkmann Number**

It is a dimensionless number used in polymer manufacturing to represent heat transmission from a wall to a moving viscous fluid. It expresses the proportion of heat generated by viscous fluids to heat generated by external sources. The greater the value, the less heat is transmitted by viscous dissipation, causing temperature to rise. This is calculated as follows:

$$Br = Pr Ec, \quad (1.6)$$

**v. Eckert Number**

In continuum mechanics, Eckert number is a dimensionless number which shows the relation amid temperature and kinetic energy to demonstrate viscous dissipation

$$Ec = \frac{c^2}{C_p \Delta T}, \quad (1.7)$$

where  $C_p$  and  $\Delta T$  are specific heat and change in temperature.

#### vi. Hartmann Number

An electrically conducting fluid experiences the Lorentz force under the effects of applied magnetic field. The study of these fluids is known as magnetohydrodynamics (MHD). The Lorentz force, which is a repulsive force, slows the velocity field. It is represented as a body force in the momentum equation. The Hartmann number is a non-dimensional quantity obtained by dividing the Lorentz force by the viscous force. The Hartmann number can so be written as

$$M = \sqrt{\frac{\sigma}{\mu}} B_0 d, \quad (1.8)$$

where  $\sigma$  is electrical conductivity parameter

#### vii. Prandtl Number

It is the momentum-to-thermal-diffusivity ratio, it is dimensionless number which can be written as mathematically

$$\text{Pr} = \frac{\mu C_p}{\xi}, \quad (1.9)$$

where  $\xi$  is thermal conductivity constant.

#### viii. Radiation Parameter

The relation among thermal radiation and conduction heat transfer is defined by the radiation parameter.

$$Rd = \frac{16T_0^3 \sigma^*}{3k^* \xi}, \quad (1.10)$$

where  $\sigma^*$ ,  $T_0$  and  $k^*$  represent the Stefan - Boltzmann constant, energy at upper wall, and mean absorption coefficient respectively.

## 1.6 Governing equations

The study of fluid behavior based on some important fluid mechanics laws. These laws are as follows [18]:

### i. Continuity Equation

The mass conservation law is quantitatively stated in the continuity equation. It is as follows for compressible flows.

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{V}) = 0, \quad (1.11)$$

where  $t$  denotes time. The density of incompressible flows remains constant, hence the continuity equation becomes

$$\nabla \cdot \mathbf{V} = 0, \quad (1.12)$$

### ii. Momentum Equation

For magnetohydrodynamic flow, the appropriate equation of motion that illustrates the law of conservation of momentum is as follows:

$$\frac{d\mathbf{V}}{dt} = \frac{1}{\rho} \operatorname{div} \boldsymbol{\tau} + \frac{1}{\rho} \mathbf{f}, \quad (1.13)$$

The Cauchy stress tensor is denoted by  $\boldsymbol{\tau} = \widehat{\mathbf{S}} - \widehat{\mathbf{p}}\widehat{\mathbf{I}} + 2\mu\widehat{\mathbf{D}}$ , in the above expression. Where  $d/dt$ ,  $\widehat{\mathbf{p}}$ ,  $\widehat{\mathbf{I}}$ ,  $\widehat{\mathbf{S}}$ ,  $\widehat{\mathbf{D}}$ , and  $\mathbf{V}$  are material derivative, pressure, identity, extra stress tensors, Symmetric part of velocity gradient, and velocity vector respectively. The term  $\mathbf{f}$  represents the body force. It reflects the Lorentz force that develops because of a change in magnetic field in the current thesis.

So,

$$\mathbf{f} = \mathbf{J} \times \mathbf{B}, \quad (1.14)$$

In which  $\mathbf{B} = \mathbf{B}_0$  represent applied magnetic field.

### iii. Energy Equation

The first law of thermodynamics is where the energy equation is obtained, and it applies the energy conservation law.

$$\frac{dT}{dt} = \frac{1}{\rho C_p} \boldsymbol{\tau} \cdot \widehat{\mathbf{L}} + \frac{\xi}{\rho C_p} \nabla^2 T - \frac{1}{\rho C_p} \nabla \cdot \mathbf{q}_r, \quad (1.15)$$

where  $T, \widehat{\mathbf{L}}$  and  $\mathbf{q}_r$  are temperature velocity gradient and thermal radiation respectively.

## 1.7 Tensor equation of Johnson-Segalman (JS) fluid

The following expression describes the Cauchy stress tensor  $\boldsymbol{\tau}$  for the JS fluid model.

$$\boldsymbol{\tau} = \widehat{\mathbf{S}} - \widehat{p}\mathbf{I} + 2\mu\widehat{\mathbf{D}}, \quad (1.16)$$

In which extra stress tensor  $\widehat{\mathbf{S}}$  satisfies.

$$\widehat{\mathbf{S}} + m \left[ \frac{d\widehat{\mathbf{S}}}{dt'} + \widehat{\mathbf{S}}(\widehat{\mathbf{W}} - e\widehat{\mathbf{D}})^T + (\widehat{\mathbf{W}} - e\widehat{\mathbf{D}})\widehat{\mathbf{S}} \right] = 2\eta\widehat{\mathbf{D}}, \quad (1.17)$$

$$\widehat{\mathbf{D}} = \frac{1}{2}[\widehat{\mathbf{L}} + \widehat{\mathbf{L}}^T], \quad \widehat{\mathbf{W}} = \frac{1}{2}[\widehat{\mathbf{L}} - \widehat{\mathbf{L}}^T], \quad \widehat{\mathbf{L}} = \text{grad}\mathbf{V}, \quad (1.18)$$

Notice that the current model diminishes to the fluid model given by Maxwell for  $e=1$  and we attain the basic NS model for  $\mu = 0$ .

The velocity for 2-D unsteady flow is specified as:

$$\mathbf{V} = [\widehat{U}(\widehat{X}, \widehat{X}, t'), \widehat{V}(\widehat{X}, \widehat{Y}, t'), 0], \quad (1.19)$$

The aforementioned equation allows one to write down

$$\widehat{\mathbf{L}} = \text{grad}\mathbf{V} = \begin{bmatrix} \frac{\partial \widehat{U}}{\partial \widehat{X}} & \frac{\partial \widehat{U}}{\partial \widehat{Y}} & 0 \\ \frac{\partial \widehat{V}}{\partial \widehat{X}} & \frac{\partial \widehat{V}}{\partial \widehat{Y}} & 0 \\ 0 & 0 & 0 \end{bmatrix}, \quad \widehat{\mathbf{L}}^T = (\text{grad}\mathbf{V})^T = \begin{bmatrix} \frac{\partial \widehat{U}}{\partial \widehat{X}} & \frac{\partial \widehat{V}}{\partial \widehat{X}} & 0 \\ \frac{\partial \widehat{U}}{\partial \widehat{Y}} & \frac{\partial \widehat{V}}{\partial \widehat{Y}} & 0 \\ 0 & 0 & 0 \end{bmatrix}, \quad (1.20)$$

$$\begin{aligned}
\widehat{\mathbf{D}} &= \frac{1}{2}[\widehat{\mathbf{L}} + \widehat{\mathbf{L}}^r] = \frac{1}{2} \begin{bmatrix} 2\frac{\partial \widehat{U}}{\partial X} & \frac{\partial \widehat{U}}{\partial Y} + \frac{\partial \widehat{V}}{\partial X} & 0 \\ \frac{\partial \widehat{V}}{\partial X} + \frac{\partial \widehat{U}}{\partial Y} & 2\frac{\partial \widehat{V}}{\partial Y} & 0 \\ 0 & 0 & 0 \end{bmatrix} \\
&= \begin{bmatrix} \frac{\partial \widehat{U}}{\partial X} & \left[ \frac{1}{2}\frac{\partial \widehat{U}}{\partial Y} + \frac{1}{2}\frac{\partial \widehat{V}}{\partial X} \right] & 0 \\ \left[ \frac{1}{2}\frac{\partial \widehat{V}}{\partial X} + \frac{1}{2}\frac{\partial \widehat{U}}{\partial Y} \right] & \frac{\partial \widehat{V}}{\partial Y} & 0 \\ 0 & 0 & 0 \end{bmatrix},
\end{aligned} \tag{1.21}$$

$$\begin{aligned}
\widehat{\mathbf{W}} &= \frac{1}{2}[\widehat{\mathbf{L}} - \widehat{\mathbf{L}}^r] = \frac{1}{2} \begin{bmatrix} 0 & \frac{\partial \widehat{U}}{\partial Y} - \frac{\partial \widehat{V}}{\partial X} & 0 \\ \frac{\partial \widehat{V}}{\partial X} - \frac{\partial \widehat{U}}{\partial Y} & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \\
&= \begin{bmatrix} 0 & \left[ \frac{1}{2}\frac{\partial \widehat{U}}{\partial Y} - \frac{1}{2}\frac{\partial \widehat{V}}{\partial X} \right] & 0 \\ \left[ \frac{1}{2}\frac{\partial \widehat{V}}{\partial X} - \frac{1}{2}\frac{\partial \widehat{U}}{\partial Y} \right] & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix},
\end{aligned} \tag{1.22}$$

Using Eqs. (1.20) - (1.22) in Eq. (1.17)

$$\begin{aligned}
(\widehat{\mathbf{W}} - e\widehat{\mathbf{D}}) &= \begin{bmatrix} -e\frac{\partial\widehat{U}}{\partial\widehat{X}} & \frac{1}{2}\left[\frac{\partial\widehat{U}}{\partial\widehat{Y}} - e\frac{\partial\widehat{U}}{\partial\widehat{Y}}\right] + \frac{1}{2}\left[e\frac{\partial\widehat{V}}{\partial\widehat{X}} - \frac{\partial\widehat{V}}{\partial\widehat{X}}\right] & 0 \\ \frac{1}{2}\left[\frac{\partial\widehat{V}}{\partial\widehat{X}} - e\frac{\partial\widehat{V}}{\partial\widehat{X}}\right] + \frac{1}{2}\left[e\frac{\partial\widehat{U}}{\partial\widehat{Y}} - \frac{\partial\widehat{U}}{\partial\widehat{Y}}\right] & -e\frac{\partial\widehat{V}}{\partial\widehat{Y}} & 0 \\ 0 & 0 & 0 \end{bmatrix}, \\
(\widehat{\mathbf{W}} - e\widehat{\mathbf{D}})^T &= \begin{bmatrix} -e\frac{\partial\widehat{U}}{\partial\widehat{X}} & \frac{1}{2}\left[\frac{\partial\widehat{V}}{\partial\widehat{X}} - e\frac{\partial\widehat{V}}{\partial\widehat{X}}\right] + \frac{1}{2}\left[e\frac{\partial\widehat{U}}{\partial\widehat{Y}} - \frac{\partial\widehat{U}}{\partial\widehat{Y}}\right] & 0 \\ \frac{1}{2}\left[\frac{\partial\widehat{U}}{\partial\widehat{Y}} - e\frac{\partial\widehat{U}}{\partial\widehat{Y}}\right] + \frac{1}{2}\left[e\frac{\partial\widehat{V}}{\partial\widehat{X}} - \frac{\partial\widehat{V}}{\partial\widehat{X}}\right] & -e\frac{\partial\widehat{V}}{\partial\widehat{Y}} & 0 \\ 0 & 0 & 0 \end{bmatrix},
\end{aligned} \tag{1.23}$$

$$2\eta\widehat{\mathbf{D}} = \begin{bmatrix} 2\eta\frac{\partial\widehat{U}}{\partial\widehat{X}} & \left[\eta\frac{\partial\widehat{U}}{\partial\widehat{Y}} + \eta\frac{\partial\widehat{V}}{\partial\widehat{X}}\right] & 0 \\ \left[\eta\frac{\partial\widehat{V}}{\partial\widehat{X}} + \eta\frac{\partial\widehat{U}}{\partial\widehat{Y}}\right] & 2\eta\frac{\partial\widehat{V}}{\partial\widehat{X}} & 0 \\ 0 & 0 & 0 \end{bmatrix}, \tag{1.24}$$

$$\widehat{\mathbf{S}} + m \frac{d\widehat{\mathbf{S}}}{dt} + \widehat{\mathbf{S}} \left[ \begin{array}{c} \left[ \begin{array}{ccc} -e \frac{\partial \widehat{U}}{\partial \widehat{X}} & \frac{1}{2} \left[ \frac{\partial \widehat{U}}{\partial \widehat{Y}} - e \frac{\partial \widehat{U}}{\partial \widehat{Y}} \right] + \frac{1}{2} \left[ e \frac{\partial \widehat{V}}{\partial \widehat{X}} - \frac{\partial \widehat{V}}{\partial \widehat{X}} \right] & 0 \\ \frac{1}{2} \left[ \frac{\partial \widehat{V}}{\partial \widehat{X}} - e \frac{\partial \widehat{V}}{\partial \widehat{X}} \right] + \frac{1}{2} \left[ e \frac{\partial \widehat{U}}{\partial \widehat{Y}} - \frac{\partial \widehat{U}}{\partial \widehat{Y}} \right] & -e \frac{\partial \widehat{V}}{\partial \widehat{Y}} & 0 \\ 0 & 0 & 0 \end{array} \right] + \\ \left[ \begin{array}{ccc} -e \frac{\partial \widehat{U}}{\partial \widehat{X}} & \frac{1}{2} \left[ \frac{\partial \widehat{V}}{\partial \widehat{X}} - e \frac{\partial \widehat{V}}{\partial \widehat{X}} \right] + \frac{1}{2} \left[ e \frac{\partial \widehat{U}}{\partial \widehat{Y}} - \frac{\partial \widehat{U}}{\partial \widehat{Y}} \right] & 0 \\ \frac{1}{2} \left[ \frac{\partial \widehat{U}}{\partial \widehat{Y}} - e \frac{\partial \widehat{U}}{\partial \widehat{Y}} \right] + \frac{1}{2} \left[ e \frac{\partial \widehat{V}}{\partial \widehat{X}} - \frac{\partial \widehat{V}}{\partial \widehat{X}} \right] & -e \frac{\partial \widehat{V}}{\partial \widehat{Y}} & 0 \\ 0 & 0 & 0 \end{array} \right] \end{array} \right]$$

$$= \begin{bmatrix} 2\eta \frac{\partial \widehat{U}}{\partial \widehat{Y}} & \left[ \eta \frac{\partial \widehat{U}}{\partial \widehat{Y}} + \eta \frac{\partial \widehat{V}}{\partial \widehat{X}} \right] & 0 \\ \left[ \eta \frac{\partial \widehat{V}}{\partial \widehat{X}} + \eta \frac{\partial \widehat{U}}{\partial \widehat{Y}} \right] & 2\eta \frac{\partial \widehat{V}}{\partial \widehat{Y}} & 0 \\ 0 & 0 & 0 \end{bmatrix}, \quad (1.25)$$

$$2\mu \widehat{\mathbf{D}} = \begin{bmatrix} 2\mu \frac{\partial \widehat{U}}{\partial \widehat{X}} & \left[ \mu \frac{\partial \widehat{U}}{\partial \widehat{Y}} + \mu \frac{\partial \widehat{V}}{\partial \widehat{X}} \right] & 0 \\ \left[ \mu \frac{\partial \widehat{V}}{\partial \widehat{X}} + \mu \frac{\partial \widehat{U}}{\partial \widehat{Y}} \right] & 2\mu \frac{\partial \widehat{V}}{\partial \widehat{Y}} & 0 \\ 0 & 0 & 0 \end{bmatrix}, \quad (1.26)$$

Using Eqs (1.25) -(1.26) in (1.16), we get Cauchy stress tensor for JS fluid.

$$\begin{aligned} \tau_{\widehat{X}\widehat{X}} &= \widehat{\mathbf{S}}_{\widehat{X}\widehat{X}} - \widehat{P} + 2\mu \frac{\partial \widehat{U}}{\partial \widehat{X}}, \quad \tau_{\widehat{X}\widehat{Y}} = \tau_{\widehat{Y}\widehat{X}} = \widehat{\mathbf{S}}_{\widehat{X}\widehat{Y}} + \mu \left[ \frac{\partial \widehat{U}}{\partial \widehat{Y}} + \frac{\partial \widehat{V}}{\partial \widehat{X}} \right], \\ \tau_{\widehat{Y}\widehat{Y}} &= \widehat{\mathbf{S}}_{\widehat{Y}\widehat{Y}} - \widehat{P} + 2\mu \frac{\partial \widehat{V}}{\partial \widehat{Y}}. \end{aligned} \quad (1.27)$$

## 1.8 Solution method

Many phenomena in engineering and technology are nonlinear in nature and can be effectively represented using ordinary or partial differential equations. Finding the answer to these DEs is a difficult task due to the presence of strong nonlinearity. However, a variety of analytical and numerical techniques can be used to solve these equations. The following sections explain the fundamental concepts of a few different methods for solving (ODE) and (PDE).

### i. Perturbation Technique

The perturbation technique is the most adaptable nonlinear dynamical model procedure, and it is constantly evolving and being used on increasingly complex problems. The perturbation method is based on the presence of perturbation quantities, which are small/large variables or parameters that can be found naturally in equations or artificially introduced for convenience. To put it another way, perturbation quantities are used to convert a nonlinear problem into many linear sub-problems. The addition of the solutions to the first few sub-problems, usually no more than two terms, is the solution to the problem.

Example

Consider a nonlinear DE

$$\frac{dg}{dt} + g = \varepsilon g^2 \tag{1.28}$$

with (IC's)

$$g(0) = 1. \tag{1.29}$$

By performing straight forward expansion around  $\varepsilon$  as in Eq. (1.28), we assume the solution.

$$g(t, \varepsilon) = g_0(t, \varepsilon) + \varepsilon g_1(t, \varepsilon) + \dots, \tag{1.30}$$

placing the Eq. (1.30) in Eq. (1.29) and (1.28) we get

$$\frac{dg_0}{dt} + \varepsilon \frac{dg_1}{dt} + \dots + (g_0 + \varepsilon g_1 + \dots) = \varepsilon (g_0 + \varepsilon g_1 + \dots)^2 \tag{1.31}$$

And



$$g_0(0) + \varepsilon g_1(0) + \dots = 1. \quad (1.32)$$

One can obtain the following systems by joining like powers of  $\varepsilon$  in Eqs. (1.31) and (1.32).

