

**Thermal performance of hybrid nanofluid in a rotating
vertical channel between two plates**



Thesis Submitted By

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Session (2019-2021)

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Thesis Completion Certificate

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Dedicated to

My beloved parents and respected teachers

Thanks for your love, pray and support.

My supporting brother and caring sisters

Thanks for all your love to me

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Robash Qasim

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Abstract

The main purpose of this thesis is to construct the mathematical model of the fluid flow in a rotating system between two infinitely flat surfaces. In this model one plate is stretchable while the other is penetrable. By using basic fundamental laws, equations of momentum and energy are formulated. Then, these energy and momentum equations are converted into non-linear ordinary differential equations by using similarity variables. These ordinary differential equations are further solved by using the Adomian decomposition method (ADM). The impact of various parameters on temperature and velocity profiles is investigated. The obtained results show the variation of the Nusselt number by increasing the radiation and injection parameters. This thesis is split into five chapters. In chapter 1, a comprehensive review analysis is done to determine gaps that exist, where we can fill them up by developing the modification in fundamental laws and methodology. Chapter 2 is related to the basic concepts of fluid and its properties. Chapter 3 is a review of work done by Ali J Chamkha et al [35] that deals with the flow of hybrid nanofluid between two parallel plates. Chapter 4 is an extension of chapter 3 in which we have developed the channel flow with various effects that improve the thermal conductivity and flow behavior between the channels. In the very last chapter, the conclusion of the entire analysis is presented.

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Nomenclature

u^*, v^*, w^*	Velocity components
T^*	Temperature
P	Pressure
$\bar{\sigma}$	Electrical conductivity
σ^*	Stefan Boltzmann constant
g	Magnitude of acceleration due to gravity
ρ_{hnf}	Hybrid nanofluid effective density
μ_{hnf}	Hybrid nanofluid dynamic viscosity
μ_f	Base fluid's dynamic viscosity
k_{hnf}	Hybrid nanofluid thermal conductivity
k_{hnf}^*	Hybrid nanofluid's mean absorption coefficient
k_f	Base fluid's thermal conductivity
ρ_f	Base fluid's viscosity
ν_f	Kinematic viscosity
$(\rho C_p)_{hnf}$	Hybrid nanofluid heat capacity
$(\rho C_p)_f$	Base fluid's heat capacity
β	Thermal expansion coefficient
Mn	Magnetic parameter
N	Radiation parameter
Ro	Rotation parameter
Re	Reynold number
A	Suction/injection
Ec	Eckert number
Pr	Prandtl number
Gr_m	Mixed convection parameter
Q_o	Heat generation/absorption
Q	Heat source or sink parameter
Gr	Grashaf number
MHD	magneto-hydrodynamic

Chapter1

1. Introduction and literature review

Heat transfer and rotating flow study has huge scope due to its large application in many industries like transportation and engineering. Such techniques are helpful in heat transfer enhancement and nanofluid plays a vital role in heat transfer. The term nanofluid can be expressed as suspension of nanometer sized particle with some base fluid. Water and other lubricant are used as base fluid. Nanoparticles like *Al*, *Ag* and *Cu* are used for the production of nanofluid. Nanofluid was first ever proposed by *Choi*. [1]. He used nanoparticles to increase the thermal conductivity of base fluid. These tiny size particles are mostly of metals, oxide and carbides. Nanofluids are commonly used in many fields like Medical and pharmacy. Due to enormous application nanofluid receives special attention from several bright researchers. *Das*. [2] also examined the flow behavior of nanofluid with alumination. Number of authors [3-10] explained the vital relationship between heat transfer and nanofluid particles.

Magnetohydrodynamic (MHD) is the combination of words magneto-meaning magnetic, hydro-meaning fluid and dynamic- meaning movement. It is the phenomena in which fluid is electrically conducting in the presence of magnetic field. In 1942, Swedish scientist Hannes Alfven et al. [11] introduced the term MHD in his paper and discovered the MHD waves known as Alfven, Which has number of application in astrophysical problems. MHD flow between two parallel plates has importance in many applications such as; MHD generator, pumps, cooling of nuclear reactor. The experimental investigation on MHD flow was carried out by Hartman and Lazarus et al. [12] and they analyzed the influence of effects of uniform magnetic field on the flow of electrically conducting fluid between parallel plates. Later on, Rosson et al. [13] also investigated the flow of electrically conducting fluid over flat plate in the presence of magnetic field. The investigation also found that fluid velocity changes due to this magnetic field.

As nanoparticles in fluid raise the thermal conductivity [1], they are used in magneto hydrodynamic (MHD) flow along with radiation to accumulate its efficiency. Effect of MHD is used by many renowned researchers due to its characteristic of heat transfer. Heat transfer is a process of exchanging thermal energy which takes place through conduction, convection and radiation. Research studies confirm that the heat transformation of nanofluid in rotating surfaces between two parallel plates. According to the Mustafa et al. [14] heat transfer enhancement

significantly depends upon nano-sized particles. The study also found that Nusselt number is increasing function of Prandtl number. Another study made by Alizdin et al. [15] regarding the magneto hydrodynamic micro-polar fluid with in a channel filled with nanofluid under the influence of thermal radiation. Results show that by increasing radiation parameter and volume fraction, Nusselt number also increases. Ellahi et al. [16] studied the flow in a pipe with MHD effects at nanofluid. It was observed that MHD parameters reduce the motion of fluid and when variable viscosities occur velocity is greater than the temperature. Another study on heat transfer between two surfaces and rotating channel was published by Sheikholeslami et al. [17]. The study discussed that the surface heat transfer rate increases the suction/injection parameter and nanofluid volume fraction. The impact of nano-particle magneto hydrodynamic flow in a rotating channel under influence of thermal radiation is explained by some researchers [18-31].

The nonlinear movement of nanoparticles in the fluid is Brownian motion which is obtained from the motion of the molecules of fluid. The nonlinear motion of fluid is due to the position of nanoparticle within the sub-domain of fluid. Thermal equilibrium of fluid is defined by this motion through its temperature. Fluid also remain linear all time because of the Brownian motion. After the botanist Robert Brown, this motion of nanoparticle is named as Brownian motion. In 1905, Albert Einstein defined this Brownian movement in his paper and his paper has made a huge contribution in science.

Currently, researcher use another kind of nanofluid called hybrid nanofluid that is formed by using two or more different material of nanofluid. Hybrid nanofluid is used for further improvement of heat and mass transfer among the surfaces. Chamkha et al. [32] used hybrid nanofluid in their experiment and results show that by using hybrid nanofluid the average Nusselt number increases. Glora et al. [33] also studied the impact of hybrid nanofluid flow in a square porous with heat source/sink. Their study shows that Nusselt number decrease by changing the position of heat source. Further, they explore that as compared to nanofluid, hybrid nanofluid has low average Nusselt number. Tayebi and Chamkha. [34] Proved by their experiments that by using hybrid nanofluid heat transfer rate become more efficient. Recently, analytical technique is introduced to solve the nonlinear problems. Liao et al. [35] introduce this technique in his problem. Results shows that analytical technique has successfully been applied to many nonlinear problems.