**0<sup>th</sup>- order system:**

$$\frac{dg_0}{dt} + g_0 = 0, \quad g_0(0) = 1, \quad (1.33)$$

**1<sup>st</sup>-order system:**

$$\frac{dg_1}{dt} + g_1 = g_0^2, \quad g_1(0) = 0, \quad g_1'(0) = 0 \quad (1.34)$$

Eqs. (1.33) and (1.34) have the following solutions:

$$g_0 = e^{-t}, \quad (1.35)$$

$$g_1 = e^{-t} - e^{-2t}, \quad (1.36)$$

Using Eqs. (1.35)–(1.36) in (1.30), we obtain

$$g(t, \varepsilon) = e^{-t} + \varepsilon(e^{-t} - e^{-2t}) + \dots$$

## CHAPTER 2

### LITERATURE REVIEW

#### 2.1 Overview

In this chapter, we have represented the study related to peristaltic transport of JS fluid in a tapered asymmetric channel, theory of lubrication approximation and MHD with viscous dissipation and thermal radiation.

#### 2.2 Literature Review

Peristalsis is a pattern of fluid thrusting in ducts in which a progressive wave of area contraction or expansion propagates throughout the length of a fluid-filled distensible tube. Pumping fluid against an increase in pressure produces broad propulsive and mixing motions. Peristalsis is a biologically necessary component of smooth muscle contraction. It is a useful and automated system that controls numerous processes, including the movement of ovaries in the fallopian tube and the flow of bile from the gallbladder into the duodenum and bile from the kidney to the bladder. The peristalsis procedure can be applied to a variety of biological systems, such as the gastrointestinal tract's chyme movement, small blood vessels' blood flow, and the male reproductive system's duct afferents. Peristaltic pumping is also employed in industry for a few useful purposes, including the movement of hygienic fluids, the blood pump in heart-lung machines, and the movement of internal and hazardous fluids to prevent inclusion in the environment. Peristaltic phenomena are characterized as having important industrial uses in the strategy of roller pumps, which are used to pump fluids without being damaged by the connection with the pumping equipment. A positive displacement pump that is used to pump a variety of fluids is referred to as a peristaltic pump (often called a roller pump). There have been a lot of investigations into the peristaltic activity of liquids in a variety of physical contexts and flow geometries. Latham [1] examined the sinusoidal wall movement of viscous liquid. Shapiro et al. [2] employed lubrication theory to present a precise

summary of viscid fluid in peristaltic transport along a duct and tube. Abdelsalam et al. [3] examined the effects of various peristaltic factors while analyzing plasma flow with sinusoidal wall activity via a very small flexible artery using the lubrication hypothesis. Jeffrey liquid flowing with Newtonian fluid following peristaltic motion under the premise of minimal inertial forces and a small wave number was investigated by Kavitha et al. [4] The thermal radiative properties of a viscous liquid travelling over a porous surface are examined by Hussain et al. [5]. Theoretical simulations of magnetized Prandtl fluid flowing through a porous annulus are deliberated by Bhatti et al. [6]. Vaidya et al. [7] used the Rabinowitsch model with fluctuating liquid parameters to examine the sinusoidal wall explanation under the lubrication theory. The consequences of hydromagnetic peristaltic flow of Williamson liquid in a curved channel were investigated by Rashid et al. [8]. Rabinowitsch model with two compliant walls that obey peristalsis and the influence of variable liquid characteristics examined by Rajashekhar et al. [9]. The heat source and sink properties of the peristaltic transport of Prandtl-Eyring nanomaterial over the channel boundaries were studied by Akram et al. [10]. They showed that raising the parameters for wall mass and tension enhances liquid velocity, while increasing the value for wall damping has the opposite effect. The theory of lubrication approximation was implemented by Abbas et al. [11] to explain the effect of the activation energy research on the peristalsis of Casson fluid in a non-uniform tube under the effects of thermal radiation. [12–15] contains more works that are pertinent to this topic.

Theoretical modelling of NNF is crucial for predicting and comprehending the behavior of a wide range of emergent natural processes. Many natural fluids, including plasma, fuel, lubricants, oils, clay, and polymer solutions, have substantial rheologic assets which do not follow the Newton's law of viscosity's usual direct relationship between strain and stress. The performance of NNF in modern industries and technology may generate a lot of interest in the issue (see refs. [16–17]). On the other hand, the constitutive terms which are involved in modelling such fluids are often complex, making obtaining exact solutions challenging. This study took the Johnson-Segalman fluid into account. Johnson-Segalman liquid is one of the NNF imperative subclass that can describe the "spurt" fact [18]. The term "spurt" has been used to designate a huge rise in

volume with a minor upsurge in intensity in a driving rate of pressure. In a driving pressure gradient, the term "spurt" has been used to represent a high rise in volume with a little increase in intensity. Investigation of the peristaltic transport of Johnson-Segalman liquid in a curved geometry using lubrication theory to simplify the normalized equations is discussed by Hina et al. [19]. Kothandapani et al. [20] performed a theoretical examination of the peristaltic activity of Johnson-Segalman material within a microfluidic tapered pipe and determined that when the non-uniform factor is increased, pressure rise is more influenced in the free pumping area. A few more explorations into different geometries can be found in the references [21–22].

Numerous researchers are interested in the study of magnetohydrodynamic (MHD) peristaltic motion due to its expanding applications in areas such as plasma pumping, producing, medication targeting, (MRI), magnetotherapy, hyperthermia, and others. The hydromagnetic Williamson fluid's oscillatory propagation was bent by Rashid et al. [23]. Akram et al. [24] used the lubrication theory to evaluate the diffusion of Prandtl nanomaterials in the presence of Lorentz force along a non-uniform conduit with sinusoidal walls. Abbas et al. [25] reported and obtained analytical conclusions concerning the impact of Lorentz force in a channel on the peristalsis phenomenon of Jeffrey liquid. They noticed that increasing the Brinkman number caused a rise in the thermal profile. The importance of entropy analysis for the movement of hydromagnetic, viscid liquid peristalsis in a changing tube using lubrication theory approximation was recently investigated by Abbas et al. [26]. Some recent demonstrative inquiries in this approach might be found at [27–29]. Additionally, thermal radiation effects are significant on heat transfer in industry, particularly in the design of gas turbines, nuclear power plants, missiles, spacecraft, satellites, and other manufacturing and industrial machinery. It has been proven that thermal radiation works well in a variety of extreme-temperature processes. Nisar et al. [30] examined the radiative properties of the peristaltic interest of Eyring-Powell nanomaterial in flexible channel walls. The main conclusion of this study is that raising the thermal Biot number lowers the radiative profile while raising it for parameters affecting Brownian flow and thermophoresis. The thermal study of the peristaltic activity of Rabinowitch fluid in a channel was examined by Imran et al. [31]. Alsaedi et al. [32] also investigated how hall current affected the sinusoidal wall transport

of oily nanomaterials along a conduit. [33–36] contains more analyses of heat conduction by thermal radiation. Non-pregnant myometrial contractions can occur in both symmetrical and asymmetrical directions, which results in a peristaltic-type liquid transfer uterus problem known as intrauterine liquid transport. In addition, it is investigated that the intrauterine carriage of fluid in a uterus at the sagittal cross over reveals a narrow channel surrounded by two relatively comparable walls as well as wave trains with different time differences and scales [37–39]. Aside from the research indicated above, we are particularly interested in investigating the effect of heat transport phenomena on the peristaltic movement of an electrically conducting Johnson-Segalman liquid in a tapered channel with velocity slip circumstances. It is worth mentioning that such a study does not appear to be available in the current literature. The formulas governing the flow of the Johnson-Segalman liquid are simplified by lubrication theory. The perturbation technique is used to derive the following equations, and the physical properties of key variable quantities are investigated and explained using graphs.

## CHAPTER 3

# A TAPERED ASYMMETRIC CHANNEL WITH NONLINEAR PERISTALTIC MOTION OF JOHNSON- SEGALMAN FLUID

### 3.1 Overview

This comparative study discusses the nonlinear peristaltic transport of Johnson-Segalman fluid in a thin asymmetric channel. The thin asymmetric channel was formed as a peristaltic wave train passed by beyond non-uniform walls with unique amplitudes and phases. Assumptions of low Reynolds number and long wavelength were used to simplify the Johnson-Segalman fluid's 2-D equations. In order to solve the streamline, pressure gradient, and axial velocity equations, the regular perturbation method is used.

### 3.2 Mathematical formulation

Consider (2-D) channel that is infinitely asymmetric and contains an incompressible Johnson-Segalman fluid. The coordinate approach employed is rectangular, with  $X$  horizontal to the channel walls and  $Y$  perpendicular to them. There is also a proposal for an immense wave train travelling at  $c$  alongside the channel walls. The peristaltic wave train on the walls exhibits irregular amplitudes and phases. The channel walls have a specific shape.

$$H_2(\widehat{X}, t') = a_2 \sin\left(\frac{2\pi\widehat{X}}{\lambda} - \frac{ct'}{\lambda}\right) + d + k'\widehat{X}, \quad (3.1)$$

$$H_1(\widehat{X}, t') = -a_1 \sin\left(\frac{2\pi\widehat{X}}{\lambda} - \frac{ct'}{\lambda} + \phi\right) - d - k'\widehat{X}, \quad (3.2)$$

where  $\phi \in [0, \pi]$  the difference of phases and the waves amplitudes are  $a_1$  and  $a_2$ . Waves in phase are designated by  $\phi = \pi$ , while waves out of phase are designated by  $\phi = 0$ . Furthermore  $d_1$ ,  $d_2$ ,  $a_1$ ,  $a_2$  and  $\phi$  satisfy the condition.

$$a_1^2 + a_2^2 + 2a_1a_2\cos\phi \leq (2d)^2. \quad (3.3)$$

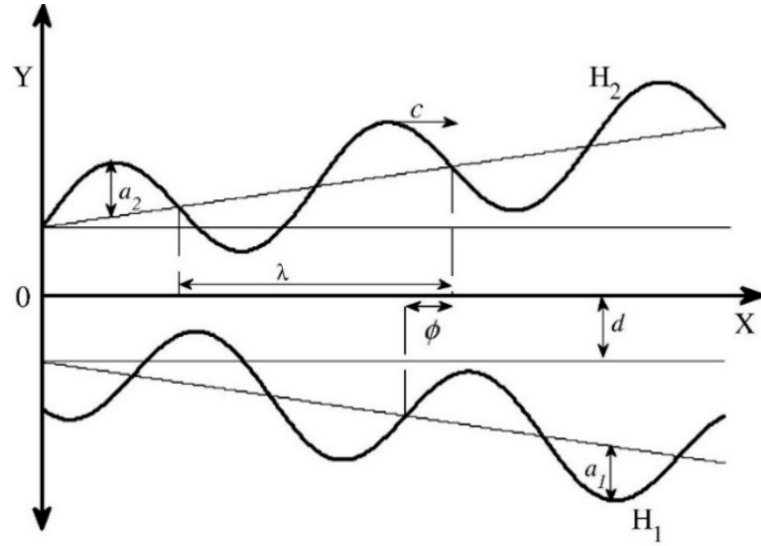


Figure 3.1: Problems geometry

An incompressible fluid flow equations are as follows:[18]

$$\text{div}\mathbf{V} = 0, \text{div}\boldsymbol{\tau} = \rho \frac{\partial \mathbf{V}}{\partial t}, \quad (3.4)$$

For a (JS) fluid, the Cauchy stress tensor is defined in Chapter one using Eqs. (1.16) - (1.18). For  $e=1$ , model (3.4) is reduced to the Maxwell fluid model, which is then recovered as the traditional NS fluid model by taking  $\mu=0$ . In the context of the situation, the 2-D flow velocity is depicted.

$$\mathbf{V} = [\widehat{U}(\widehat{X}, \widehat{Y}, t'), \widehat{V}(\widehat{X}, \widehat{Y}, t'), 0], \quad (3.5)$$

From Eqs. (3.4) and (1.16) - (1.18), we have

$$\frac{\partial \widehat{U}}{\partial \widehat{X}} + \frac{\partial \widehat{V}}{\partial \widehat{Y}} = 0, \quad (3.6)$$

$$\rho \left( \frac{\partial}{\partial t'} + \widehat{U} \frac{\partial}{\partial \widehat{X}} + \widehat{V} \frac{\partial}{\partial \widehat{Y}} \right) \widehat{U} = \frac{\partial \widehat{S}_{\widehat{X}\widehat{X}}}{\partial \widehat{X}} + \frac{\partial \widehat{S}_{\widehat{X}\widehat{Y}}}{\partial \widehat{Y}} - \frac{\partial \widehat{P}}{\partial \widehat{X}} + \mu \left( \frac{\partial^2}{\partial \widehat{X}^2} + \frac{\partial^2}{\partial \widehat{Y}^2} \right) \widehat{U}, \quad (3.7)$$

$$\rho \left( \frac{\partial}{\partial t'} + \widehat{U} \frac{\partial}{\partial \widehat{X}} + \widehat{V} \frac{\partial}{\partial \widehat{Y}} \right) \widehat{V} = \frac{\partial \widehat{S}_{\widehat{Y}\widehat{Y}}}{\partial \widehat{X}} + \frac{\partial \widehat{S}_{\widehat{X}\widehat{Y}}}{\partial \widehat{Y}} - \frac{\partial \widehat{P}}{\partial \widehat{Y}} + \mu \left( \frac{\partial^2}{\partial \widehat{X}^2} + \frac{\partial^2}{\partial \widehat{Y}^2} \right) \widehat{V}, \quad (3.8)$$

$$2\eta \frac{\partial \widehat{U}}{\partial \widehat{X}} = \widehat{S}_{\widehat{X}\widehat{X}} - 2em\widehat{S}_{\widehat{X}\widehat{X}} \frac{\partial \widehat{U}}{\partial \widehat{X}} + m\widehat{S}_{\widehat{X}\widehat{X}} \left[ \frac{\partial}{\partial t'} + \widehat{U} \frac{\partial}{\partial \widehat{X}} + \widehat{V} \frac{\partial}{\partial \widehat{Y}} \right] + m\widehat{S}_{\widehat{X}\widehat{Y}} \left[ (1-e) \frac{\partial \widehat{V}}{\partial \widehat{X}} - (1+e) \frac{\partial \widehat{U}}{\partial \widehat{Y}} \right], \quad (3.9)$$

$$\left( \eta \frac{\partial \widehat{U}}{\partial \widehat{Y}} + \eta \frac{\partial \widehat{V}}{\partial \widehat{X}} \right) = \widehat{S}_{\widehat{X}\widehat{Y}} + m\widehat{S}_{\widehat{X}\widehat{Y}} \left[ \frac{\partial}{\partial t'} + \widehat{U} \frac{\partial}{\partial \widehat{X}} + \widehat{V} \frac{\partial}{\partial \widehat{Y}} \right] + \frac{m}{2} \widehat{S}_{\widehat{X}\widehat{X}} \left[ (1-e) \frac{\partial \widehat{U}}{\partial \widehat{Y}} - (1+e) \frac{\partial \widehat{V}}{\partial \widehat{X}} \right] + \frac{m}{2} \widehat{S}_{\widehat{Y}\widehat{Y}} \left[ (1-e) \frac{\partial \widehat{V}}{\partial \widehat{X}} - (1+e) \frac{\partial \widehat{U}}{\partial \widehat{Y}} \right], \quad (3.10)$$

$$2\eta \frac{\partial \widehat{V}}{\partial \widehat{Y}} = \widehat{S}_{\widehat{Y}\widehat{Y}} - 2em\widehat{S}_{\widehat{Y}\widehat{Y}} \frac{\partial \widehat{V}}{\partial \widehat{Y}} + m\widehat{S}_{\widehat{Y}\widehat{Y}} \left[ \frac{\partial}{\partial t'} + \widehat{U} \frac{\partial}{\partial \widehat{X}} + \widehat{V} \frac{\partial}{\partial \widehat{Y}} \right] + m\widehat{S}_{\widehat{X}\widehat{Y}} \left[ (1-e) \frac{\partial \widehat{U}}{\partial \widehat{Y}} - (1+e) \frac{\partial \widehat{V}}{\partial \widehat{X}} \right], \quad (3.11)$$

Defining dimensionless quantities

$$x = \frac{\widehat{X}}{\lambda}, y = \frac{\widehat{Y}}{d}, t = \frac{ct'}{\lambda}, u = \frac{\widehat{U}}{c}, v = \frac{\widehat{V}}{c}, \delta = \frac{d}{\lambda}, h_1 = \frac{H_1}{d}, h_2 = \frac{H_2}{d}, p = \frac{d^2 \widehat{P}}{c\lambda\mu}, s_{ij} = \frac{d}{\mu c} \widehat{S}_{ij}(\widehat{X}),$$

$$Re = \frac{\rho cd}{\mu}, We = \frac{mc}{d}, a = \frac{a_1}{d}, b = \frac{a_2}{d}, p = \frac{d^2}{\lambda(\mu + \eta)c} \widehat{P}(\widehat{X}), k = \frac{\lambda k'}{d}. \quad (3.12)$$

Using (3.12) into the Eqs. (3.6) - (3.11) with the help of  $u = \psi_y, v = -\delta \psi_x$  we have

$$Re\delta(\psi_y \psi_{xy} - \psi_x \psi_{yy}) = -\frac{\partial p}{\partial x} \left( \frac{\mu + \eta}{\mu} \right) + \delta \frac{\partial}{\partial x} (s_{xx}) + \frac{\partial}{\partial y} (s_{xy}) + (\delta^2 \psi_{xxy} + \psi_{yyy}), \quad (3.13)$$



$$-Re\delta^3(\psi_y\psi_{xx} - \psi_x\psi_{yy}) = -\frac{\partial p}{\partial y}\left(\frac{\mu+\eta}{\mu}\right) + \delta^2\frac{\partial}{\partial x}(s_{yx}) + \delta\frac{\partial}{\partial y}(s_{yy}) - \delta^2\left(\frac{\delta^2\psi_{xxx}}{+\psi_{yyy}}\right), \quad (3.14)$$

$$\begin{aligned} \left(\frac{2\eta\delta}{\mu}\right)\psi_{xy} &= s_{xx} - 2emWe\delta\psi_{xy} + We\delta\left[\psi_y\frac{\partial}{\partial x}(s_{xx}) - \psi_x\frac{\partial}{\partial y}(s_{xx})\right] \\ &\quad - Wes_{xy}\left[\delta^2(1-e)\psi_{xx} + (1+e)\psi_{yy}\right], \end{aligned} \quad (3.15)$$

$$\begin{aligned} \frac{\eta}{\mu}(\psi_{yy} - \delta^2\psi_{xx}) &= s_{xy} + We\left[\psi_y\frac{\partial}{\partial x}(s_{xy}) - \psi_x\frac{\partial}{\partial y}(s_{xy})\right] \\ + \frac{We}{2}s_{xx}\left[(1-e)\psi_{yy} + \delta^2(1+e)\psi_{xx}\right] &- \frac{We}{2}s_{yy}\left[\delta^2(1-e)\psi_{xx} + (1+e)\psi_{yy}\right], \end{aligned} \quad (3.16)$$

$$\begin{aligned} -\left(\frac{2\eta\delta}{\mu}\right)\psi_{xy} &= s_{xy} + We\delta\left[\psi_y\frac{\partial}{\partial x}(s_{yy}) - \psi_x\frac{\partial}{\partial y}(s_{yy})\right] \\ + 2eWe\delta s_{yy}\psi_{xy} + Wes_{xy}\left[(1-e)\psi_{yy} + (1+e)\delta^2\psi_{xx}\right], \end{aligned} \quad (3.17)$$

Using the approximation theory of lubrication ( $Re \rightarrow 0$  and  $\delta \ll 1$ ), Equations (3.13)-(3.17) develops as follows:

$$\frac{\partial}{\partial y}s_{xy} + \psi_{yyy} = \left(\frac{\mu+\eta}{\mu}\right)\frac{\partial p}{\partial x}, \quad (3.18)$$

$$\frac{\partial p}{\partial y} = 0, \quad (3.19)$$

$$s_{xx} = We(1+e)\psi_{yy}s_{xy}, \quad (3.20)$$

$$\frac{\eta}{\mu}\psi_{yy} = s_{xy} + \frac{We}{2}(1-e)\psi_{yy}s_{xx} - \frac{We}{2}(1+e)\psi_{yy}s_{yy}, \quad (3.21)$$

$$s_{yy} = -We(1-e)\psi_{yy}s_{xy}, \quad (3.22)$$

Eq (3.19) also suggests that with this approximation.  $p \neq p(y)$ . Removal of  $\psi$  after Eqs. (3.18) and (3.19) generates

$$\frac{\partial^2}{\partial y^2}s_{xy} + \psi_{yyy} = 0, \quad (3.23)$$

Using Eqs. (3.20) and (3.22) into Eqs. (3.21), we have

$$s_{xy} = \frac{\left(\frac{\eta}{\mu}\right)\psi_{yy}}{1 + We^2(1 - e^2)(\psi_{yy})^2}, \quad (3.24)$$

Using Eq. (3.24) in Eqs. (3.18) and (3.23), We can write

$$\frac{\partial^2}{\partial y^2} \left[ \frac{\left(\frac{\eta}{\mu} + 1\right)\psi_{yy} + We^2(1 - e^2)(\psi_{yy})^3}{1 + We^2(1 - e^2)(\psi_{yy})^2} \right] = 0, \quad (3.25)$$

$$\left(\frac{\mu + \eta}{\mu}\right) \frac{\partial p}{\partial x} = \psi_{yyy} + \frac{\partial}{\partial y} \left[ \frac{\left(\frac{\eta}{\mu}\right)\psi_{yy}}{1 + We^2(1 - e^2)(\psi_{yy})^2} \right] = 0, \quad (3.26)$$

The following are the problem's relevant boundary conditions:

$$\begin{aligned} \psi &= \frac{F}{2}, & \frac{\partial \psi}{\partial y} &= 0, & \text{at } y &= h_2, \\ \psi &= -\frac{F}{2}, & \frac{\partial \psi}{\partial y} &= 0, & \text{at } y &= h_1. \end{aligned} \quad (3.27)$$

### 3.3 Solution of the problem

When using binomial for small  $We^2$ , Eqs. (3.25) and (3.26), may be simplified

$$\frac{\partial^2}{\partial y^2} \left[ \psi_{yy} + We^2\alpha_1(\psi_{yy})^3 + We^4\alpha_2(\psi_{yy})^5 \right] = 0, \quad (3.28)$$

$$\frac{\partial p}{\partial x} = \psi_{yyy} + We^2\alpha_1 \frac{\partial}{\partial y} \left[ (\psi_{yy})^3 \right] + We^4\alpha_2 \frac{\partial}{\partial y} \left[ (\psi_{yy})^5 \right], \quad (3.29)$$

$$\text{where, } \alpha_1 = \frac{(e^2 - 1)\eta}{(\eta + \mu)}, \alpha_2 = (e^2 - 1)\alpha_1,$$

**0<sup>th</sup> - order system**

$$\frac{\partial^4 \psi_0}{\partial y^4} = 0, \quad (3.30)$$

$$\frac{\partial p_0}{\partial x} = \frac{\partial^3 \psi_0}{\partial y^3}, \quad (3.31)$$

$$\begin{aligned} \psi_0 &= \frac{F}{2}, & \frac{\partial \psi_0}{\partial y} &= 0, & \text{at } y &= h_2, \\ \psi_0 &= -\frac{F}{2}, & \frac{\partial \psi_0}{\partial y} &= 0, & \text{at } y &= h_1. \end{aligned} \quad (3.32)$$

**1<sup>st</sup> - order system**

$$\frac{\partial^4 \psi_1}{\partial y^4} = -\alpha_1 \frac{\partial^2}{\partial y^2} \left[ \left( \frac{\partial^2 \psi_0}{\partial y^2} \right)^3 \right], \quad (3.33)$$

$$\frac{\partial p_1}{\partial x} = \frac{\partial}{\partial y} \left[ \frac{\partial^2 \psi_1}{\partial y^2} + \alpha_1 \left( \frac{\partial^2 \psi_0}{\partial y^2} \right)^3 \right], \quad (3.34)$$

$$\begin{aligned} \psi_1 &= \frac{F}{2}, & \frac{\partial \psi_1}{\partial y} &= 0, & \text{at } y &= h_2, \\ \psi_1 &= -\frac{F}{2}, & \frac{\partial \psi_1}{\partial y} &= 0, & \text{at } y &= h_1. \end{aligned} \quad (3.35)$$

**2<sup>nd</sup> - order system**

$$\frac{\partial^4 \psi_2}{\partial y^4} = -3\alpha_1 \frac{\partial^2}{\partial y^2} \left[ \frac{\partial^2 \psi_1}{\partial y^2} \left( \frac{\partial^2 \psi_0}{\partial y^2} \right)^2 \right] - \alpha_2 \frac{\partial^2}{\partial y^2} \left[ \left( \frac{\partial^2 \psi_0}{\partial y^2} \right)^5 \right], \quad (3.36)$$

$$\frac{\partial p_2}{\partial x} = \frac{\partial^3 \psi_2}{\partial y^3} + 3\alpha_1 \frac{\partial}{\partial y} \left[ \frac{\partial^2 \psi_1}{\partial y^2} \left( \frac{\partial^2 \psi_0}{\partial y^2} \right)^2 \right] + \alpha_2 \frac{\partial}{\partial y} \left[ \left( \frac{\partial^2 \psi_0}{\partial y^2} \right)^5 \right], \quad (3.37)$$

$$\begin{aligned} \psi_2 &= \frac{F}{2}, & \frac{\partial \psi_2}{\partial y} &= 0, & \text{at } y &= h_2, \\ \psi_2 &= -\frac{F}{2}, & \frac{\partial \psi_2}{\partial y} &= 0, & \text{at } y &= h_1. \end{aligned} \quad (3.38)$$

Solving the above systems yields axial velocity, stream function, and pressure gradient.

The usual increase in  $\Delta p$  concluded one wavelength period is given by

$$\Delta p = \int_0^1 \int_0^1 \frac{\partial p}{\partial x} dx dt. \quad (3.39)$$

### 3.4 Graphical results and discussion

We consider that the instantaneous volume rate  $F(x, t)$  of flow is periodic in  $(x-t)$  to examine the quantitative results obtained.

$$F(x, t) = Q + a \sin 2\pi(x-t) + b \sin[2\pi(x-t) + \phi]. \quad (3.40)$$

$Q$  is the flow's average time value throughout a single wave period.

The integration of  $\frac{\partial p}{\partial x}$  is used in the expression for  $\Delta p$ . Eq. (3.39) is not integrable

analytically due to the complexity of  $\frac{\partial p}{\partial x}$ . As a result, the evaluation of the integrals

necessitates the use of a numerical integration scheme. The result is executed with the

help of MATHEMATICA, and all graphs were made for several values of the variables

of importance. Because the (PDE) system resulting from the mathematical modelling of

the problem at hand is strongly nonlinear and coupled, it cannot be used directly for the

analytical solution. As a result, the formulas for axial velocity, pressure rise, and

streamlines are handled and checked for differences in flow parameters. Figures (3.2 -

3.7) exhibits a graph of the  $\Delta p$  vs. the change in time-average flux  $Q$ . Figures. (3.2 - 3.7)

demonstrate pumping zones such as peristaltic injecting ( $Q > 0, \Delta p > 0$ ) enhanced driving

( $Q > 0, \Delta p < 0$ ), and backward injecting ( $Q < 0, \Delta p > 0$ ). Figure 3.2 depicts the  $\Delta p$  as

a function of  $(a)$ . As shown in Fig. 3.3, the peristaltic pumping section and free thrusting

( $\Delta p = 0$ ) diminish as the non-consistent factor  $(k)$  increases, and the situation is

remarkably like that of enhanced pumping. For various values of  $(We)$ , Figure 3.4

depicts the variance of  $\Delta p$  vs  $Q$ . The pumping rate drops as  $(We)$  increases, and the

free pumping bends seem to be intersecting. The graph in Figure 3.5 shows that the  $Q$

rises as  $\Delta p$  diminishes, and the pumping area shrinks as the amplitude of phase difference

$(\phi)$  rises. For several values of the slip factor  $(e)$ , the plots of  $\Delta p$  against  $Q$  are shown in Fig. 3.6. It illustrates that the dispersal of  $\Delta p$  in a rising trend due to the slip factor  $(e)$  is nonlinear. The fluctuations of the dynamic viscosity factor on  $\Delta p$  against  $Q$  are shown in Figure 3.7. The  $\Delta p$  is reduced by enhancing the dynamic viscosity factor  $(\eta)$  in the enhanced pumping zone ( $\Delta p < 0$  and  $Q > 0$ ), as shown in this graph. The nonlinear nature of the curves depicting the  $\Delta p$  against  $Q$  is reflected in the nonlinear nature of the curves for large values of  $(\eta)$ . Fig. 3.8 shows the impact of the bottom wall's amplitude  $(a)$  on the axial velocity. The axial velocity rises by rising  $(a)$ . Figure 3.9 depicts the influence of the slip factor  $(e)$  on  $u$ . The axial velocity  $u$  seems to decline in the trapped asymmetric channel's nearer lower and upper halves; however, the differing compartment seems to be reflected in the trapped channel's core region. The velocity dispersal of the liquid is studied for several variations of the dynamic viscosity factor  $(\eta)$  non-uniform factor  $(k)$ , and  $(We)$  in Figures (3.10 - 3.12). The graphs show that increasing the values of  $(\eta)$ ,  $(k)$ , and  $(We)$  lowers the axial velocity in the tapered asymmetric channel's central area. The impact of  $Q$  on the  $u$  allocation is seen in Figure 3.13. It demonstrates that when  $Q$  rises,  $u$  rises with it.

Another interesting aspect of the occurrence is the trapping (PT). When closed streamlines in a reference wave structure form an internally moving bolus of fluid, the peristaltic wave pushes it forward. Bolus can also be discovered in the fixed frame, owing to the impact of a time-average of the stream over a single wave period which is nonzero. Figure 3.14 depicts the streamlines for various  $s$  values. It's also worth noting that when  $a$  increases, the amount of the bolus grows. The sound impacts of  $(We)$  on trapping are depicted in Fig.3.15 for the tapered asymmetric channel. The bolus is irregular around the centerline, as seen in Figure 3.15(a), and its size reduces as  $(We)$  rises. Figure 3.16 shows the effect of  $Q$  on the streamlines. The trapped bolus grows, and further trapped bolus seems as  $Q$  rises.

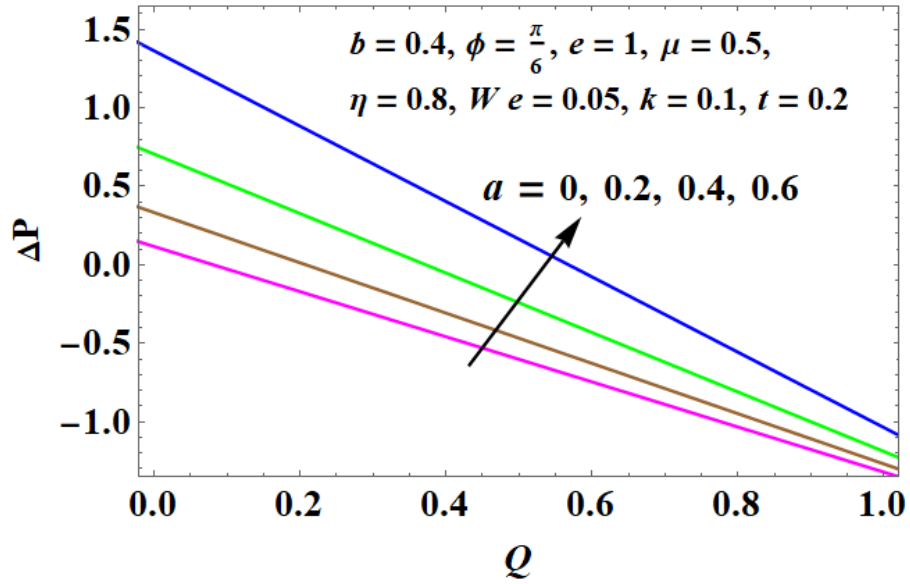


Figure 3.2: Upshot of  $a$  on pressure

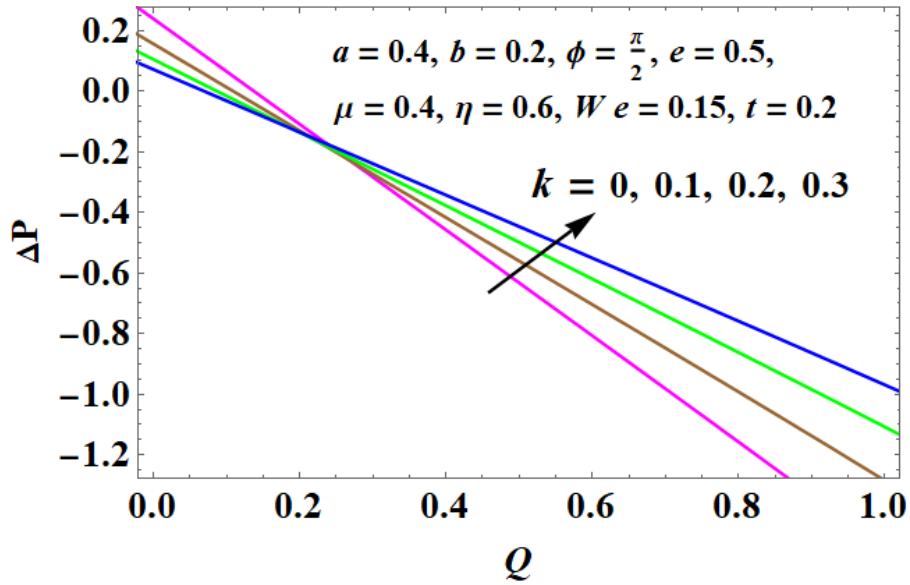


Figure 3.3: Upshot of  $k$  on pressure

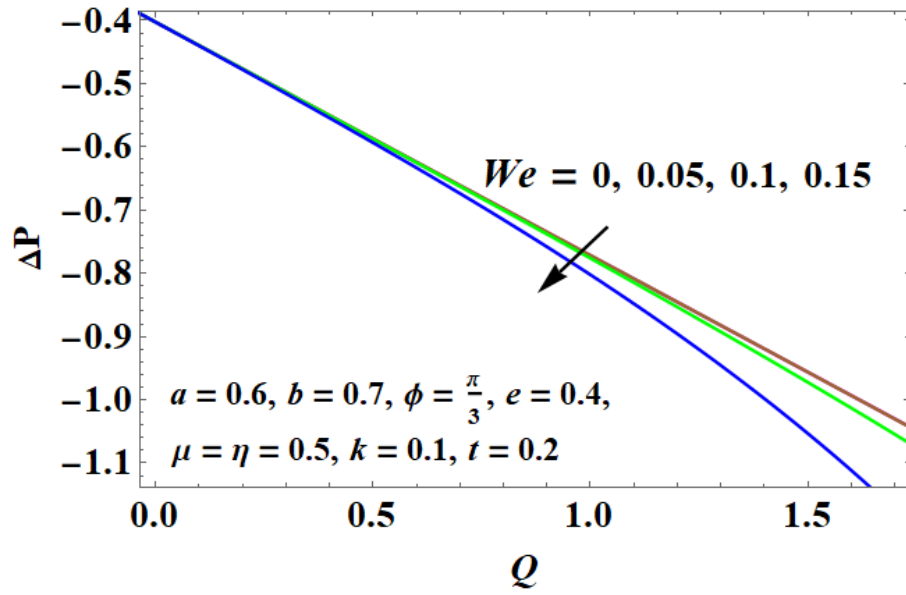


Figure 3.4: Upshot of  $We$  on pressure.