Flow in a channel is one of the most significant branch of fluid mechanics where fluid is enclosed between two surfaces no matter both the surfaces are flat or corrugated. Channel is further discuss in two ways i.e., open channel and closed channel. In open channel flow is depending upon

time. Viscosity and inertia have strong effect on open channel flow. Flow that occurs in a closed channel is closed channel flow. In closed channel flow is either Laminar or Turbulent. In Laminar flow velocity of every particle remain constant and during flow layers do not intersect with each other while flow of liquid is irregular in turbulent flow.

Based on above mentioned literature review, entire thesis is set up for rotating channel flow filled by hybrid nanofluid. Chapter 3, discusses the review of published work done by Ali J Chamkha et al [35]. In chapter 4, I have extended the chapter 3 for new effects as: Mixed convection and heat generation/absorption in vertical rotating channel and stretchable surface. Finally, chapter 5 addresses the thorough conclusion of this thesis.

Chapter 2

Elementary concepts of fluid

In this section some essential definition are discussed.

2.1. Fluid mechanics

Branch of mechanics that deals with fluid behavior at rest and motion.

2.2. Fluid

Substance that continuously deform when pressure is applied is called fluid. For example blood, air, honey.

2.2.1. Physical properties

Some fundamental properties are defined below.

2.2.2. Pressure

The force which applied perpendicularly to the surface and cause some effects called pressure. Mathematical form of pressure is;

$$P = \frac{\text{force}}{\text{area}} = \frac{F}{A}$$

2.2.3. Density

When mass is divided by volume of fluid particle it gives density of that object .it is denoted by “ ρ ” and defined as;

$$\rho = \frac{\text{mass}}{\text{volume}}$$

2.2.4. Viscosity

Force which resistance the motion of fluid is known as viscosity. Mathematical form is “ μ ”.

$$\mu = \frac{\text{shear stress}}{\text{rate of deformation}}$$

2.3. Kinds of fluid

2.3.1. Ideal fluid

Fluid which has zero viscosity is ideal fluid.

2.3.2. Real fluid

Fluid that contains viscosity or viscous force is called real fluid. For example, air, honey etc.

2.3.3. Steady flow

Flow that is not time dependent is steady flow. Mathematical form is;

$$\frac{\partial \eta}{\partial t} = 0$$

2.3.4. Unsteady flow

Flow that is time dependent is unsteady flow.

2.3.5. Compressible flow

Flow in which density changes due to stress called compressible flow. For example gases etc.

2.3.6. Incompressible flow

Flow in which density does not change is consider as incompressible flow. Liquids and lubricants are usually incompressible.

2.3.7. Rotational flow

Flow in which fluid particle rotate with some angular velocity is rotational flow.

$$\frac{\partial \eta}{\partial t} = 0$$

2.3.8. Irrotational flow

Flow in which fluid particles does not rotate is irrotational flow.

2.3.9. One dimensional flow

Flow which depends on one co-ordinate and all particles are parallel to certain straight line is known as one dimensional flow.

2.3.10. Two dimensional flow

Flow which depends on two co-ordinates and velocity is parallel to plane is known as two dimensional flow.

2.3.11. Three dimensional flow

Fluid flow which depends on all co-ordinates of space is known as three dimensional flow.

2.3.12. Heat transfer

The phenomena in which heat is transfer from one location to another with the motion of molecule.

2.3.13. Thermal energy

Internal energy kept by a system or objects because of the movement of molecules is called thermal energy.

2.3.14. Magnetohydrodynamics

The study of electrically conducting fluid in the presence of magnetic field is known as MHD.

2.3.15. Thermal conductivity

The process of heat transfer because of internal capability of any material is thermal conductivity.

2.3.16. Nanofluid

Nanofluid is the mixture of nano meter size particles and base fluid. The base fluid may be Newtonians and non-Newtonian. Mathematically we can write it as

$$\lambda = \frac{\alpha}{\delta}$$

Chapter 3

Magneto-hydrodynamic flow and heat transfer of a hybrid nanofluid in a rotating system between two surfaces in the presence of thermal radiation and Joule heating

In this chapter rotating flow of hybrid nanoparticles and heat transfer property is discussed. First we formulate the basic equation of momentum and energy. Resulted PDE's are further transformed in to corresponding ODE's. Then we convert higher order nonlinear ODE's in system of first order equation and applied numerical technique. Result are discussed in detail for each parameter involved in equation.

3.1 Formulation and solution

Consider steady, incompressible flow between two parallel plates. Due to rotation of channel fluid is rotating with velocity Ω . Motion of lower plate is due to velocity $u^* = u_w^* = ax$.

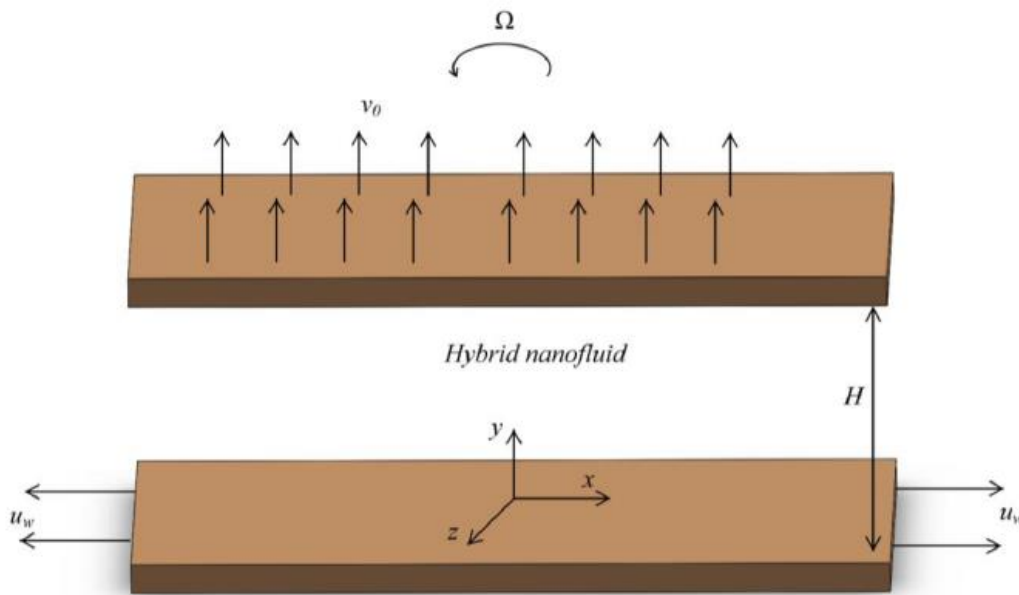


Figure 3.1: Geometry of problem

$$\nabla \cdot \mathbf{V} = 0 \quad (3.1)$$

$$\rho_{hnf} \left(\frac{d\mathbf{V}}{dt} + 2\Omega \times \mathbf{V} + \Omega \times (\Omega \times \mathbf{r}) \right) = \text{div} \boldsymbol{\tau} - \bar{\sigma}_f B_o^2 \mathbf{V}, \quad (3.2)$$