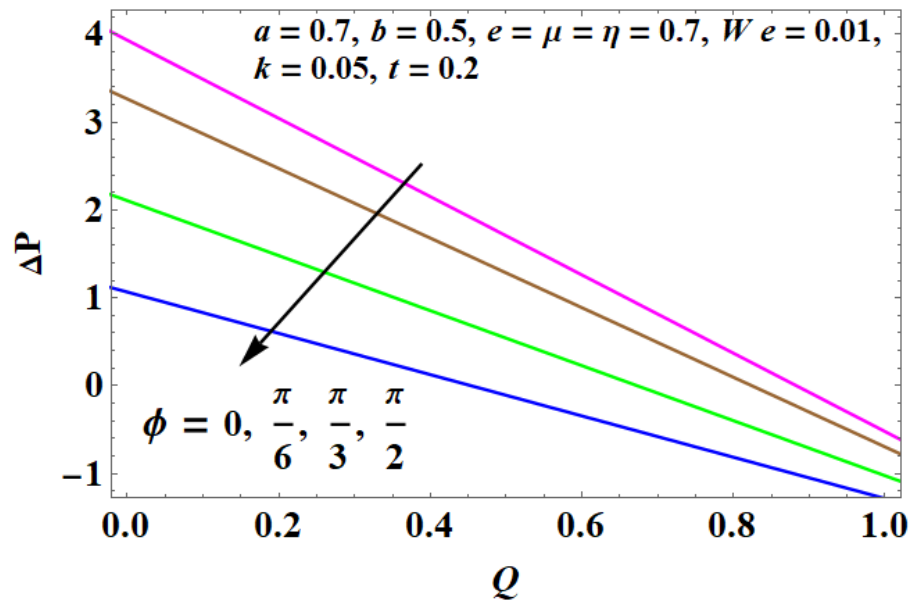


Figure 3.5: Upshot of  $\phi$  on pressure.

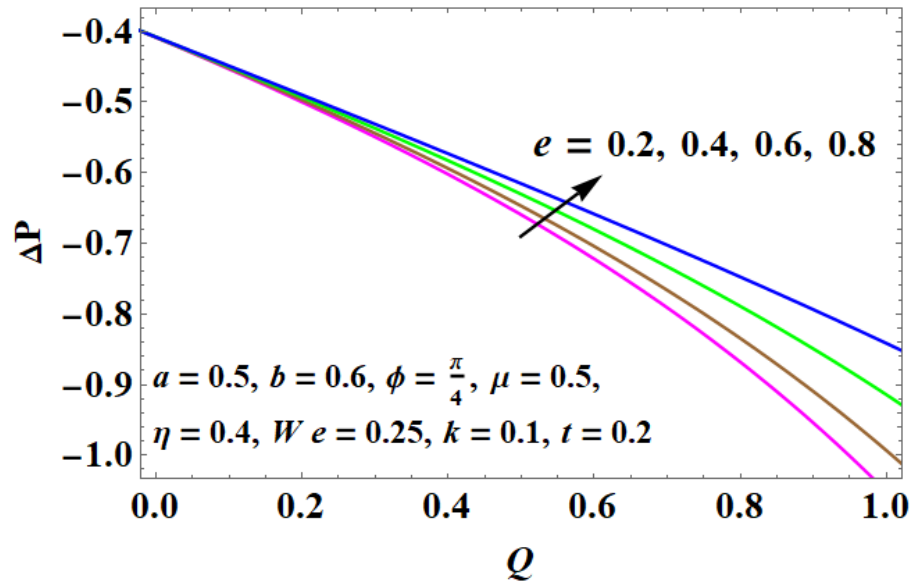


Figure 3.6: Upshot of  $e$  on pressure.

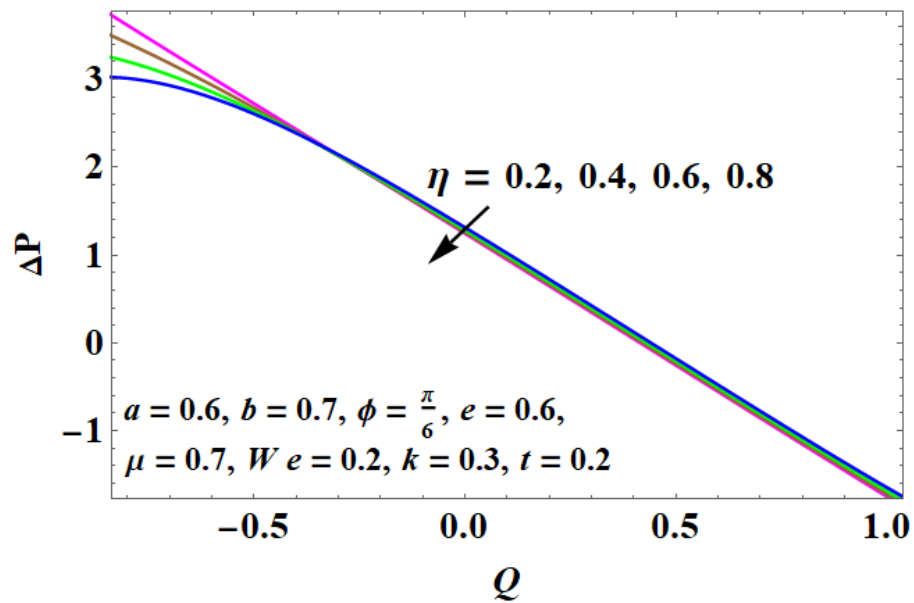


Figure 3.7: Upshot of  $\eta$  on pressure.



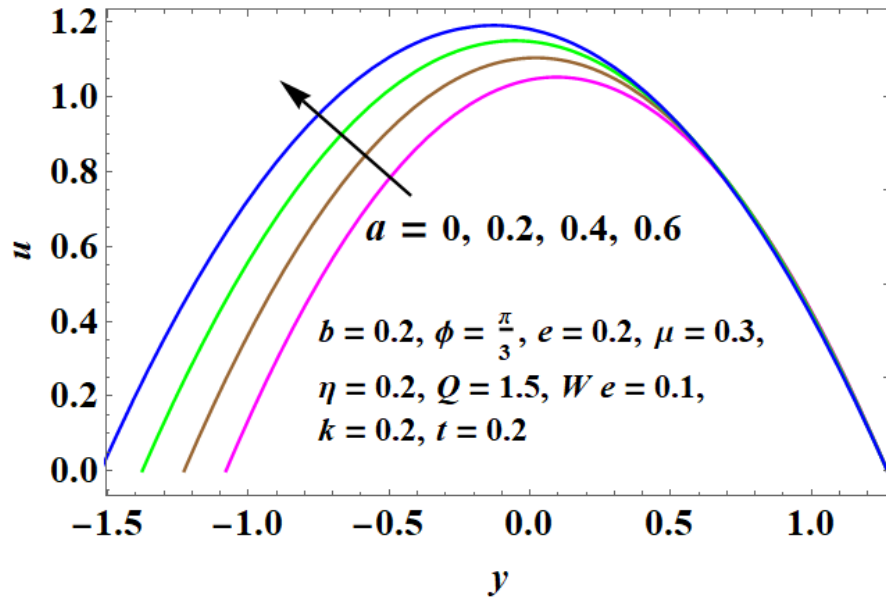


Figure 3.8: Upshot of  $a$  on axial velocity.

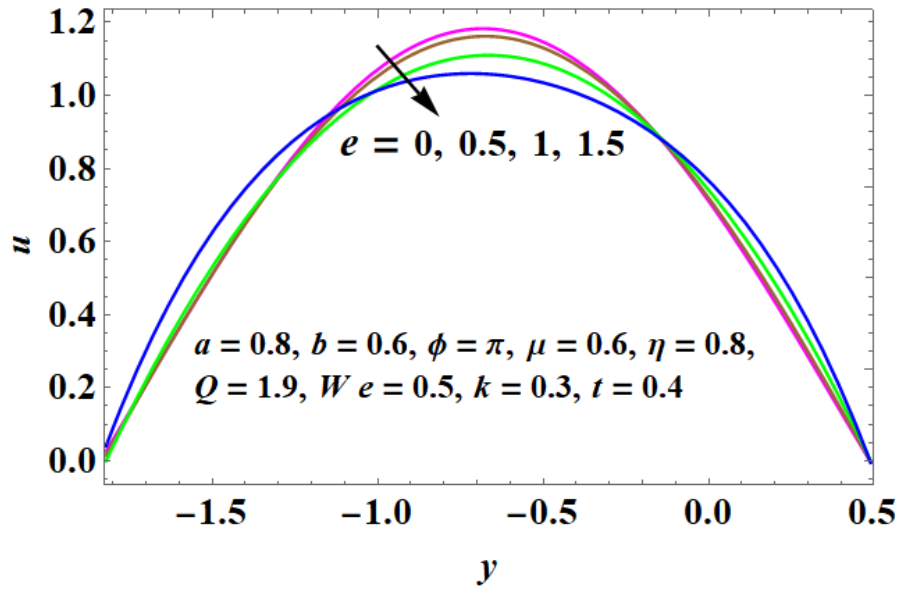


Figure 3.9: Upshot of  $e$  on axial velocity

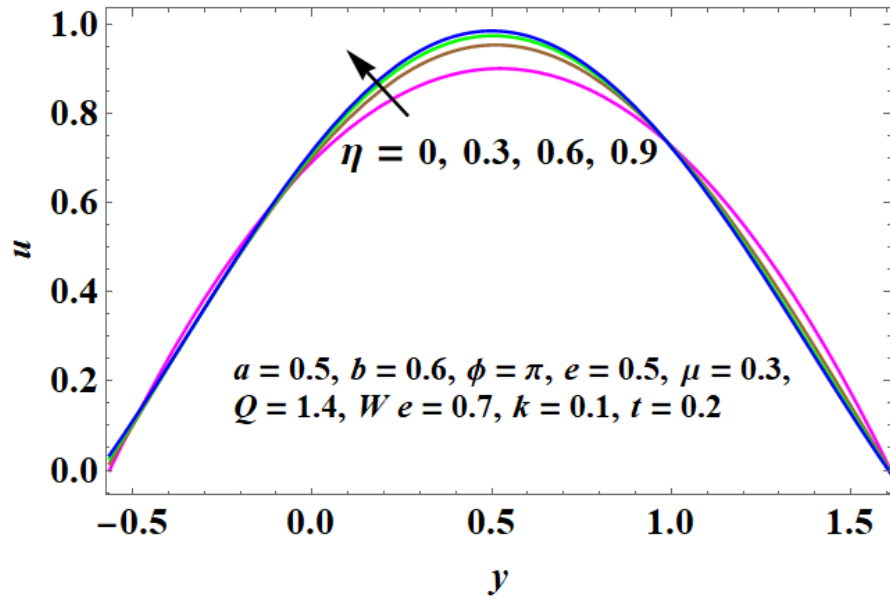


Figure 3.10: Upshot of  $\eta$  on axial velocity.

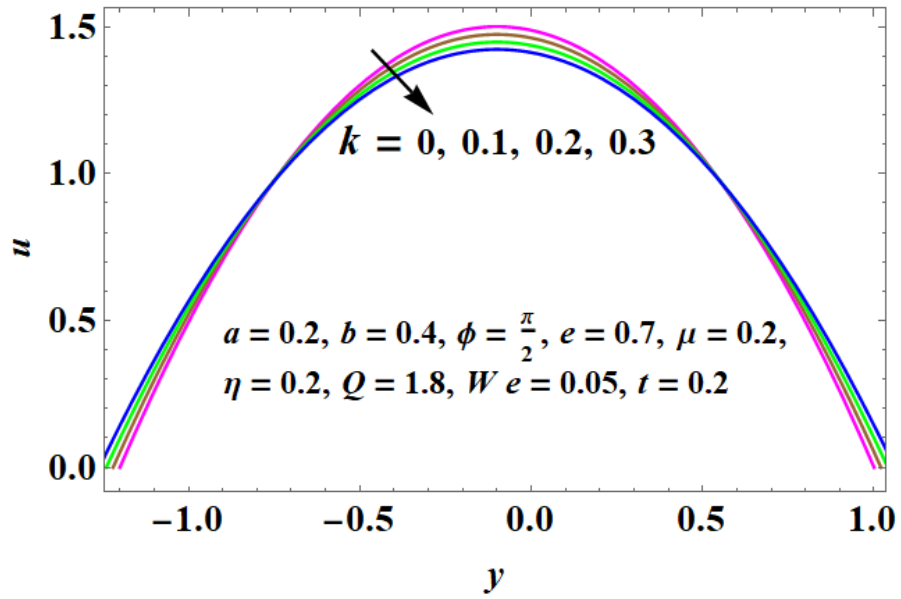


Figure 3.11: Upshot of  $k$  on axial velocity

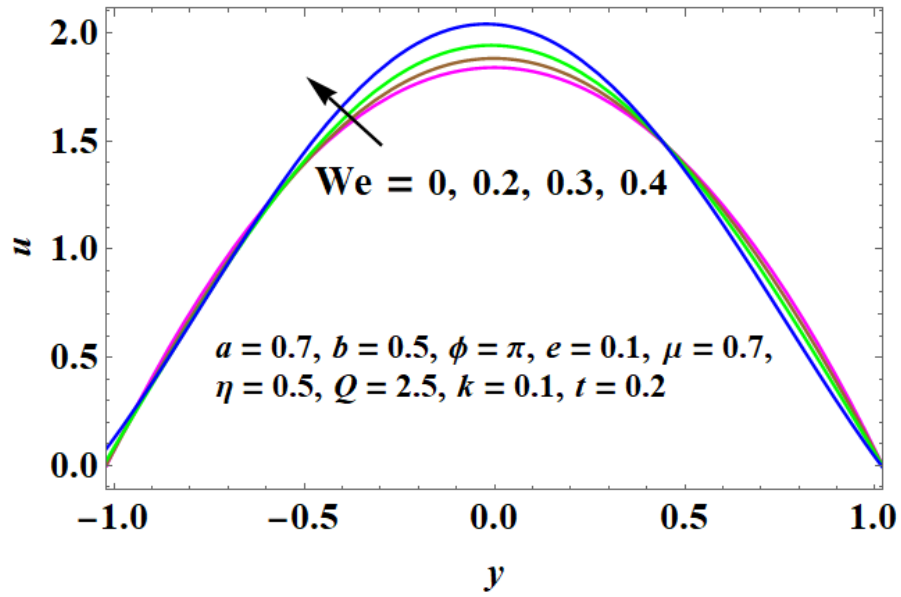


Figure 3.12: Upshot of  $We$  on axial velocity.

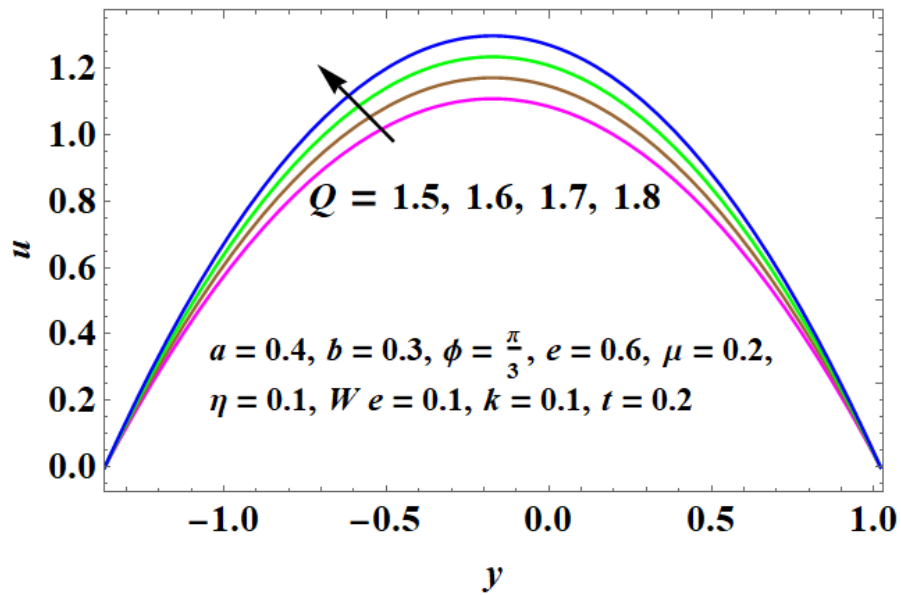


Figure 3.13: Upshot of  $Q$  on axial velocity

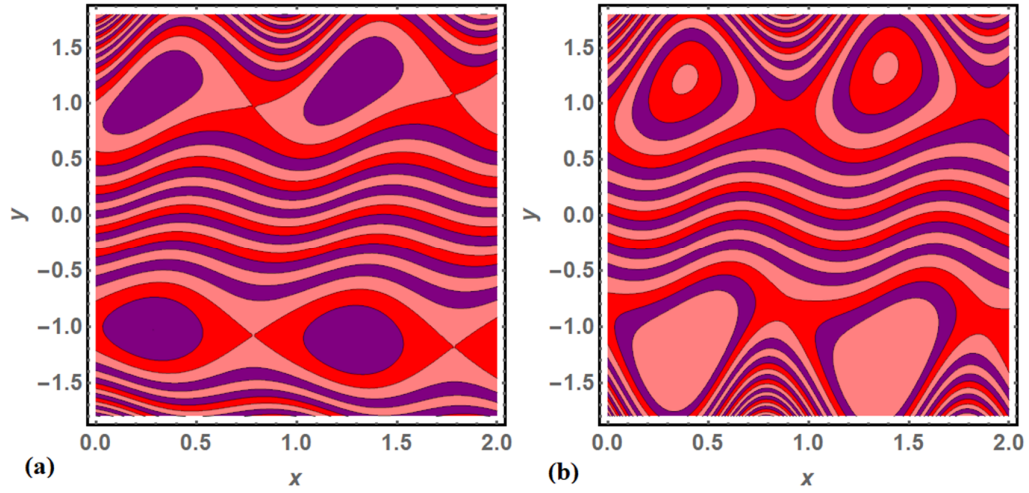


Figure 3.14: Streamlines for different values of (a)  $a = 0$ , (b)  $a = 0.3$  while other factors are  $b = 0.2$ ,  $\phi = \frac{\pi}{3}$ ,  $e = 0.7$ ,  $\mu = 0.8$ ,  $\eta = 0.5$ ,  $Q = 1.8$ ,  $We = 0.1$ ,  $k = 0.1$ ,  $t = 0.2$