$$(\rho C_p)_{hnf} ((\mathbf{V} \cdot \nabla) T^*) = \boldsymbol{\tau} \cdot \mathbf{L} - \bar{\sigma}_f B_o^2 \mathbf{V}, \quad (3.3)$$

Where \mathbf{V} is the velocity in x, y, z direction.

$$\boldsymbol{\tau} = -\dot{p}\mathbf{l} + \mu A_1, \quad (3.4)$$

μ Represent the viscosity and A_1 is Rivlin-Ericksen tensor,

$$A_1 = \mathbf{L} + \mathbf{L}^t, \quad (3.5)$$

$$\mathbf{L} = \nabla \cdot \mathbf{V}, \quad (3.6)$$

Temperature and velocity are respectively given as

$$T^* = T^*(x, y, z), \quad \mathbf{V} = [u^*(x, y), v^*(x, y), w^*(x, y)],$$

$$\mathbf{L} = \begin{bmatrix} u_x^* & u_y^* & 0 \\ v_x^* & v_y^* & 0 \\ w_x^* & w_y^* & 0 \end{bmatrix} \quad (3.7)$$

Where $u_x^* = \frac{\partial u^*}{\partial x}$, $v_x^* = \frac{\partial v^*}{\partial x}$, $w_x^* = \frac{\partial w^*}{\partial x}$ and $u_y^* = \frac{\partial u^*}{\partial y}$, $v_y^* = \frac{\partial v^*}{\partial y}$, $w_y^* = \frac{\partial w^*}{\partial y}$

$$\mathbf{L}^t = \begin{bmatrix} u_x^* & v_x^* & w_x^* \\ u_y^* & v_y^* & w_y^* \\ 0 & 0 & 0 \end{bmatrix} \quad (3.8)$$

By using equations (3.7) and (3.8) in (3.5) we get

$$A_1 = \begin{bmatrix} 2u_x^* & v_x^* + u_y^* & w_x^* \\ u_y^* + v_x^* & 2v_y^* & w_y^* \\ w_x^* & w_y^* & 0 \end{bmatrix} \quad (3.9)$$

By using (3.9) in (3.4) we get

$$\boldsymbol{\tau} = \begin{bmatrix} 2\mu u_x^* - p & \mu(v_x^* + u_y^*) & \mu w_x^* \\ \mu(u_y^* + v_x^*) & 2\mu v_y^* & \mu w_y^* \\ \mu w_x^* & \mu w_y^* & -p \end{bmatrix} \quad (3.10)$$

Momentum equation in reduce form for rotational flow is

$$\rho_{hnf} \frac{\partial \mathbf{V}}{\partial t} + 2\Omega \times \mathbf{V} = \text{div} \boldsymbol{\tau} + \mathbf{J} \times \mathbf{B}, \quad (3.11)$$

Where $\Omega = [0, \Omega, 0]$ and $\mathbf{J} \times \mathbf{B} = [-\bar{\sigma}_f B_o^2 u^*, 0, -\bar{\sigma}_f B_o^2 w^*]$.

For law of conservation of mass, continuity equation define as:

$$\frac{\partial v^*}{\partial y} + \frac{\partial u^*}{\partial x} = 0 \quad (3.12)$$

For the momentum equation

Along x-component:

$$\rho_{hnf} \frac{\partial \mathbf{V}}{\partial t} + 2\Omega \times \mathbf{V} = \frac{\partial}{\partial x} \tau_{xx} + \frac{\partial}{\partial y} \tau_{xy}, \quad (3.13)$$

By using (3.10) in (3.11) we have

$$v^* \frac{\partial u^*}{\partial y} + u^* \frac{\partial u^*}{\partial x} + 2\Omega w^* = -\frac{1}{\rho_{hnf}} \frac{\partial P}{\partial x} + \frac{\mu_{hnf}}{\rho_{hnf}} \left(\frac{\partial^2 u^*}{\partial x^2} + \frac{\partial^2 u^*}{\partial y^2} \right) - \frac{\bar{\sigma}_f B_o^2}{\rho_{hnf}} u^*. \quad (3.14)$$

Along y -component:

$$\rho_{hnf} \frac{\partial \mathbf{V}}{\partial t} + 2\Omega \times \mathbf{V} = \frac{\partial}{\partial x} \tau_{yx} + \frac{\partial}{\partial y} \tau_{yy}, \quad (3.15)$$

By using (3.10) in (3.14)

$$v^* \frac{\partial v^*}{\partial y} + u^* \frac{\partial v^*}{\partial x} = -\frac{1}{\rho_{hnf}} \frac{\partial P}{\partial y} + \frac{\mu_{hnf}}{\rho_{hnf}} \left(\frac{\partial^2 v^*}{\partial x^2} + \frac{\partial^2 v^*}{\partial y^2} \right). \quad (3.16)$$

Along z -component:

$$\rho_{hnf} \frac{\partial \mathbf{V}}{\partial t} + 2\Omega \times \mathbf{V} = \frac{\partial}{\partial x} \tau_{zx} + \frac{\partial}{\partial y} \tau_{zy}, \quad (3.17)$$

By using (3.10) in (3.16) we get

$$v^* \frac{\partial w^*}{\partial y} + u^* \frac{\partial w^*}{\partial x} - 2\Omega u^* = \frac{\mu_{hnf}}{\rho_{hnf}} \left(\frac{\partial^2 w^*}{\partial x^2} + \frac{\partial^2 w^*}{\partial y^2} \right) - \frac{\bar{\sigma}_f B_o^2}{\rho_{hnf}} w^*. \quad (3.18)$$

For energy equation, we have:

$$(\rho C_p)_{hnf} ((\mathbf{V} \cdot \nabla) T^*) = \boldsymbol{\tau} \cdot \mathbf{L} + \mathbf{J} \times \mathbf{B}, \quad (3.19)$$

Using value of $\tau \cdot \mathbf{L}$ in equation (3.18) we have

$$\begin{aligned}
v^* \frac{\partial T^*}{\partial y} + u^* \frac{\partial T^*}{\partial x} &= \frac{k_{hnf}}{(\rho C_p)_{hnf}} \left(\frac{\partial^2 T^*}{\partial x^2} + \frac{\partial^2 T^*}{\partial y^2} \right) - \frac{1}{(\rho C_p)_{hnf}} \frac{\partial q_{rad}^*}{\partial y} \\
&+ \frac{\bar{\sigma}_f B_o^2}{(\rho C_p)_{hnf}} (u^{*2} + w^{*2}) , \tag{3.20}
\end{aligned}$$

In equations Ω is angular velocity, u^*, w^*, v^* are velocities in x, y and z directions, B_o is magnetic field, P is pressure, T^* is temperature, $\bar{\sigma}_f$ is electrical conductivity and q_{rad}^* is radiative demonstrate heat flux.