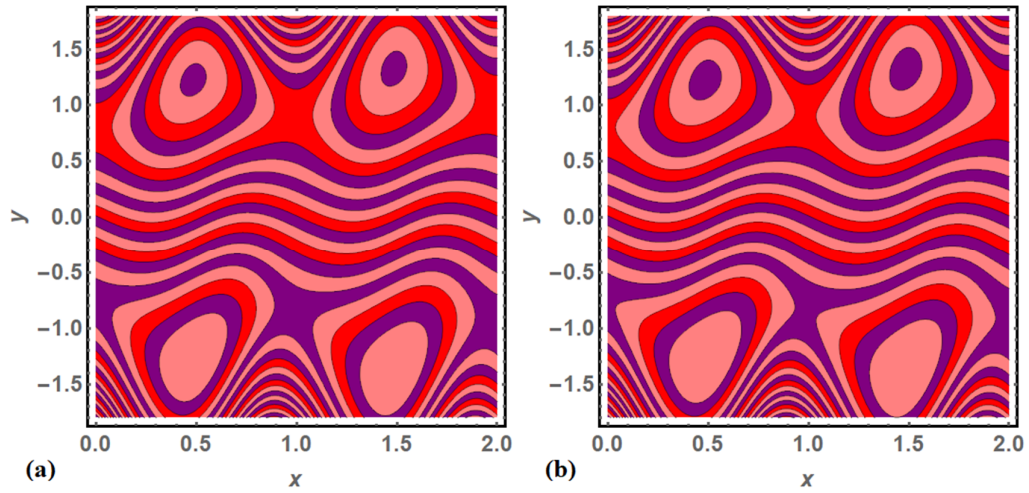


Figure 3.15: Streamlines for different values of (a)  $Q = 1.5$ , (b)  $Q = 1.6$  while other factors are  $a = 0.3$ ,  $b = We = e = 0.2$ ,  $\phi = \frac{\pi}{3}$ ,  $\mu = 0.8$ ,  $\eta = 0.5$ ,  $k = 0.1$ ,  $t = 0.3$

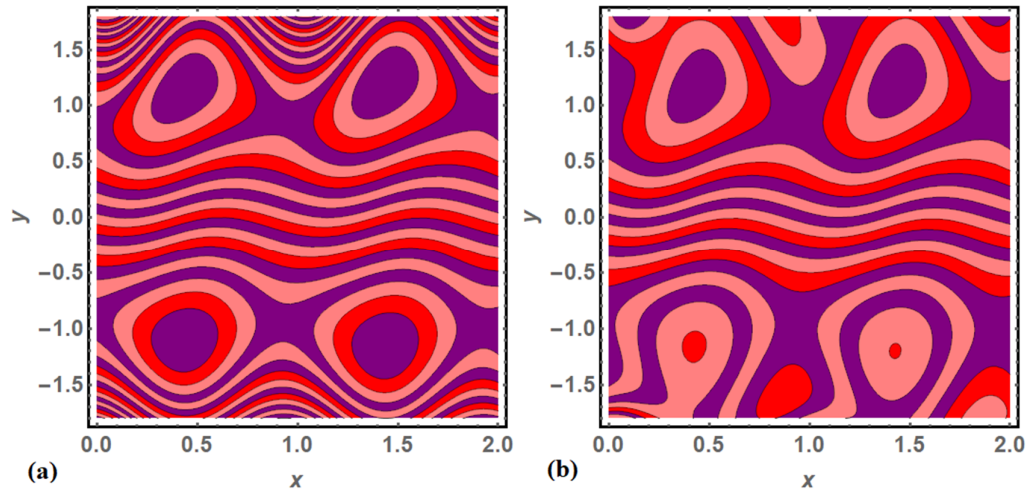


Figure 3.16: Streamlines for different values of (a)  $We = 0$ , (b)  $We = 0.6$  while other factors are  $a = 0.1$ ,  $b = 0.2$ ,  $\phi = \frac{\pi}{3}$ ,  $e = 0.4$ ,  $\mu = 0.1$ ,  $\eta = 0.8$ ,  $Q = 1.2$ ,  $k = 0.05$ ,  $t = 0.3$ .

## CHAPTER 4

# HEAT TRANSFER ANALYSIS OF JOHNSON-SEGALMAN FLUID IN TAPERED ASYMMETRIC CHANNEL

### 4.1 Overview

This chapter examines the heat transfer study of a Johnson-Segalman liquid in a tapered asymmetric channel, MHD with viscous dissipation and radiation effects. To create the Johnson-Segalman fluid model's governing equations, dimensionless variables were used. Using the perturbation approach, we can resolve these equations. At the conclusion, the results will be shown in graphs.

### 4.2 Problem Statement

Consider an incompressible peristaltic motion of electrically conducting Johnson-Segalman liquid through a two-dimensional tapering channel with velocity slip at upper and lower walls. Flow inside the thin channel is produced by the trains of sinusoidal waves moving alongside the walls of the channel with constant speed  $c$ . We employ a rectangular coordinate system in such a manner that  $X$  – axis is taken in the flow direction and  $Y$  – axis is taken perpendicular to the direction of flow (see Fig. 4.1). A uniform applied magnetic field is employed in the oblique direction with strength  $\mathbf{B}_0$ . For the peristaltic pattern, the wave trains with distinct amplitude and phases at both boundaries of the channel is given as

$$H_1(\widehat{X}, t') = -a_1 \sin\left(\frac{2\pi \widehat{X}}{\lambda} - \frac{ct'}{\lambda} + \phi\right) - d - k' \widehat{X}, \quad (4.1)$$

$$H_2(\widehat{X}, t') = a_2 \sin\left(\frac{2\pi \widehat{X}}{\lambda} - \frac{ct'}{\lambda}\right) + d + k' \widehat{X}, \quad (4.2)$$

where  $\phi \in [0, \pi]$  represents the phase difference and amplitudes of the waves are  $a_1, a_2$ . Keep in mind, waves are in phase when  $\phi = \pi$ , while waves out of phase are designated by  $\phi = 0$ . Furthermore  $d_1, d_2, a_1, a_2$  and  $\phi$  satisfy the condition

$$a_1^2 + a_2^2 + 2a_1a_2 \cos \phi \leq (2d)^2.$$

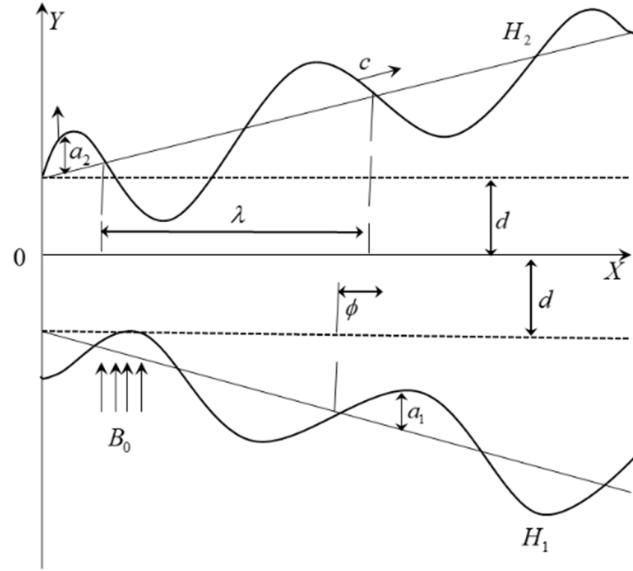


Figure 4.1: Problems geometry

The important equations to govern the flow in vector form are given as [18]:

$$\nabla \cdot \mathbf{V} = 0, \quad (4.3)$$

$$\frac{d\mathbf{V}}{dt} = \frac{1}{\rho} \text{div} \boldsymbol{\tau} + \frac{1}{\rho} \mathbf{f}, \quad (4.4)$$

$$\frac{dT}{dt} = \frac{1}{\rho C_p} \boldsymbol{\tau} \cdot \mathbf{L} + \frac{\xi}{\rho C_p} \nabla^2 T - \frac{1}{\rho C_p} \nabla \cdot \mathbf{q}_r. \quad (4.5)$$

where  $d/dt$  designates the material derivative,  $\boldsymbol{\tau}$  signifies the Cauchy stress tensor and  $\mathbf{V}$  indicates the velocity vector.

The (JS) material has the subsequent mathematical illustration for its extra stress tensor [18]: which is defined in chapter one Eqs. (1.16) -(1.18).

Notice that the current model diminishes to fluid model given by Maxwell for  $e=1$  and  $\mu = 0$ , we attain the basic NS model.

The velocity for 2-D unsteady flow is defined as:

$$\mathbf{V} = \left[ \widehat{U}(\widehat{X}, \widehat{Y}, t'), \widehat{V}(\widehat{X}, \widehat{Y}, t'), 0 \right]. \quad (4.6)$$

The vector equations in components form are given by:

$$\widehat{U}_{\widehat{X}} + \widehat{V}_{\widehat{Y}} = 0, \quad (4.7)$$

$$\rho(\widehat{U}_{t'} + \widehat{U}\widehat{U}_{\widehat{X}} + \widehat{V}\widehat{U}_{\widehat{Y}}) = (\widehat{S}_{\widehat{X}\widehat{X}})_{\widehat{X}} + (\widehat{S}_{\widehat{X}\widehat{Y}})_{\widehat{Y}} - \widehat{P}_{\widehat{X}} + \mu(\widehat{U}_{\widehat{X}\widehat{X}} + \widehat{U}_{\widehat{Y}\widehat{Y}}) - \sigma B_0^2 \widehat{U}, \quad (4.8)$$

$$\rho(\widehat{V}_{t'} + \widehat{U}\widehat{V}_{\widehat{X}} + \widehat{V}\widehat{V}_{\widehat{Y}}) = (\widehat{S}_{\widehat{Y}\widehat{Y}})_{\widehat{X}} + (\widehat{S}_{\widehat{X}\widehat{Y}})_{\widehat{Y}} - \widehat{P}_{\widehat{Y}} + \mu(\widehat{V}_{\widehat{X}\widehat{X}} + \widehat{V}_{\widehat{Y}\widehat{Y}}), \quad (4.9)$$

$$2\eta\widehat{U}_{\widehat{X}} = \widehat{S}_{\widehat{X}\widehat{X}} - 2em\widehat{S}_{\widehat{X}\widehat{X}}\widehat{U}_{\widehat{X}} + m \left[ (\widehat{S}_{\widehat{X}\widehat{X}})_{t'} + \widehat{U}(\widehat{S}_{\widehat{X}\widehat{X}})_{\widehat{X}} + \widehat{V}(\widehat{S}_{\widehat{X}\widehat{X}})_{\widehat{Y}} \right] + m \left[ (1-e)\widehat{V}_{\widehat{X}} - (1+e)\widehat{U}_{\widehat{X}} \right] \widehat{S}_{\widehat{X}\widehat{X}}, \quad (4.10)$$

$$\eta(\widehat{U}_{\widehat{Y}} + \widehat{V}_{\widehat{X}}) = \widehat{S}_{\widehat{X}\widehat{Y}} + m\widehat{S}_{\widehat{X}\widehat{Y}} \left[ (\widehat{S}_{\widehat{X}\widehat{Y}})_{t'} + \widehat{U}(\widehat{S}_{\widehat{X}\widehat{Y}})_{\widehat{X}} + \widehat{V}(\widehat{S}_{\widehat{X}\widehat{Y}})_{\widehat{Y}} \right] + \frac{m}{2}\widehat{S}_{\widehat{X}\widehat{X}} \left[ (1-e)\widehat{U}_{\widehat{Y}} - (1-e)\widehat{V}_{\widehat{X}} \right] + \frac{m}{2}\widehat{S}_{\widehat{Y}\widehat{Y}} \left[ (1-e)\widehat{V}_{\widehat{X}} - (1-e)\widehat{U}_{\widehat{Y}} \right], \quad (4.11)$$

$$2\eta\widehat{V}_{\widehat{Y}} = \widehat{S}_{\widehat{Y}\widehat{Y}} - 2em\widehat{S}_{\widehat{Y}\widehat{Y}}\widehat{V}_{\widehat{Y}} + m \left[ (\widehat{S}_{\widehat{Y}\widehat{Y}})_{t'} + \widehat{U}(\widehat{S}_{\widehat{Y}\widehat{Y}})_{\widehat{X}} + \widehat{V}(\widehat{S}_{\widehat{Y}\widehat{Y}})_{\widehat{Y}} \right] + m \left[ (1-e)\widehat{U}_{\widehat{Y}} - (1-e)\widehat{V}_{\widehat{X}} \right] \widehat{S}_{\widehat{X}\widehat{Y}}, \quad (4.12)$$

$$\rho C_p (T_{t'} + \widehat{U}T_{\widehat{X}} + \widehat{V}T_{\widehat{Y}}) = \xi(T_{\widehat{X}\widehat{X}} + T_{\widehat{Y}\widehat{Y}}) + (\widehat{U}_{\widehat{Y}} + \widehat{V}_{\widehat{X}}) \widehat{S}_{\widehat{X}\widehat{Y}} + \widehat{S}_{\widehat{Y}\widehat{Y}}\widehat{V}_{\widehat{Y}} + \widehat{S}_{\widehat{X}\widehat{X}}\widehat{U}_{\widehat{X}} - (q_r)_{\widehat{Y}}. \quad (4.13)$$

Defining the following dimensionless quantities

$$M = \sqrt{\sigma/\mu} B_0 d, \quad Br = Ec \text{ Pr}, \quad q_r = -\frac{16\sigma^* T_0^3}{3k^*} T_{\widehat{Y}}, \quad \theta = \frac{T - T_0}{T_1 - T_0}. \quad (4.14)$$

Invoking Eq. (3.12) and dimensionless quantities in Eq. (4.14) into Eqs. (4.7) - (4.13) and introducing stream functions  $u = \psi_y, v = -\delta\psi_x$ , we have

$$Re\delta(\psi_y\psi_{xy} - \psi_x\psi_{yy}) + M^2\psi_y + p_x \left( \frac{\mu + \eta}{\mu} \right) = \delta(s_{xx})_x + (s_{xy})_y + (\delta^2\psi_{xxy} + \psi_{yyy}), \quad (4.15)$$



$$-Re\delta^3(\psi_y\psi_{xx} - \psi_x\psi_{xy}) = -p_y \left( \frac{\mu + \eta}{\mu} \right) + \delta^2(s_{yx})_x + \delta(s_{yy})_y - \delta^2(\delta^2\psi_{xxx} + \psi_{xyy}), \quad (4.16)$$

$$\begin{aligned} \left( \frac{2\eta\delta}{\mu} \right) \psi_{xy} + 2ems_{xx}We\delta\psi_{xy} &= s_{xx} + We\delta \left[ \psi_y(s_{xx})_x - \psi_x(s_{xx})_y \right] \\ &- Wes_{xy} \left[ \delta^2(1-e)\psi_{xx} + (1+e)\psi_{yy} \right], \end{aligned} \quad (4.17)$$

$$\begin{aligned} \frac{\eta}{\mu}(\psi_{yy} - \delta^2\psi_{xx}) &= s_{xy} + We\delta \left[ \psi_y(s_{xy})_x - \psi_x(s_{xy})_y \right] \\ &+ \frac{We}{2}s_{xx} \left[ (1-e)\psi_{yy} + \delta^2(1+e)\psi_{xx} \right] - \frac{We}{2} \left[ \delta^2(1-e)\psi_{xx} + (1+e)\psi_{yy} \right] s_{yy}, \end{aligned} \quad (4.18)$$

$$\begin{aligned} - \left( \frac{2\eta\delta}{\mu} \right) \psi_{xy} &= s_{xy} + 2eWe\delta s_{yy}\psi_{xy} + We\delta \left[ \psi_y(s_{yy})_x - \psi_x(s_{yy})_y \right] + \\ &Wes_{xy} \left[ (1-e)\psi_{yy} + (1+e)\delta^2\psi_{xx} \right], \end{aligned} \quad (4.19)$$

$$Pr Re \delta (\psi_y\theta_x - \psi_x\theta_y) = (\theta_{yy} + \delta^2\theta_{xx}) + B_r \left( \frac{\delta s_{xx}\psi_{xy} - \delta\psi_{xy}s_{yy}}{+s_{xy}(\psi_{yy} - \delta^2\psi_{xx})} \right) + Rd\theta_{yy}. \quad (4.20)$$

Utilizing approximation theory of lubrication i.e ( $Re \rightarrow 0$  and  $\delta \ll 1$ ), Eqs. (4.15) -(4.20) turns into:

$$\left( \frac{\mu + \eta}{\mu} \right) p_x = (s_{xy})_y + \psi_{yyy} - M^2\psi_y, \quad (4.21)$$

$$p_y = 0, \quad (4.22)$$

$$s_{xx} = We(1+e)\psi_{yy}s_{xy}, \quad (4.23)$$

$$\frac{\eta}{\mu}\psi_{yy} = s_{xy} + \frac{We}{2}(1-e)\psi_{yy}s_{xx} - \frac{We}{2}(1+e)\psi_{yy}s_{yy}, \quad (4.24)$$

$$s_{yy} = -We(1-e)\psi_{yy}s_{xy}, \quad (4.25)$$

$$\theta_{yy} = \frac{B_r s_{xy} \psi_{yy}}{(1+Rd)} \quad (4.26)$$

Removal of pressure from Eqs. (4.21) and (4.22), we have

$$(s_{xy})_{yy} + \psi_{yyy} - M^2\psi_{yy} = 0. \quad (4.27)$$

Invoking Eqs. (4.23), (4.25) into Eq. (4.24), we have

$$s_{xy} = \frac{\left(\frac{\eta}{\mu}\right)\psi_{yy}}{1+We^2(1-e^2)(\psi_{yy})^2}. \quad (4.28)$$

Eq. (4.28) allows Eqs. (4.21), (4.26), and (4.27) to be written in the following form

$$\frac{\partial^2}{\partial y^2} \left[ \frac{\left(\frac{\eta}{\mu}+1\right)\psi_{yy} + We^2(1-e^2)(\psi_{yy})^3}{1+We^2(1-e^2)(\psi_{yy})^2} \right] = M^2\psi_{yy}, \quad (4.29)$$

$$\left(\frac{\mu+\eta}{\mu}\right)p_x = \frac{\partial}{\partial y} \left[ \frac{\left(\frac{\eta}{\mu}\right)\psi_{yy}}{1+We^2(1-e^2)(\psi_{yy})^2} \right] + \psi_{yyy} = M^2\psi_y, \quad (4.30)$$

$$\theta_{yy} = \frac{Br\left(\frac{\eta}{\mu}\right)\psi_{yy}^2}{(1+Rd)(1+We^2(1-e^2)(\psi_{yy})^2)}. \quad (4.31)$$

The transformed boundary conditions are

$$\begin{aligned} \psi = \frac{F}{2}, \quad \psi_y + \beta\psi_{yy} = 0, \quad \theta = 0 \quad \text{at} \quad y = h_1, \\ \psi = -\frac{F}{2}, \quad \psi_y - \beta\psi_{yy} = 0, \quad \theta = 1 \quad \text{at} \quad y = h_2. \end{aligned} \quad (4.32)$$

### 4.3. Solution of the problem

After using binomial for small  $We^2$ , Eqs. (4.29), (4.30) and (4.31), may be simplified.

$$\left[\psi_{yy} + We^2\alpha(\psi_{yy})^3\right]_{yy} - M^2\psi_{yy} = 0, \quad (4.33)$$

$$p_x = \psi_{yyy} + \left[We^2\alpha(\psi_{yy})^3\right]_y - M^2\psi_y = 0, \quad (4.34)$$

$$\theta_{yy} = \left[ \frac{Br \left( \frac{\eta}{\mu} \right) \psi_{yy}^2}{(1+Rd)(1+We^2(1-e^2)(\psi_{yy})^2)} \right], \quad (4.35)$$

$$\text{where } \alpha = \frac{(e^2-1)\eta}{(\eta+\mu)},$$

Since Eqs. (4.33) -(4.35) are highly nonlinear which are difficult to solve them analytically. So, using the regular perturbation method, approximate results are achieved.

For perturbation solution, we express  $\psi, p_x$  and  $\theta$  as

$$\begin{aligned} \psi &= \psi_0 + We^2 \psi_1, \\ p_x &= p_{0x} + We^2 p_{1x}, \\ \theta &= \theta_0 + We^2 \theta_1. \end{aligned} \quad (4.36)$$

Invoking Eq. (4.36) in Eqs. (4.33) -(4.35) and competing the same exponents of  $We^2$ , we have the subsequent systems.

#### 0<sup>th</sup> -order system

$$\psi_{0yyyy} = M^2 \psi_{0yy}, \quad (4.37)$$

$$p_{0x} = \psi_{0yyy} - M^2 \psi_{0y}, \quad (4.38)$$

$$\theta_{0yy} = \frac{\eta Br}{\mu(1+Rd)} \psi_{0yy}^2, \quad (4.39)$$

$$\begin{aligned} \psi_0 &= \frac{F}{2}, & \psi_{1y} + \beta \psi_{1yy} &= 0, & \theta_0 &= 0 & \text{at } y &= h_1, \\ \psi_0 &= -\frac{F}{2}, & \psi_{1y} - \beta \psi_{1yy} &= 0, & \theta_0 &= 1 & \text{at } y &= h_2. \end{aligned} \quad (4.40)$$

#### 1<sup>st</sup> -order system

$$\psi_{1yyyy} = -\alpha [(\psi_{0yy}^2)^3] + M^2 \psi_{1yy}, \quad (4.41)$$

$$p_{1x} = \psi_{1yyy} + \alpha [(\psi_{0yy}^2)^3]_y - M^2 \psi_{1y}, \quad (4.42)$$

$$\theta_{1yy} = \left[ \frac{Br \left( \frac{\eta}{\mu} \right) \psi_{1yy}^2}{(1+Rd)(1-e^2)(\psi_{0yy})^2} \right], \quad (4.43)$$

$$\begin{aligned} \psi_1 &= \frac{F}{2}, & \psi_{1y} + \beta \psi_{1yy} &= 0, & \theta_1 &= 0 & \text{at } y &= h_1, \\ \psi_1 &= -\frac{F}{2}, & \psi_{1y} - \beta \psi_{1yy} &= 0, & \theta_1 &= 1 & \text{at } y &= h_2. \end{aligned} \quad (4.44)$$

After resolving the aforementioned systems, we arrive at the formulas for the stream function, axial velocity, pressure, and temperature.

$$\psi = \frac{1}{8M^2} e^{-3My} \left( \begin{aligned} &8e^{2My} M (B_3 e^{My} M - C_2 We^2 + e^{My} (C_1 e^{My} We^2 + C_4 M We^2 + B_4 My)) \\ &+ 3B_2^3 M We^2 \alpha - 3B_1^3 e^{6My} M We^2 \alpha + 8B_2 e^{2My} + 8B_1 e^{4My} - \\ &6B_1^2 B_2 e^{4My} M We^2 (-3 + 2My) \alpha - 6B_1 B_2^2 e^{2My} M We^2 (3 + 2My) \alpha \end{aligned} \right), \quad (4.45)$$

$$u = \frac{1}{8M} e^{-3My} \left( \begin{aligned} &8e^{2My} M (B_4 e^{My} + (C_2 + C_1 e^{2My}) We^2) - 9B_2^3 M We^2 \alpha \\ &- 9B_1^3 e^{6My} M We^2 \alpha + 8B_1 e^{4My} + 6B_1 B_2^2 e^{2My} M We^2 (1 + 2My) \alpha \\ &- 2B_2 e^{2My} (4 + 3B_1^2 e^{2My} M We^2 (-1 + 2My) \alpha) \end{aligned} \right), \quad (4.46)$$

$$\begin{aligned} p_x &= B_4 M^2 (h_1 - h_2) \\ &+ \frac{1}{8} We^2 \left( \begin{aligned} &8C_4 h_1 M^2 - 8C_4 h_2 M^2 + 9B_1^3 e^{3h_2 M} (1 - 3M) \alpha + 9B_1^3 e^{3h_1 M} (3M - 1) \alpha \\ &- 9B_2^3 e^{-3h_1 M} (3M + 1) \alpha + 9B_2^3 e^{-3h_2 M} (3M + 1) \alpha \\ &+ 2e^{h_1 M} (-4C_1 (M - 1) + 3B_1^2 B_2 (1 + M + 2h_1 (M - 1) M) \alpha) \\ &- 2e^{h_2 M} (-4C_1 (M - 1) + 3B_1^2 B_2 (1 + M + 2h_2 (M - 1) M) \alpha) \\ &- 2e^{-h_1 M} (-4C_2 (M + 1) + 3B_1 B_2^2 (-1 + M - 2h_1 M (M + 1)) \alpha) \\ &+ 2e^{-h_2 M} (-4C_2 (M + 1) + 3B_1 B_2^2 (-1 + M - 2h_2 M (M + 1)) \alpha) \end{aligned} \right), \end{aligned} \quad (4.47)$$

$$\begin{aligned}
\theta = & B_5 + C_3 We^2 + B_6 y + C_6 We^2 y - \frac{ABr(B_2^2 e^{-2My} + B_1^2 e^{2My} + 4B_1 B_2 M^2 y^2)}{4M(M + M \text{Pr} Rd)} \\
& + \frac{1}{8M(M + M \text{Pr} Rd)} ABrWe^2 \\
& \left( \begin{aligned} & B_2^3 e^{-3My} \alpha + B_1^3 e^{3My} \alpha - 2e^{My} \left( 4C_1 + B_1 \left( 4(e^2 - 1)M^2 + 15B_1 B_2 \alpha \right) \right) \\ & - 2e^{-My} \left( 4C_2 + B_2 \left( 4(e^2 - 1)M^2 + 15B_1 B_2 \alpha \right) \right) \end{aligned} \right)
\end{aligned} \tag{4.48}$$

At a fixed location  $\widehat{X}$ , the time averaged flow is defined as

$$Q = \int_0^T Q dt . \tag{4.49}$$

We discover

$$Q = q + a_1 c \sin \left[ \frac{2\pi}{\lambda} (\widehat{X} - ct) + \phi \right] + a_2 c \sin \left[ \frac{2\pi}{\lambda} (\widehat{X} - ct) \right],$$

where  $q = \int_{H_1}^{H_2} \bar{u}(\bar{x}, \bar{y}) d\bar{y}$  represents the dimensional volume flow rate in the wave frame.

By the meanings of dimensionless mean flows  $\Theta$  in the wave frame and  $F$  in the laboratory frame are described as

$$F = \frac{Q}{cd}, \quad \Theta = \frac{q}{cd}.$$

We find that

$$F(x, t) = a \sin 2\pi(x - t) + b \sin [\phi + 2\pi(x - t)] + \Theta,$$

$$\text{In which } F = \int_{h_1}^{h_2} u dy .$$

The usual increase in  $\Delta p$  over one wavelength period is given by

$$\Delta p = \int_0^1 \int_0^1 \left( \frac{dp}{dx} \right)_{y=0} dx dt . \tag{4.50}$$

The constant appearing in above equations are given in appendix.

## 4.4 Discussion of the findings

This section uses graphical findings to show how different variables affect velocity, pressure rise, temperature, and streamlines. The representation for  $\Delta p$  contains the integration of  $dp/dx$  which is difficult to integrate analytically. Therefore, the integral occurring in Eq. (4.50) has been estimated numerically utilizing MATHEMATICA through composite Simpson's rule. During this investigation, In order to facilitate computations, the following standard parametric values are used:  $\beta = 0.01$ ,  $M = 1$ ,  $t = 0.2$ ,  $a = 0.3$ ,  $\Theta = 1.75$ ,  $\mu = 0.3$ ,  $B_r = 2$ ,  $Rd = 0.2$ ,  $\eta = 0.2$ ,  $e = 0.2$ ,  $k = 0.2$ ,  $x = 0.4$ ,  $\phi = \pi/4$  and  $b = 0.2$ .

Figure 4.2 (a-d) is intended to examine and discuss the effects of substantial parameters on the momentum profile.  $u$ . Figure 4.2a is displayed to observe the Hartmann parameter impressions ( $M$ ) on momentum transfer. It is shown that as the value of ( $M$ ) increases, the velocity of the liquid decreases. Physically, increasing the strength of a magnetic field enhances the Lorentz force, causing fluid materials to encounter more resistance, reducing liquid velocity. This perception has a significant impact in the medication field, where the local energy augments in the existence of a structured external magnetic field, which aids in the elimination of tumor cells. Figure 4.2b depicts the effect of the slip parameter ( $\beta$ ) on liquid velocity. This graph shows that increasing behavior in slip parameter cause a decrease the liquid velocity in the center of channel. Figure 4.2c portrays the behavior in momentum profile for various values of ( $We$ ). The liquid velocity decreases as ( $We$ ) increases. Figure 4.2d examines the deviations in the momentum profile for different values of ( $e$ ). Figure 4.2d shows that higher values of ( $e$ ) increase liquid velocity.

The influences of governing variable quantities on temperature are available in Figure 4.3(a-c). In Figure 4.3a we depict the effects of ( $Br$ ) on temperature profile. It is notable that temperature improves with enhancing amounts of ( $Br$ ). Physically, the ( $Br$ ) boosts the conflict to the flow for the reason that of its shear strength, which in turn leads

to an improvement in intensity due to the viscous dissipation influence. So, rises the fluid temperature. Figure 4.3b explains the impact of  $(Rd)$  on temperature distribution. The graph signifies that liquid temperature reduces for boosting quantities of the parameter  $(Rd)$ . Figure 4.3c demonstrates the variation of the  $(We)$  on the fluid temperature. We can examine from this graph; fluid temperature enhances for greater values of the  $(We)$ . Figure 4.4(a-d) exhibits a graph of the  $\Delta p$  vs. the change in time-average flux  $Q$ . Figure 4.4(a-d) demonstrate pumping zones such as peristaltic injecting ( $Q > 0, \Delta p > 0$ ) enhanced driving ( $Q > 0, \Delta p < 0$ ), and backward injecting ( $Q < 0, \Delta p > 0$ ). Figure 4.4a is portrayed to perceive the influences of  $(M)$  on pressure gradient profile  $\Delta p$ . It is discovered since this diagram that the injecting rate shows a decrement with increasing  $(M)$  in the enhanced driving region, whereas the inverse trend is scrutinized in the backward driving zone. The graph illustrated in Figure 4.4b displays the deviation of rise in pressure with different values of slip parameter. From this graph, we perceive that the injecting rate is increased with slip parameter in the augmented driving segment and reduces in the backward driving zone. The influence of  $(e)$  on  $\Delta p$  is displayed in Figure 4.4c. This graph demonstrates greater values of  $(e)$  increasing the  $\Delta p$  in the backward driving zone. Figure 4.4d is graphed to depict the deviation in pressure rise for various values of  $We$ . We can note that pressure in the retrograde pumping portion is reduced with the changing behavior of  $We$ .

The process of trapping, in which a bolus is moved along a peristaltic movement at the speed of the wave and is pushed forward, is one of the most exciting aspects of fluid transportation. Figure 4.5 produces the variation of  $(M)$  on  $\psi$ . It can be seen from this Figure that an improvement in  $(M)$  results in a decrease in the trapping bolus. The Lorentz forces, which serve as a retarding force, are partially responsible for this decline in the size of the bolus. The effect of the flow average flow  $Q$  on the streamlines is presented in Figure 4.6 and examine that the trapped bolus is increased in magnitude as  $Q$  improves and more trapped bolus appears with rising values  $Q$ . Figure 4.7 illustrates

the difference in  $(We)$  on  $\psi$ . The plots depict that when  $(We)$  increases then the confining bolus also increases.

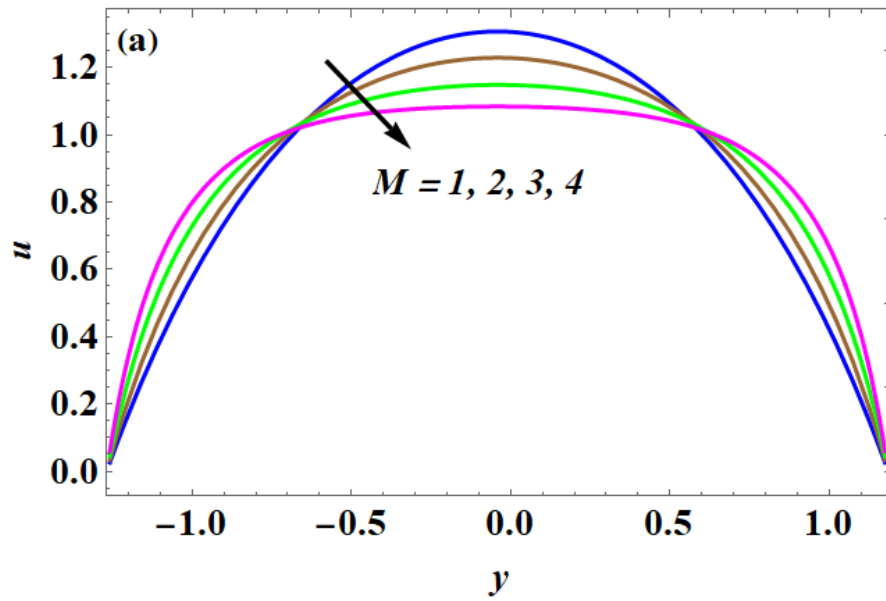


Figure 4.2(a): Effects of  $M$  on axial velocity.

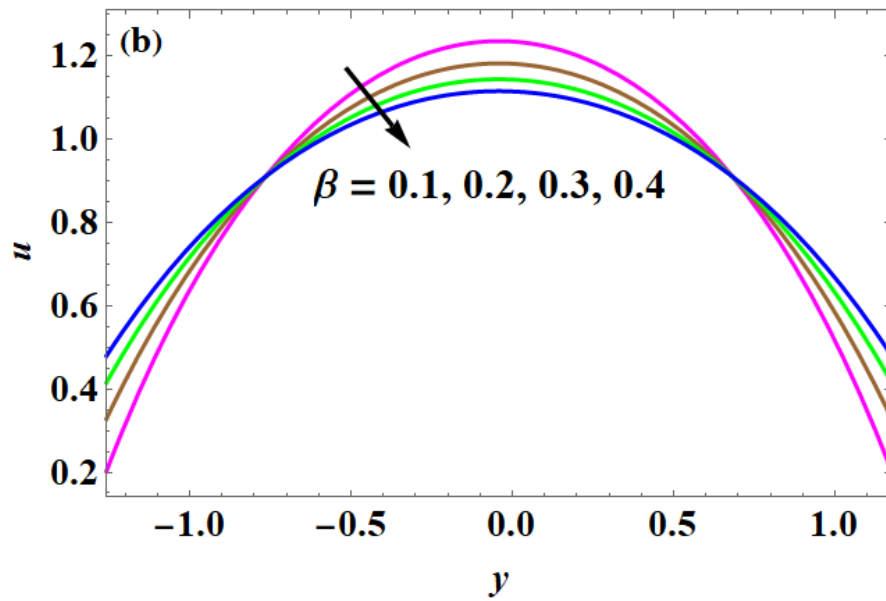


Figure 4.2(b): Effects of  $\beta$  on axial velocity.



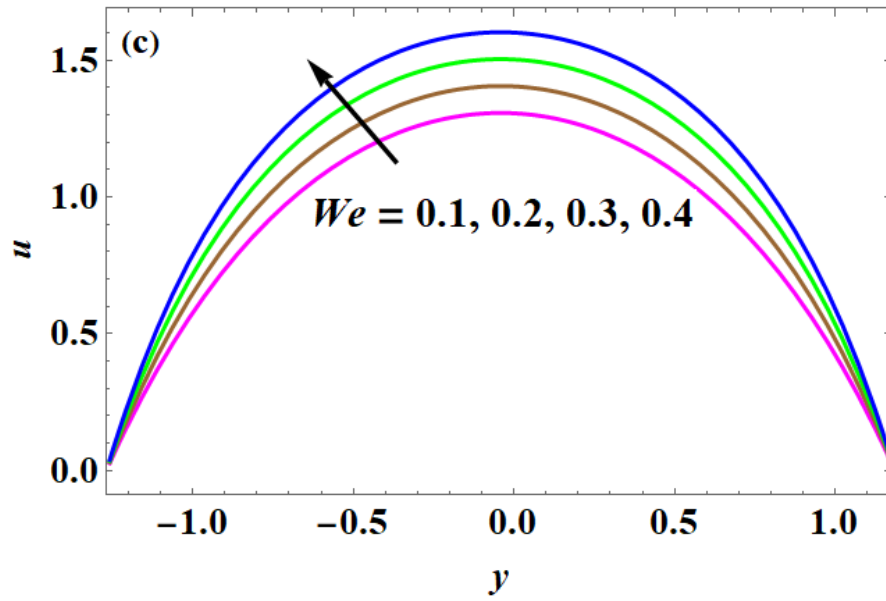


Figure 4.2(c): Effects of  $We$  on axial velocity.