For radiation

$$q_{rad}^* = - \left(\frac{4\sigma^*}{3k_{hnf}^*} \right) \frac{\partial T^{*4}}{\partial y} , \tag{3.21}$$

We can expand T^{*4} in a Taylor series and by this expansion we get

$$T^{*4} \cong -3T_{\infty}^{*4} + 4T_{\infty}^{*3} T^* , \tag{3.22}$$

So the equation (3.19) become

$$\begin{aligned}
v^* \frac{\partial T^*}{\partial y} + u^* \frac{\partial T^*}{\partial x} &= \frac{k_{hnf}}{(\rho C_p)_{hnf}} \left(\frac{\partial^2 T^*}{\partial x^2} + \frac{\partial^2 T^*}{\partial y^2} \right) + \frac{16\sigma^* T_{\infty}^{*3}}{3k_{nf}^* (\rho C_p)_{nf}} \frac{\partial^2 T^*}{\partial y^2} \\
&+ \frac{\bar{\sigma}_f B_o^2}{(\rho C_p)_{hnf}} (u^{*2} + w^{*2}) , \tag{3.23}
\end{aligned}$$

Effective dynamic viscosity, heat capacity and thermal conductivity are define as:

$$\rho_{hnf} = (1 - \phi_{Cu} - \phi_{Go})\rho_f + \phi_{Cu}\rho_{Cu} + \phi_{Go}\rho_{Go} , \tag{3.24}$$

$$(\rho C_p)_{hnf} = (1 - \phi_{Cu} - \phi_{Go})(\rho C_p)_f + \phi_{Cu}(\rho C_p)_{Cu} + \phi_{Go}(\rho C_p)_{Go} , \tag{3.25}$$

$$\mu_{nf} = \mu_f (1 - \phi_{Cu} - \phi_{Go})^{-2.5} , \tag{3.26}$$

$$\frac{k_{hnf}}{k_f} = \left\{ \frac{k_{Cu}\phi_{Cu} + k_{Go}\phi_{Go}}{\phi_{Cu} + \phi_{Go}} + 2k_f + 2(k_{Cu}\phi_{Cu} + k_{Go}\phi_{Go}) - 2(\phi_{Cu} + \phi_{Go})k_f \right\} \left\{ \frac{k_{Cu}\phi_{Cu} + k_{Go}\phi_{Go}}{\phi_{Cu} + \phi_{Go}} + 2k_f - (k_{Cu}\phi_{Cu} + k_{Go}\phi_{Go}) + (\phi_{Cu} + \phi_{Go})k_f \right\}^{-1}. \quad (3.27)$$

Table1. Thermo physical properties of hybrid nanofluid and water.

	(kg/m ³)	C _p (J/kg K)	k(W/m k)
Graphene Oxide (Go)	1800	717	5000
Copper (Cu)	8933	385	401
Pure water	997.1	4179	0.613

Boundary conditions at lower and upper surfaces are:

$$u^* = u_w^* = ax, \quad v^* = 0, \quad w^* = 0, \quad T^* = T_H^* \quad \text{at } y = 0 \quad (3.28)$$

$$u^* = 0, \quad v^* = v_o, \quad w^* = 0, \quad T^* = T_o^* \quad \text{at } y = h \quad (3.29)$$

Using similarity variables:

$$\eta = \frac{y}{h}, \quad v^* = -ahf(\eta), \quad u^* = axf'(\eta), \quad w^* = axg(\eta), \quad \theta = \frac{T^* - T_H^*}{T_o^* - T_H^*}. \quad (3.30)$$

By using similarity variables the given PDE's transformed in to dimensionless ODE's.

$$f^{iv} + B_1(1 - \phi_{Cu} - \phi_{Go})^{2.5}Re(ff'''' - f'f''') - 2B_1R_o((1 - \phi_{Cu} - \phi_{Go})^{2.5}g' - Mn((1 - \phi_{Cu} - \phi_{Go})^{2.5}f'') = 0, \quad (3.31)$$

$$g'' + B_1(1 - \phi_{Cu} - \phi_{Go})^{2.5}Re(fg' - f'g) + 2B_1R_o((1 - \phi_{Cu} - \phi_{Go})^{2.5}f' - Mn((1 - \phi_{Cu} - \phi_{Go})^{2.5}g) = 0, \quad (3.32)$$

$$\theta'' + B_2PrRe\left(\frac{3}{3+4N}\right)\frac{k_f}{k_{hnf}}f\theta' + MnPrEc\left(\frac{3}{3+4N}\right)\frac{k_f}{k_{hnf}}(f'^2 + g^2) = 0. \quad (3.33)$$

B₁, B₂ are constant and given as:

$$B_1 = (1 - \phi_{Cu} - \phi_{Go}) + \frac{\phi_{Cu}\rho_{Cu} + \phi_{Go}\rho_{Go}}{\rho_f},$$

$$B_2 = (1 - \phi_{Cu} - \phi_{Go}) + \frac{\phi_{Cu}(\rho C_p)_{Cu} + \phi_{Go}(\rho C_p)_{Go}}{(\rho C_p)_f}$$

Dimensionless parameter are

$$N = \frac{4\sigma^* T_\infty^{*3}}{k_{hnf} k_{hnf}^*}, \quad Pr = \frac{\mu_f(\rho C_p)_f}{\rho_f k_f}, \quad Mn = \frac{\bar{\sigma}_f B_0^2 h^2}{\rho_f \vartheta_f}, \quad (3.34)$$

$$Re = \frac{ah^2}{\nu}, \quad Ro = \frac{\Omega h^2}{\vartheta_f}, \quad Ec = \frac{\rho_f ah^2}{(\rho C_p)_f (T_o^* - T_H^*)} \quad (3.35)$$

Relevant surface constrain for model are

$$f = 0, \quad f' = 1, \quad g = 0, \quad \theta = 1 \quad \text{at } \eta = 0, \quad (3.36)$$

$$f = A, \quad f' = 0, \quad g = 0, \quad \theta = 0 \quad \text{at } \eta = 1. \quad (3.37)$$

Skin friction coefficient is defined as

$$C_f = \frac{\mu_{hnf}}{\rho_f \nu_o^2} \left. \frac{\partial u}{\partial y} \right|_{y=0}, \quad (3.38)$$

And also Nusselt number is

$$Nu = \left[\frac{h}{k_f (T_o^* - T_H^*)} \right] \left(k_{hnf} + \frac{16\sigma^* T_\infty^{*3}}{3k_{hnf}^*} \right) \left. \frac{\partial T^*}{\partial y} \right|_{y=0}. \quad (3.39)$$

We gain:

$$C_f^* = |(1 - \phi_{Cu} - \phi_{Go})^{-2.5} f''(0)|, \quad (3.40)$$

$$Nu^* = \left| \frac{k_{hnf}}{k_f} \left(1 + \frac{4}{3} N \right) \theta'(0) \right|. \quad (3.41)$$

3.2 Implementation of method:

We convert given order of ODE's in to first order ODE's by applying modified Adomian decomposition method and then solve analytically.

First we write higher ODE's as

$$L_4 f(\eta) = -B_1 (1 - \phi_{Cu} - \phi_{Go})^{2.5} Re (ff''' - f'f'') + 2B_1 Ro ((1 - \phi_{Cu} - \phi_{Go})^{2.5} g' + Mn ((1 - \phi_{Cu} - \phi_{Go})^{2.5} f''), \quad (3.42)$$

$$L_2 g(\eta) = -\mathbb{B}_1(1 - \phi_{Cu} - \phi_{Go})^{2.5} Re(fg' - f'g) - 2\mathbb{B}_1 Ro((1 - \phi_{Cu} - \phi_{Go})^{2.5} f' + Mn((1 - \phi_{Cu} - \phi_{Go})^{2.5} g), \quad (3.43)$$

$$L_2 \theta(\eta) = -\mathbb{B}_2 Pr Re \left(\frac{3}{3 + 4N} \right) \frac{k_f}{k_{hnf}} f \theta' - Mn Pr Ec \left(\frac{3}{3 + 4N} \right) \frac{k_f}{k_{hnf}} (f'^2 + g^2), \quad (3.44)$$

Where $L_4 = \frac{d^4}{d\eta^4}$ and $L_2 = \frac{d^2}{d\eta^2}$

Let L_4^{-1} and L_2^{-1} exist:

$$L_4^{-1}(\cdot) = \int_0^\eta \int_0^\eta \int_0^\eta \int_0^\eta (\cdot) d\eta d\eta d\eta d\eta \quad (3.45)$$

$$L_2^{-1}(\cdot) = \int_0^\eta \int_0^\eta (\cdot) d\eta d\eta \quad (3.46)$$

Putting with L_4^{-1} and L_2^{-1} in equation, (3.42), (3.43) and (3.44). and by applying boundary conditions we get

$$f(\eta) = f''(0) \frac{\eta^2}{2} + f'(0)\eta + L_4^{-1}(\dot{N}_1 u^*) + f(0) + f'''(0) \frac{\eta^3}{6}, \quad (3.47)$$

and also

$$g(\eta) = L_2^{-1}(\dot{N}_2 u^*) + g(0) + g'(0)\eta, \quad (3.48)$$

$$\theta(\eta) = L_2^{-1}(\dot{N}_3 u^*) + g(0) + \theta'(0)\eta, \quad (3.49)$$

Where

$$N_1' u^* = -\mathbb{B}_1(1 - \phi_{Cu} - \phi_{Go})^{2.5} Re(ff''' - f'f'') + 2\mathbb{B}_1 Ro((1 - \phi_{Cu} - \phi_{Go})^{2.5} g' + Mn((1 - \phi_{Cu} - \phi_{Go})^{2.5} f''), \quad (3.50)$$

$$N_2' u^* = -\mathbb{B}_1(1 - \phi_{Cu} - \phi_{Go})^{2.5} Re(fg' - f'g) - 2\mathbb{B}_1 Ro((1 - \phi_{Cu} - \phi_{Go})^{2.5} f' + Mn((1 - \phi_{Cu} - \phi_{Go})^{2.5} g), \quad (3.51)$$

$$\begin{aligned}
N_3' u^* &= -B_2 Pr Re \left(\frac{3}{3+4N} \right) \frac{k_f}{k_{hmf}} f \theta' \\
&\quad - Mn Pr Ec \left(\frac{3}{3+4N} \right) \frac{k_f}{k_{hmf}} (f'^2 + g^2),
\end{aligned} \tag{3.52}$$

Now we first find the values of $f''(0)$, $f'''(0)$, $g'(0)$ and $\theta'(0)$ by using normal ADM and then put in equation (3.42), (3.43) and (3.44).

First put with L_4^{-1} on equation (3.31) at $\eta=1$ we have:

$$\int_0^1 \int_0^\eta \int_0^\eta \int_0^\eta f^{iv}(\eta) d\eta d\eta d\eta d\eta = [L_4^{-1}(N_1' u^*)]_{\eta=1}, \tag{3.53}$$

$$\int_0^1 \int_0^\eta \int_0^\eta \int_0^\eta (N_1' u^*) d\eta d\eta d\eta d\eta = [L_4^{-1}(N_1' u^*)]_{\eta=1}, \tag{3.54}$$

Integrate and by apply boundary conditions:

$$-1 - \frac{1}{2} f''(0) + A - \frac{1}{6} f'''(0) = [L_4^{-1}(N_1' u^*)]_{\eta=1} \tag{3.55}$$

First put with L_3^{-1} on equation (3.32) at $\eta=1$ we have:

$$\int_0^1 \int_0^\eta \int_0^\eta (N_1' u^*) d\eta d\eta d\eta = [L_3^{-1}(N_1' u^*)]_{\eta=1}, \tag{3.56}$$

After applying integration we get

$$-1 - f''(0) - \frac{1}{2} f'''(0) = [L_3^{-1}(N_1' u^*)]_{\eta=1} \tag{3.57}$$

By subtracting equation (3.55) from (3.57) we have.

$$f'''(0) = -6[L_3^{-1}(N_1' u^*)]_{\eta=1} - 12A + 12[L_4^{-1}(N_1' u^*)]_{\eta=1} + 6, \tag{3.58}$$

and

$$f''(0) = +2[L_3^{-1}(N_1' u^*)]_{\eta=1} + 6A - 6[L_4^{-1}(N_1' u^*)]_{\eta=1} - 4, \tag{3.59}$$