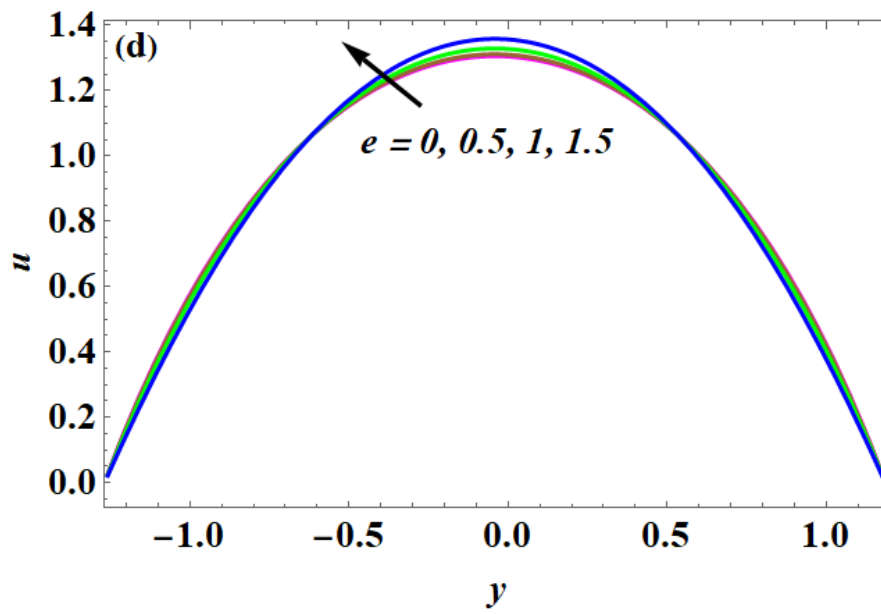


Figure 4.2(d): Effects of  $e$  on axial velocity

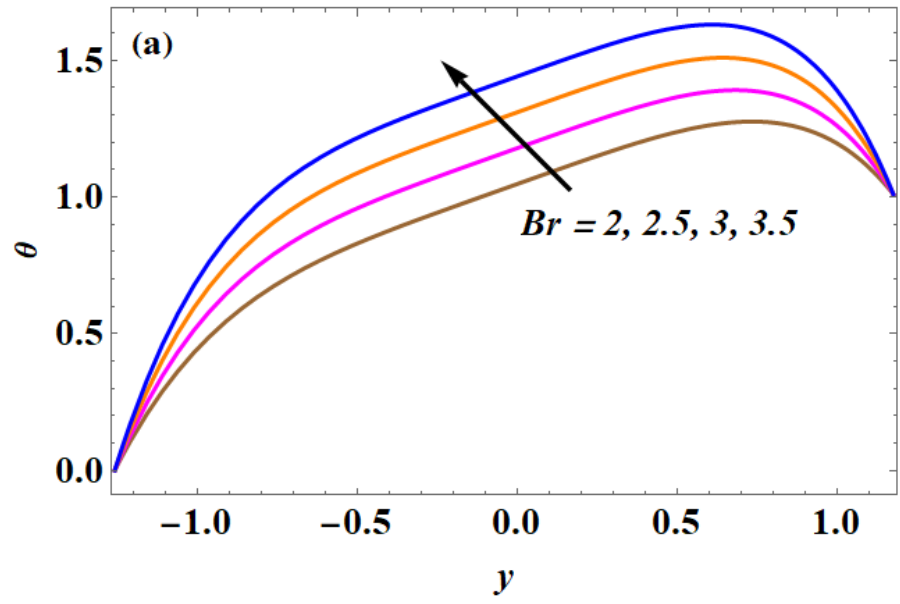


Figure 4.3(a): Effects of  $Br$  on temperature.

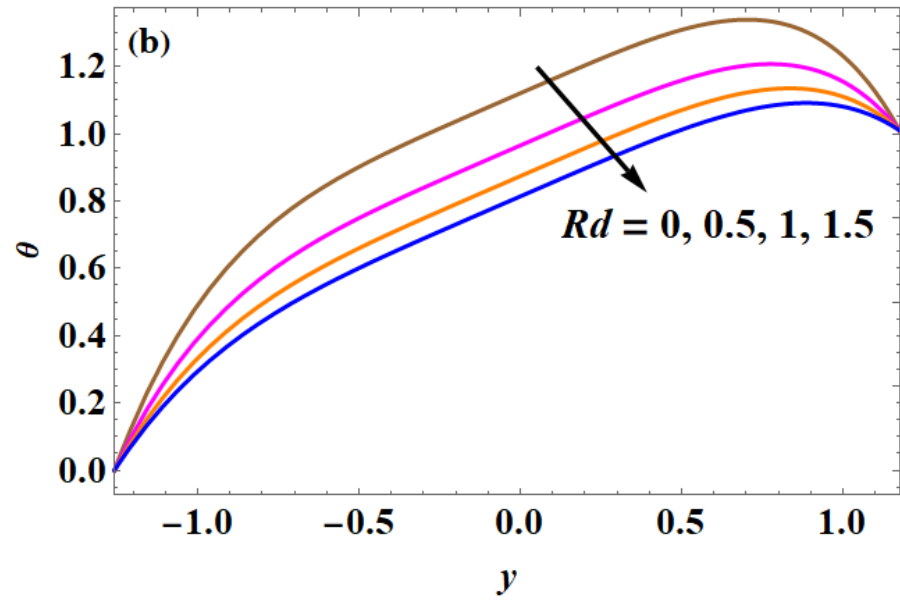


Figure 4.3(b): Effects of  $Rd$  on temperature.

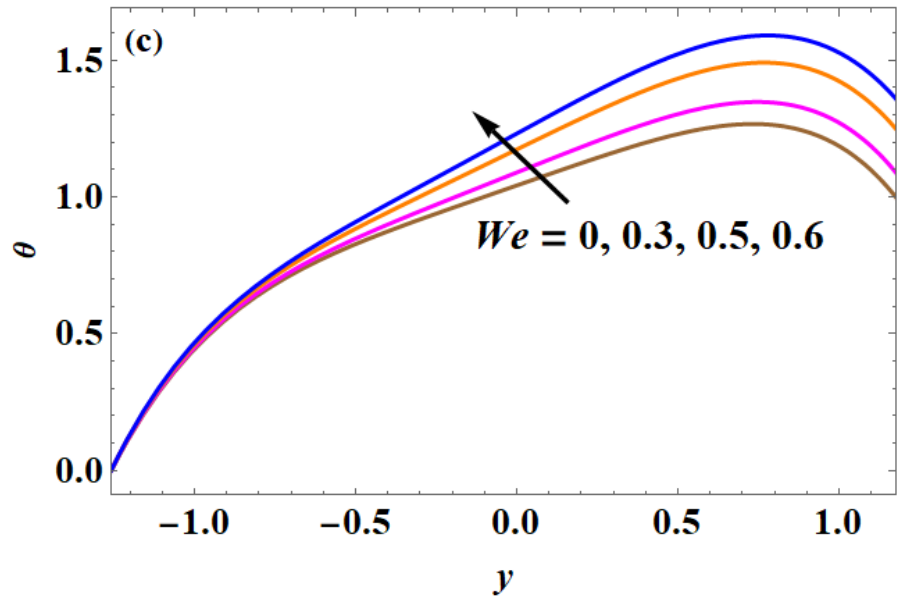


Figure 4.3(c): Effects of  $We$  on temperature.

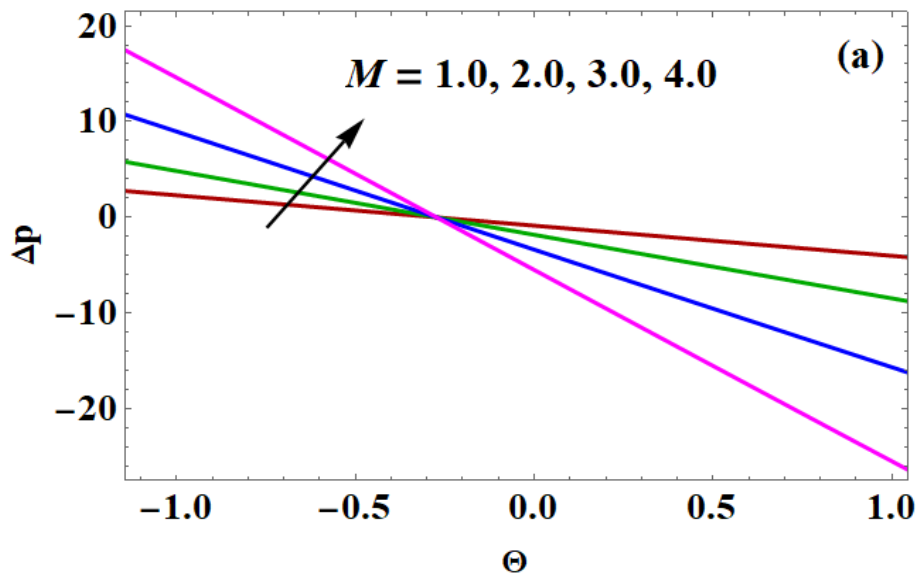


Figure 4.4(a): Effects of  $M$  on pressure.

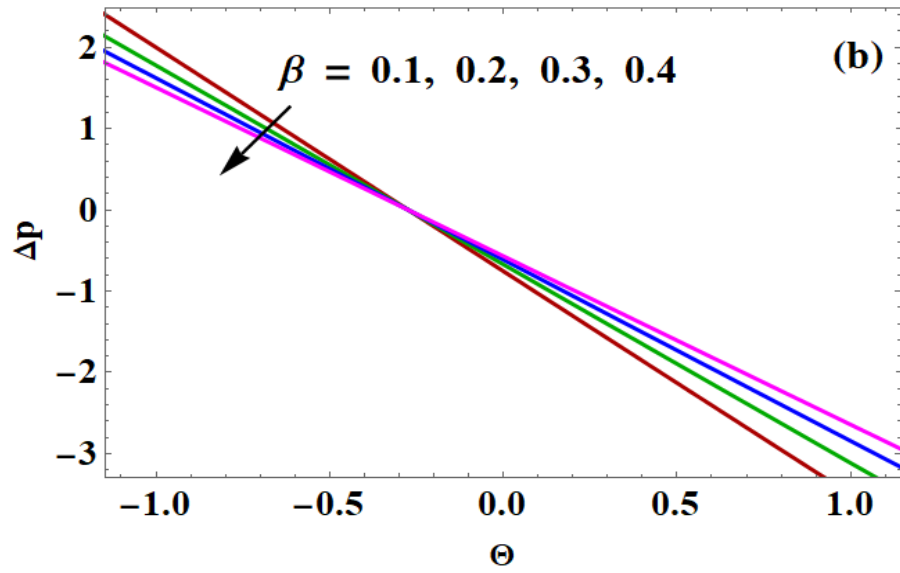


Figure 4.4(b): Effects of  $\beta$  on pressure.

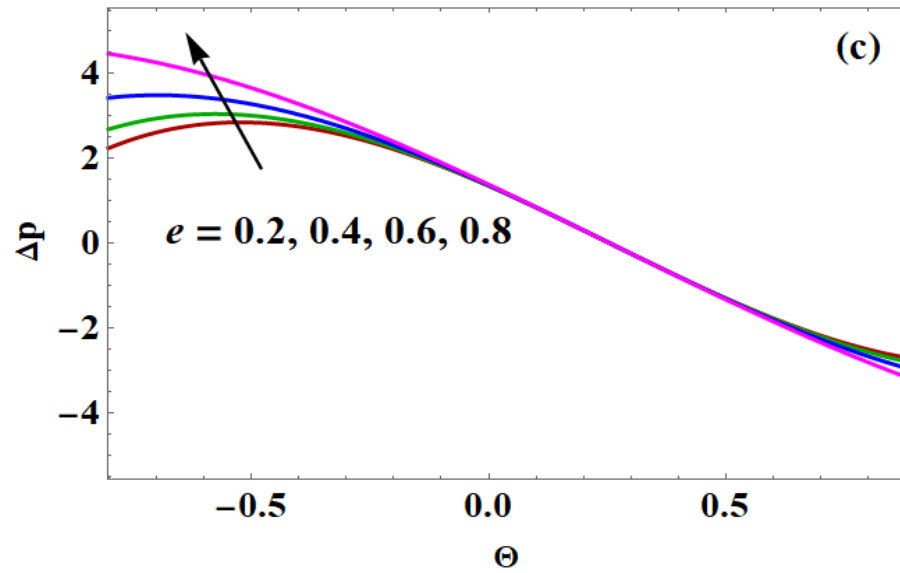


Figure 4.4(c): Effects of  $e$  on pressure.

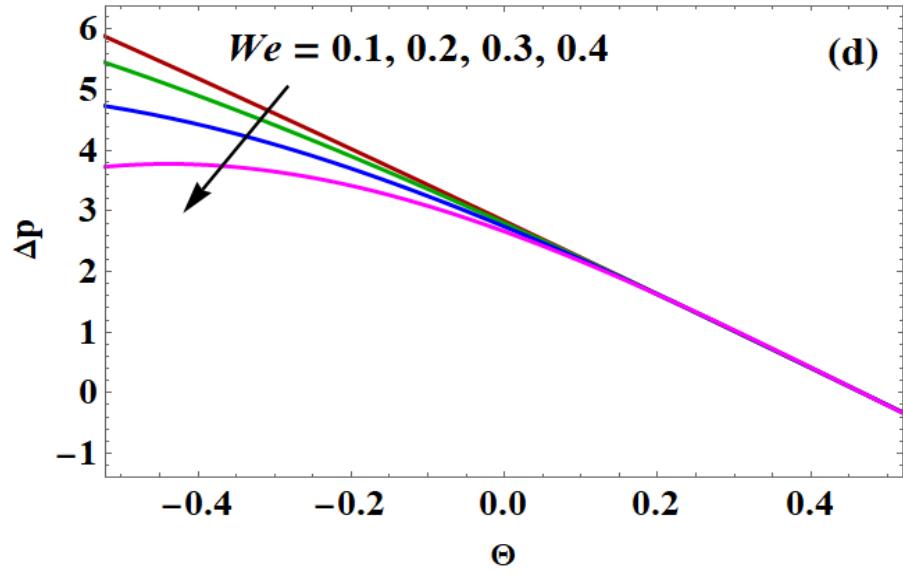


Figure 4.4(d): Effects of  $We$  on pressure.

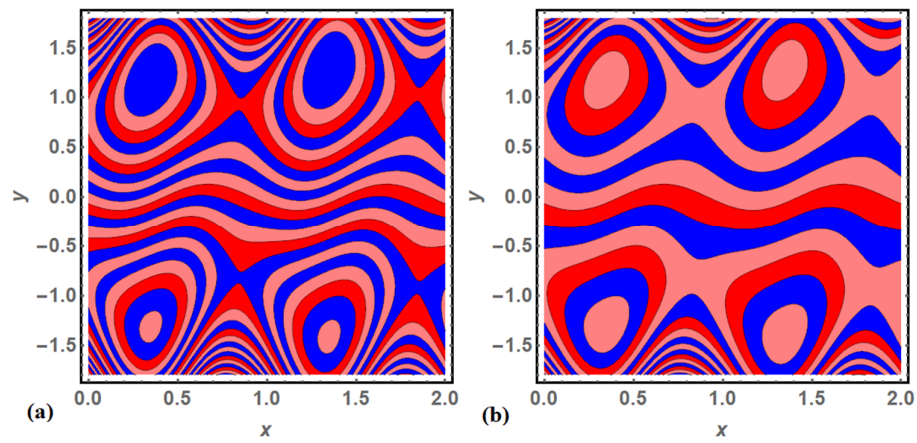


Figure 4.5: Streamlines for various values of (a)  $M = 1$  (b)  $M = 2$ .

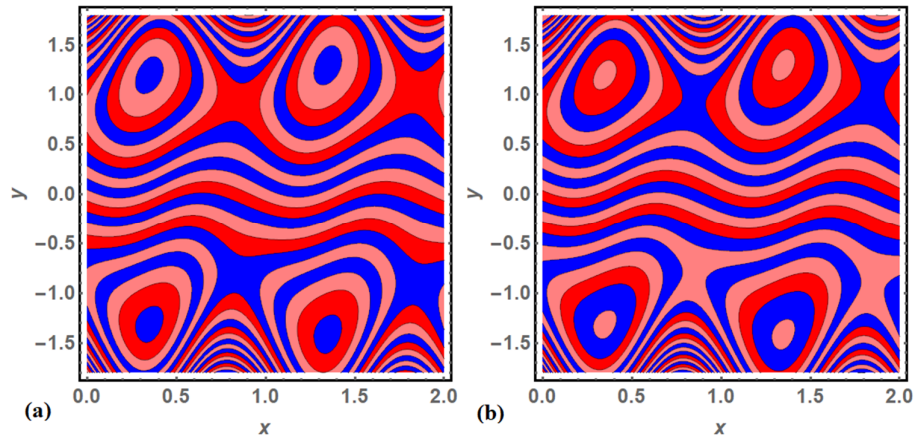


Figure 4.6: Streamlines for various values of (a)  $Q = 1.2$ , (b)  $Q = 1.4$ .