Now put $f''(0)$ and $f'''(0)$ in equation (3.46) we have

$$\begin{aligned}
f(\eta) = & -(1 - 2A)\eta^3 + [L_4^{-1}(N_1'u^*)] + \eta + (3A - 2)\eta^2 + (2\eta^3 - 3\eta^2)[L_4^{-1}(N_1'u^*)]_{\eta=1} \\
& + (\eta^2 - \eta^3)[L_3^{-1}(N_1'u^*)]_{\eta=1},
\end{aligned} \tag{3.60}$$

So we can write it as:

$$\begin{aligned}
f_o(\eta) &= -(1 - 2A)\eta^3 + \eta + (3A - 2)\eta^2, \\
f_{n+1}(\eta) &= [L_4^{-1}(N_1'u^*)] + (2\eta^3 - 3\eta^2)[L_4^{-1}(N_1'u^*)]_{\eta=1} \\
&+ (\eta^2 - \eta^3)[L_3^{-1}(N_1'u^*)]_{\eta=1},
\end{aligned} \tag{3.61}$$

and also

$$\begin{aligned}
g_o(\eta) &= 0, \\
g_{n+1}(\eta) &= [L_2^{-1}(N_2'u^*)] - \eta[L_2^{-1}(N_2'u^*)]_{\eta=1},
\end{aligned} \tag{3.62}$$

For $\theta(\eta)$

$$\begin{aligned}
\theta_o(\eta) &= 1 - \eta, \\
\theta_{n+1}(\eta) &= [L_2^{-1}(N_3'u^*)] - \eta[L_2^{-1}(N_3'u^*)]_{\eta=1}.
\end{aligned} \tag{3.65}$$

Using Maple software for analytical solution of the problem.

Table2. Contrast between present and Ref.6 results of Nusselt number.

	Re	$N, Mn=0, Ec=0$	6 results
$\emptyset = 0\%$	0.1	1.078381555	1.07650
	0.5	1.403658578	1.40437
	1	1.813100376	1.81603
	1.5	2.201327214	2.20219
$\emptyset = 5\%$	0.1	1.298621376	1.29872
	0.5	1.619052807	1.29872
	1	2.026519802	2.02732
	1.5	2.422539174	2.42441
$\emptyset = 10\%$	0.1	1.573849277	1.57195
	0.5	1.889474207	1.88889
	1	1.889474207	2.29326
	1.5	2.292857255	2.29326
		2.691972738	2.69399

3.3 Results and discussion

Fluid flow is considered between two parallel plates in which the upper wall is stretchable and other is penetrable and also under the influence of thermal radiation and joule heating. Heat transfer and MHD hybrid nanofluid flow are study analytically. Different parameters which includes rotation (R_o), radiation (N), magnetic (Mn), Reynolds number (Re), suction\injection (A) and hybrid nanofluid volume fraction (ϕ) are explored concerning the flow and heat transfer. Detail of thermo physical properties are discussed in Table.1.It is noted that equal volume fraction of graphene oxide and cupper ($\phi_{Cu} = \phi_{Go} = 0.5\phi$) are utilized. Solution is obtained by using analytical technique and then MAPLE is used for graphical representation to see the effects of velocity and temperature profile for different parameter.

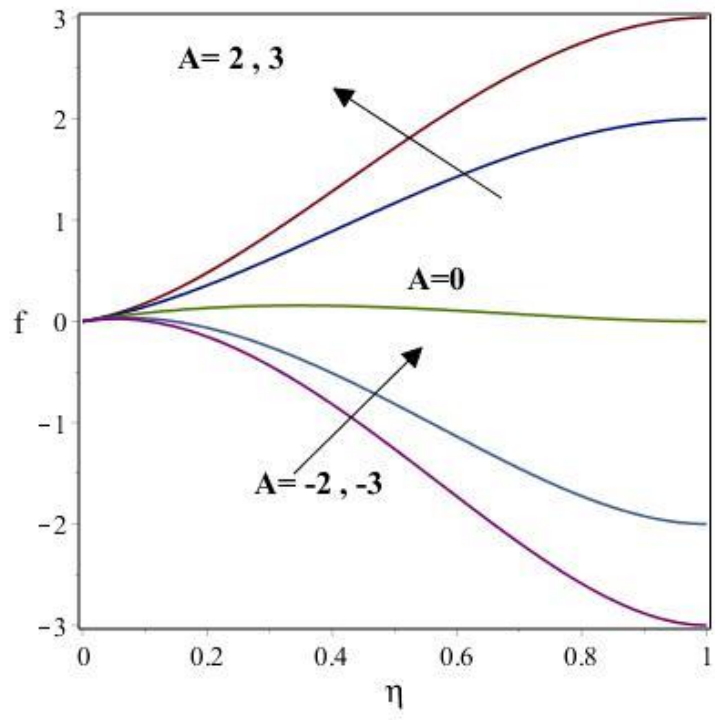
Figure. (3.2) and (3.3) shows the effect of A and Re on velocity profile f and g accordingly. It is mention earlier that $A > 0$ shows the injection flow and $A < 0$ shows the suction flow from upper wall. One can see that, if values of injection parameter increases then velocity profile also rises. While for suction parameter, increase in value of suction parameter causes decrease in velocity profile. Contrastingly, for injection process g decreases and f increases when Re number increases. Moreover, for small value of Re , the g shows centerline symmetry while at larger value of Re , higher velocity point moves to upper wall.

Figure. (3.4) and (3.5). Indicate the impact of Re and A on temperature profile and Nusselt number. For injection process temperature profile decreases and Nusselt number increases while for suction process Nusselt number goes down. With ascending Re , θ will diminish .The results also indicate that shear stress increases and Nusselt number goes up with an increase in Reynolds number. Although, this is valid for any value of injection parameter and for small value of suction parameter. Also Nusselt number become decreasing function of Re for larger value of suction parameter.

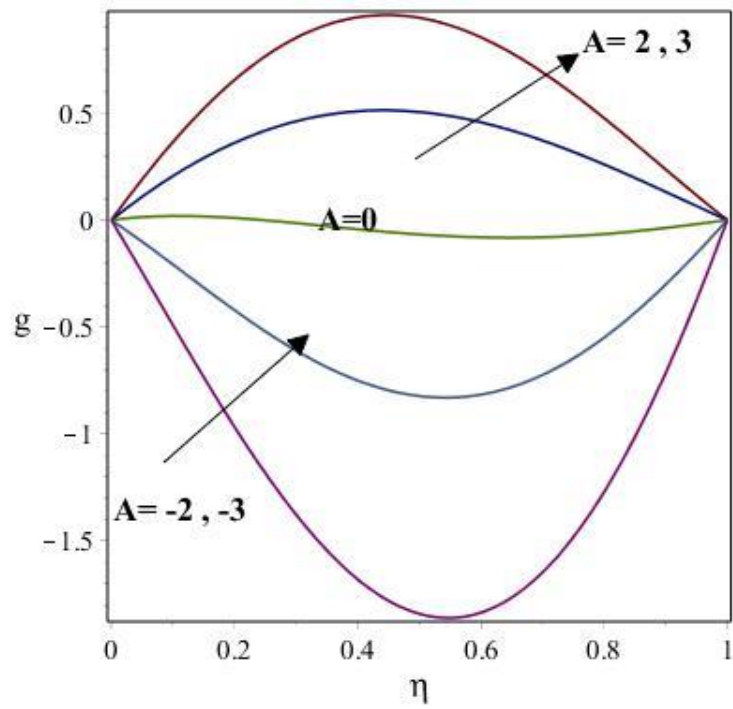
In Figure. (3.6) and (3.7) the impact of Mn and R_o on velocity profile are discussed. Experienced that, by increasing Mn , the Lorentz force also rises and resist more effectively to the flow. In this manner the velocity profile will be degraded by increasing Mn . This is introduce in Figure. (3.7). It tends to be additionally conclude that climbing upside of rotation parameter causes increase in g and decrease in f . In any case, this is valid for variety of f for rotation parameter at $\eta > 0.3$. But For $\eta < 0.3$ the value of f become increases. Figure. (3.8) and (3.9) depict that, the rising qualities of magnetic and rotation parameter cause the thermal boundary layer to be condense, bringing about the temperature profile's increases with an expanding in the magnetic and rotation parameter.

In addition, in light of the fact that the Nusselt number and the thermal boundary layer thickness have a rearranged relationship, the Nusselt number lessens with increasing Mn also, R_o .

Figure. (3.10) and (3.11). Depicts R_o and ϕ impact on Nusselt number and temperature profile. An increase in value of R_o and ϕ of hybrid nanofluid cause an increase in hybrid nanofluid temperature. Accordance to Eq. (3.41), the Nusselt number is pronounced as an intensification of $(\frac{k_{nf}}{k_f})$, $((4/3)N + 1)$ and $\theta'(0)$. As increasing the value of hybrid nanofluid volume fraction cause an increase in $(\frac{k_{nf}}{k_f})$ which is higher than the decreasing value of $\theta'(0)$ for certain value of N and also by raising the value of N results decrease in $\theta'(0)$ which is smaller than increasing value of $((4/3)N + 1)$ for certain value of ϕ . So we can securely count that the Nusselt number increases with increasing hybrid nanofluids N and ϕ . Hence we find Nusselt number as an active parameter in our study.

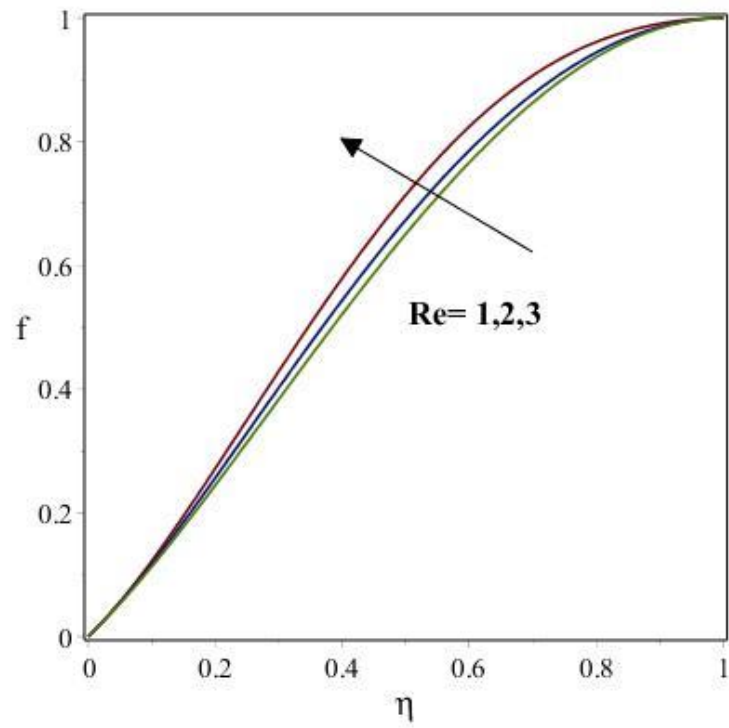


(a)

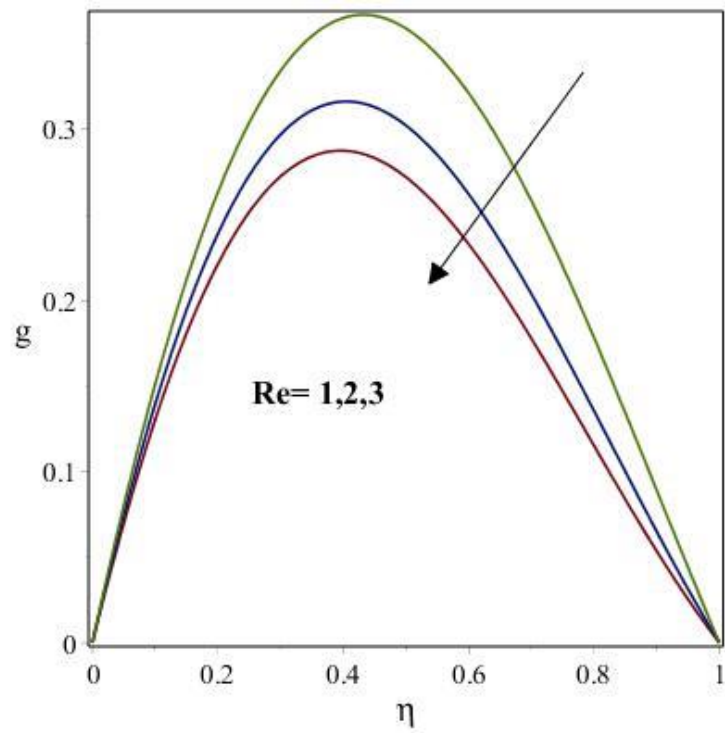


(b)

Figure.(3.2). Variation of suction/injection parameter with velocity profile (a) $f(\eta)$ and (b) $g(\eta)$.