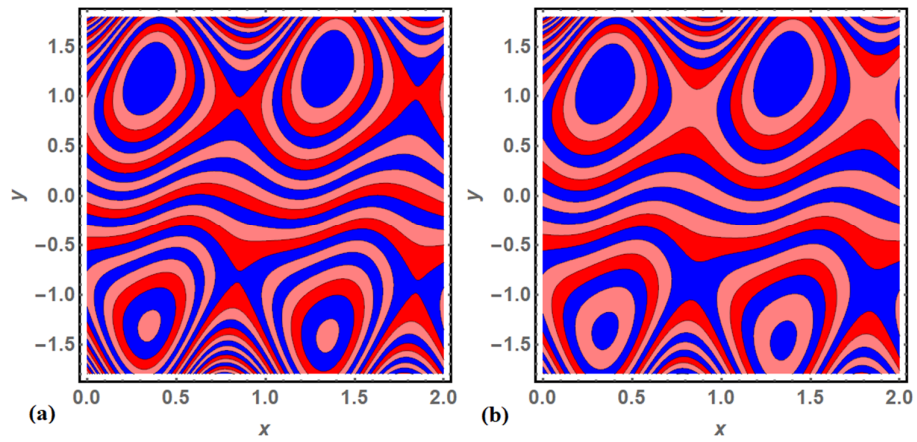


Figure 4.7: Streamlines for various values of (a)  $We = 0$ , (b)  $We = 0.2$ .

## CHAPTER 5

### CONCLUSION AND FUTURE WORK

#### 5.1 Conclusion

In this thesis, we studied, the peristaltic transport of Johnson-Segalman fluid in a tapered asymmetric channel, with viscous dissipation and effects of thermal radiation. We built a mathematical model. The tapered asymmetric channel is created by varying the amplitudes and phase of peristaltic wave trains over nonuniform walls. Approximations with a long wavelength and low Reynolds number have been used. The expressions for stream function, axial velocity, temperature profile and pressure gradient were computed using a regular perturbation approach. It is addressed how the fluid's rheological characteristics interact with peristaltic transport. The variations of dissimilar flow parameters under the change of the present flow factors are well portrayed via graphic representations. The main observations are:

- The pressure falls with changing behavior of  $We$  in retrograde pumping portion however pressure rise improves in this region with improving magnetic number.
- An augmentation in the quantities of radiation parameter causes a decline in the liquid temperature.
- The number of trapped bolus diminishes with greater values of magnetic number.
- It has been discovered that as  $a$  and  $e$  increase, the average rise in pressure  $\Delta p$  increases, whereas  $k, \phi$  and  $\eta$  decrease.
- It was also discovered that with rise in  $\eta$ ,  $k$ , and  $Q$ , the momentum transport in axial direction is decreased.

## **5.2 Future work**

For further work following may be considered

- The Johnson-Segalman model can be studied with different geometries with different boundary conditions.
- Entropy generation also can be discussed
- Chemical reaction



## APPENDIX

$$B_1 = -\frac{FM^2}{e^{h_1 M} (2 + (h_1 - h_2)M(-1 + M\beta)) + e^{h_2 M} (-2 - (h_1 - h_2)M(1 + M\beta))},$$

$$B_2 = \frac{e^{M(h_1 + h_2)} FM^2}{e^{Mh_1} (2 + M(-1 + M\beta)(h_1 - h_2)) + e^{Mh_2} (-2 + M(1 + M\beta)(-h_1 + h_2))},$$

$$B_3 = \frac{FM(e^{Mh_1}(-1 + M\beta) - e^{Mh_2}(1 + M\beta))(h_1 + h_2)}{2e^{Mh_1} (2 + M(-1 + M\beta)(h_1 - h_2)) + 2e^{Mh_2} (-2 + M(1 + M\beta)(-h_1 + h_2))},$$

$$B_4 = \frac{FM(e^{Mh_1}(1 - M\beta) + e^{Mh_2}(1 + M\beta))}{e^{Mh_1} (2 + M(-1 + M\beta)(h_1 - h_2)) + e^{Mh_2} (-2 + M(1 + M\beta)(-h_1 + h_2))},$$

$$C_1 = \frac{\left( \begin{aligned} &e^{-3M(h_1 + h_2)}(-8e^{3M(h_1 + h_2)}FM^2(e^{Mh_1}(-1 + M\beta) + e^{Mh_2}(1 + M\beta)) + \alpha B_2^2(2(e^{Mh_1} - e^{Mh_2})) \\ &(-e^{M(2h_1 + h_2)}M\beta - e^{M(h_1 + 2h_2)}M\beta + e^{3Mh_1}(-1 + 4M\beta) + e^{3Mh_2}(1 + 4M\beta)) - 3e^{M(h_1 + h_2)} \\ &M(e^{2Mh_2}(1 + 2M\beta - 3M^2\beta^2) + e^{2Mh_1}(-1 + 2M\beta + 3M^2\beta^2))h_1 + 3e^{M(h_1 + h_2)} \\ &M(e^{2Mh_2}(1 + 2M\beta - 3M^2\beta^2) + e^{2Mh_1}(-1 + 2M\beta + 3M^2\beta^2))h_2 \\ &+ e^{3M(h_1 + h_2)}\alpha B_1^3(2(e^{Mh_1} - e^{Mh_2})) \left( \begin{aligned} &e^{M(2h_1 + h_2)}M\beta + e^{M(h_1 + 2h_2)}M\beta + \\ &e^{3Mh_1}(-2 + 5M\beta) + e^{3Mh_2}(2 + 5M\beta) \end{aligned} \right) \\ &+ 3M(e^{4Mh_1}(1 - 4M\beta + 3M^2\beta^2) - e^{4Mh_2}(1 + 4M\beta + 3M^2\beta^2))h_1 \\ &- 3M(e^{4Mh_1}(1 - 4M\beta + 3M^2\beta^2) - e^{4Mh_2}(1 + 4M\beta + 3M^2\beta^2))h_2 \\ &- 12e^{2M(h_1 + h_2)}\alpha B_1 B_2^2(e^{2Mh_1} + e^{2Mh_2} - 2e^{M(h_1 + h_2)} - 2e^{2Mh_1}M\beta + 2e^{2Mh_2}M\beta \\ &+ e^{M(h_1 + h_2)}M^2(-1 + M^2\beta^2)h_1^2 - 4e^{M(h_1 + h_2)}M^2\beta h_2 + e^{M(h_1 + h_2)}M^2(-1 + M^2\beta^2)h_2^2 - 2e^{M(h_1 + h_2)} \\ &M^2h_1(-2\beta + (-1 + M^2\beta^2)h_2) + 6\alpha B_1^2 B_2(2e^{5Mh_1 + 3Mh_2}M^2(-1 + M\beta)^2 h_1^2 + e^{3M(h_1 + h_2)} \\ &Mh_1(4e^{M(h_1 + h_2)} - e^{2Mh_1}(7 - 8M\beta + M^2\beta^2) + e^{2Mh_2}(3 + 4M\beta + M^2\beta^2) - 2M \\ &(e^{2Mh_1}(-1 + M\beta)^2 + e^{2Mh_2}(1 + M\beta)^2)h_2) + e^{3M(h_1 + h_2)}(-16e^{M(h_1 + h_2)} + e^{2Mh_1}(8 - 6M\beta) + e^{2Mh_2}(8 + 6M\beta) \\ &+ M(4e^{M(h_1 + h_2)} + e^{2Mh_1}(3 - 4M\beta + M^2\beta^2) - e^{2Mh_2}(7 + 8M\beta + M^2\beta^2))h_2 + 2e^{2Mh_2}M^2(1 + M\beta)^2 h_2^2) \end{aligned} \right) \right)}{8(e^{Mh_1}(-1 + M\beta) + e^{Mh_2}(1 + M\beta))(2(e^{Mh_1} - e^{Mh_2})) + M(e^{Mh_1}(-1 + M\beta) - e^{Mh_2}(1 + M\beta))h_1 + M(e^{Mh_1}(1 - M\beta) + e^{Mh_2}(1 + M\beta))h_2)},$$

$$C_2 = \frac{\left( \begin{aligned} &e^{-2M(h_1+h_2)}(-8e^{3M(h_1+h_2)}FM^2(e^{Mh_1}(-1+M\beta)+e^{Mh_2}(1+M\beta))) \\ &+e^{3M(h_1+h_2)}\alpha B_1^3(-2(e^{Mh_1}-e^{Mh_2}))(-e^{M(2h_1+h_2)}M\beta-e^{M(h_1+2h_2)}M\beta) \\ &+e^{3Mh_1}(-1+4M\beta)+e^{3Mh_2}(1+4M\beta))+3e^{M(h_1+h_2)}M(e^{2Mh_2}(1+2M\beta-3M^2\beta^2)) \\ &+e^{2Mh_1}(-1+2M\beta+3M^2\beta^2)h_1-3e^{M(h_1+h_2)}M(e^{2Mh_2}(1+2M\beta-3M^2\beta^2)+e^{2Mh_1}(-1+2M\beta+3M^2\beta^2))h_2 \\ &+\alpha B_2^3(-2(e^{Mh_1}-e^{Mh_2}))\left(e^{M(2h_1+h_2)}M\beta+e^{M(h_1+2h_2)}M\beta+e^{3Mh_1}(-2+5M\beta)+e^{3Mh_2}(2+5M\beta)\right) \\ &-3M\left(e^{4Mh_1}(1-4M\beta+3M^2\beta^2)-e^{4Mh_2}(1+4M\beta+3M^2\beta^2)\right)h_1+3M\left(e^{4Mh_1}(1-4M\beta+3M^2\beta^2)-e^{4Mh_2}(1+4M\beta+3M^2\beta^2)\right)h_2 \\ &+12e^{3M(h_1+h_2)}\alpha B_1^2B_2(e^{2Mh_1}+e^{2Mh_2}-2e^{M(h_1+h_2)}-2e^{2Mh_1}M\beta+2e^{2Mh_2}M\beta+e^{M(h_1+h_2)}M^2(-1+M^2\beta^2))h_1^2 \\ &-4e^{M(h_1+h_2)}M^2\beta h_2+e^{M(h_1+h_2)}M^2(-1+M^2\beta^2)h_2^2-2e^{M(h_1+h_2)}M^2h_1(-2\beta+(-1+M^2\beta^2)h_2) \\ &+6\alpha B_1B_2^2(-2e^{2M(h_1+2h_2)}M^2(1+M\beta)^2h_1^2+e^{2M(h_1+h_2)}Mh_1(4e^{M(h_1+h_2)}+e^{2Mh_1}(3-4M\beta+M^2\beta^2)) \\ &-e^{2Mh_2}(7+8M\beta+M^2\beta^2)+2M(e^{2Mh_1}(-1+M\beta)^2+e^{2Mh_2}(1+M\beta)^2)h_2)+e^{2M(h_1+h_2)} \\ &\left(16e^{M(h_1+h_2)}-2e^{2Mh_2}(4+3M\beta)+e^{2Mh_1}(-8+6M\beta)-M\begin{pmatrix} -4e^{M(h_1+h_2)}+e^{2Mh_1}(7-8M\beta+M^2\beta^2) \\ -e^{2Mh_2}(3+4M\beta+M^2\beta^2) \end{pmatrix}h_2-2e^{2Mh_1}M^2(-1+M\beta)^2h_2^2\right) \end{aligned} \right) \\ \left( 8(e^{Mh_1}(-1+M\beta)+e^{Mh_2}(1+M\beta))(-2e^{Mh_1}+2e^{Mh_2}+M(e^{Mh_1}(1-M\beta)+e^{Mh_2}(1+M\beta)))h_1+M(e^{Mh_1}(-1+M\beta)-e^{Mh_2}(1+M\beta))h_2 \right), \end{aligned}$$

$$C_3 = \frac{\left( \begin{aligned} &e^{-3M(h_1+h_2)}(2e^{3M(h_1+h_2)}FM^3(-e^{2Mh_1}(-1+M\beta)^2+e^{2Mh_2}(1+M\beta)^2)(h_1+h_2) \\ &-e^{3M(h_1+h_2)}\alpha B_1^3((-e^{Mh_1}+e^{Mh_2})(e^{Mh_1}+e^{Mh_2})^2(-4e^{M(h_1+h_2)}M\beta+e^{2Mh_1}(-1+4M\beta)+e^{2Mh_2}(1+4M\beta))) \\ &+e^{Mh_1}M(e^{4Mh_1}(-3+9M\beta)+e^{2M(h_1+h_2)}(2+2M\beta-4M^2\beta^2)+e^{4Mh_2}(1+5M\beta+4M^2\beta^2))h_1 \\ &+e^{Mh_2}M(-3e^{4Mh_2}(1+3M\beta)-2e^{2M(h_1+h_2)}(-1+M\beta+2M^2\beta^2)+e^{4Mh_1}(1-5M\beta+4M^2\beta^2))h_2 \\ &+\alpha B_2^3((e^{Mh_1}-e^{Mh_2})(e^{Mh_1}+e^{Mh_2})^2(-4e^{M(h_1+h_2)}M\beta+e^{2Mh_1}(-1+4M\beta)+e^{2Mh_2}(1+4M\beta))) \\ &+e^{Mh_1}M(-3e^{4Mh_2}(1+3M\beta)-2e^{2M(h_1+h_2)}(-1+M\beta+2M^2\beta^2)+e^{4Mh_1}(1-5M\beta+4M^2\beta^2))h_1 \\ &+e^{Mh_2}M(e^{4Mh_1}(-3+9M\beta)+e^{2M(h_1+h_2)}(2+2M\beta-4M^2\beta^2)+e^{4Mh_2}(1+5M\beta+4M^2\beta^2))h_2 \\ &-6\alpha B_1^2B_2(e^{3M(h_1+h_2)}(-e^{2Mh_1}+e^{2Mh_2}))(e^{Mh_1}(-1+2M\beta)+e^{Mh_2}(1+2M\beta)) \\ &+2e^{5Mh_1+4Mh_2}M^2(-1+M\beta)h_1^2+e^{4Mh_1+3Mh_2}M(-2e^{M(h_1+h_2)}+e^{2Mh_2}(1-5M\beta-2M^2\beta^2)) \\ &+e^{2Mh_1}(1-3M\beta+2M^2\beta^2)h_2-2e^{4Mh_1+5Mh_2}M^2(1+M\beta)h_2^2+e^{3Mh_1+4Mh_2}Mh_1(-2e^{M(h_1+h_2)}+e^{2Mh_1}(1+5M\beta-2M^2\beta^2)) \\ &+e^{2Mh_2}(1+3M\beta+2M^2\beta^2)-2e^{Mh_1}M(e^{Mh_1}(-1+M\beta)-e^{Mh_2}(1+M\beta))h_2) \\ &+6e^{2M(h_1+h_2)}\alpha B_1B_2^2((e^{2Mh_1}-e^{2Mh_2})(e^{Mh_1}(-1+2M\beta)+e^{Mh_2}(1+2M\beta))+2e^{M(h_1+2h_2)}M^2(1+M\beta)h_1^2 \\ &+e^{Mh_2}M(-2e^{M(h_1+h_2)}+e^{2Mh_1}(1+5M\beta-2M^2\beta^2)+e^{2Mh_2}(1+3M\beta+2M^2\beta^2))h_2 \\ &-2e^{M(2h_1+h_2)}M^2(-1+M\beta)h_2^2+e^{Mh_1}Mh_1(-2e^{M(h_1+h_2)}+e^{2Mh_2}(1-5M\beta-2M^2\beta^2)) \\ &+e^{2Mh_1}(1-3M\beta+2M^2\beta^2)-2e^{Mh_2}M(e^{Mh_1}(1-M\beta)+e^{Mh_2}(1+M\beta))h_2) \end{aligned} \right) \\ \left( 4M^2(e^{Mh_1}(-1+M\beta)+e^{Mh_2}(1+M\beta))(-2e^{Mh_1}+2e^{Mh_2}+M(e^{Mh_1}(1-M\beta)+e^{Mh_2}(1+M\beta)))h_1+M(e^{Mh_1}(-1+M\beta)-e^{Mh_2}(1+M\beta))h_2 \right), \end{aligned}$$

$$C_4 = \frac{\left( \begin{aligned} & e^{-3M(h_1+h_2)} (-4e^{3M(h_1+h_2)} FM^2 \left( \begin{aligned} & e^{Mh_1} (1-M\beta) + \\ & e^{Mh_2} (1+M\beta) \end{aligned} \right) + e^{3M(h_1+h_2)} (e^{Mh_1} - e^{Mh_2})^2 \\ & \alpha \left( \begin{aligned} & 4e^{M(h_1+h_2)} M\beta + e^{2Mh_1} (-1+4M\beta) \\ & + e^{2Mh_2} (1+4M\beta) \end{aligned} \right) B_1^3 - (e^{Mh_1} - e^{Mh_2})^2 \\ & \alpha \left( \begin{aligned} & 4e^{M(h_1+h_2)} M\beta + e^{2Mh_1} (-1+4M\beta) + \\ & e^{2Mh_2} (1+4M\beta) \end{aligned} \right) B_2^3 + 6e^{3M(h_1+h_2)} \\ & \alpha B_1^2 B_2 \left( \begin{aligned} & -e^{2Mh_1} + e^{2Mh_2} + 2e^{2Mh_1} M\beta + 2e^{2Mh_2} M\beta - 4e^{M(h_1+h_2)} \\ & M\beta + 2e^{M(h_1+h_2)} Mh_1 - 2e^{M(h_1+h_2)} Mh_2 \end{aligned} \right) \\ & -6e^{2M(h_1+h_2)} \alpha B_1 B_2^2 \left( \begin{aligned} & -e^{2Mh_1} + e^{2Mh_2} + 2e^{2Mh_1} M\beta + 2e^{2Mh_2} M\beta \\ & -4e^{M(h_1+h_2)} M\beta + 2e^{M(h_1+h_2)} Mh_1 - 2e^{M(h_1+h_2)} Mh_2 \end{aligned} \right) \end{aligned} \right)}{\left( \begin{aligned} & 4M \left( \begin{aligned} & -2e^{Mh_1} + 2e^{Mh_2} + M(e^{Mh_1} (1-M\beta) + e^{Mh_2} (1+M\beta)) h_1 \\ & + M(e^{Mh_1} (-1+M\beta) - e^{Mh_2} (1+M\beta)) h_2 \end{aligned} \right) \end{aligned} \right)},$$

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# HEAT TRANSFER ANALYSIS OF JOHNSON-SEGALMAN FLUID IN TAPERED ASYMMETRIC CHANNEL

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