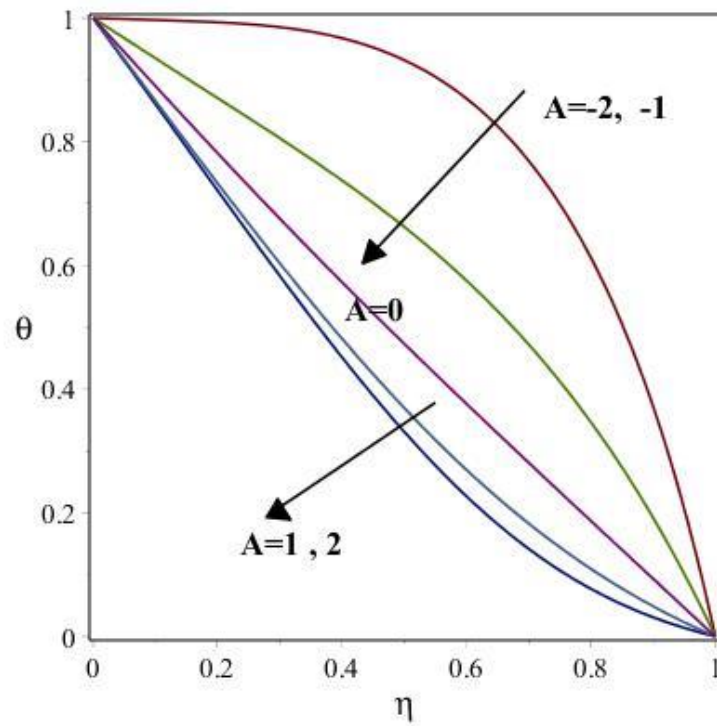


(a)

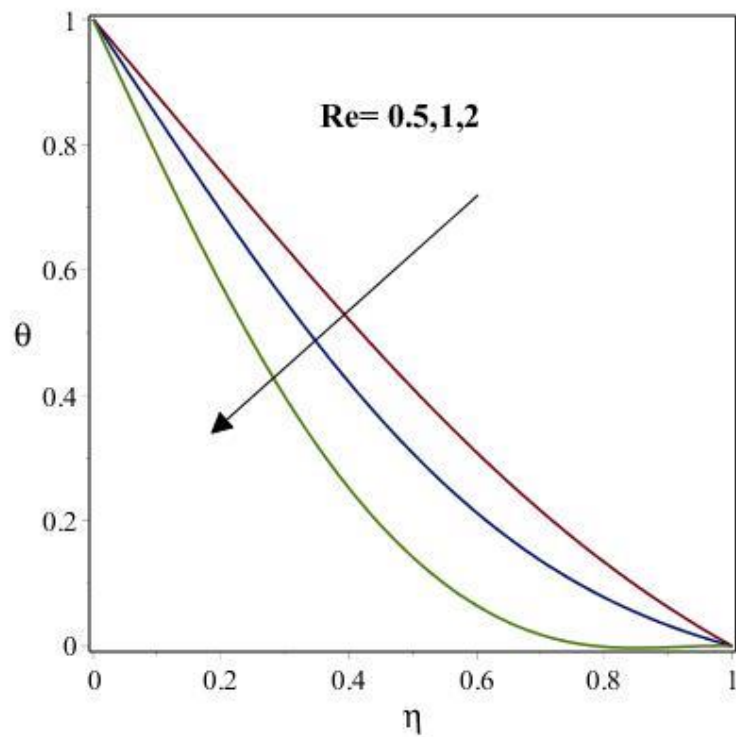


(b)

Figure.(3.3). Variation of Reynold number with velocity profiles (a) $f(\eta)$ and (b) $g(\eta)$..

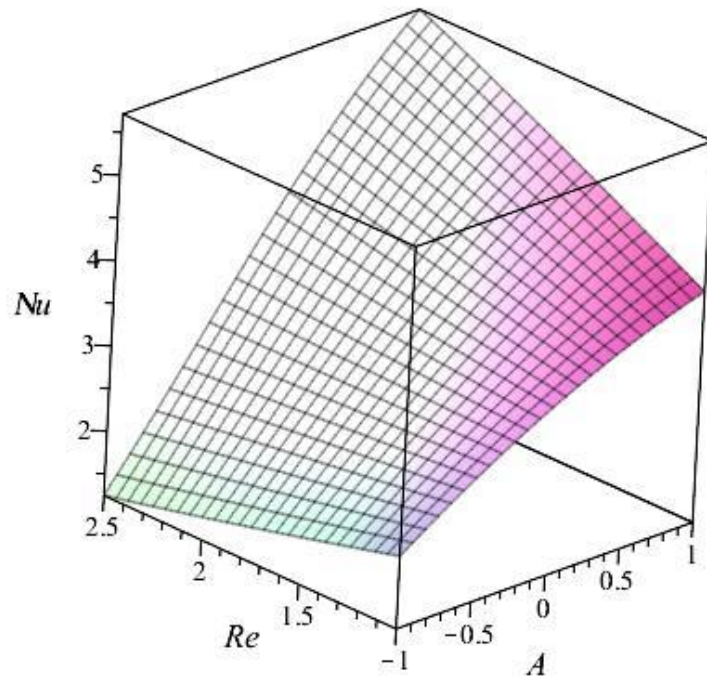


(a)

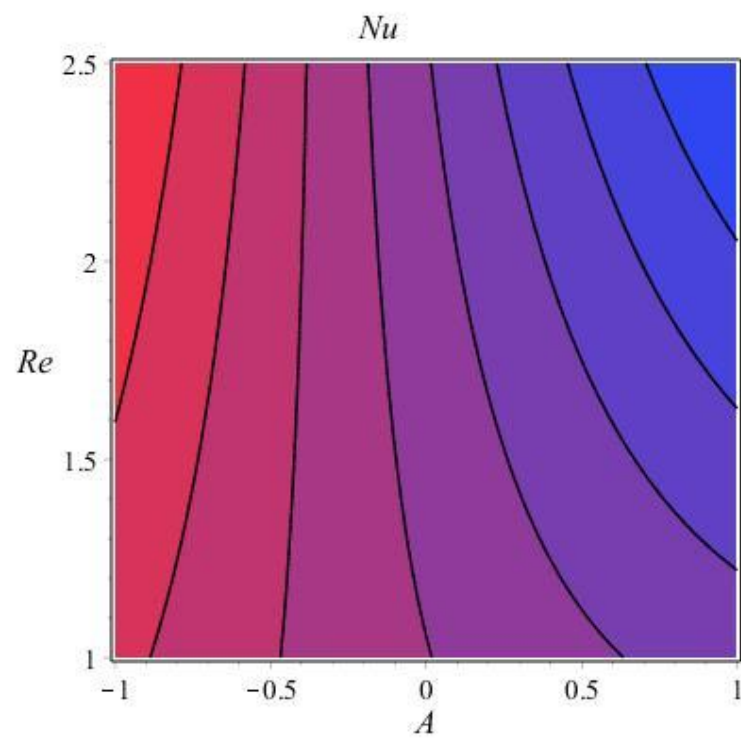


(b)

Figure. (3.4). Influence of (a) A and (b) Re on the temperature profile.

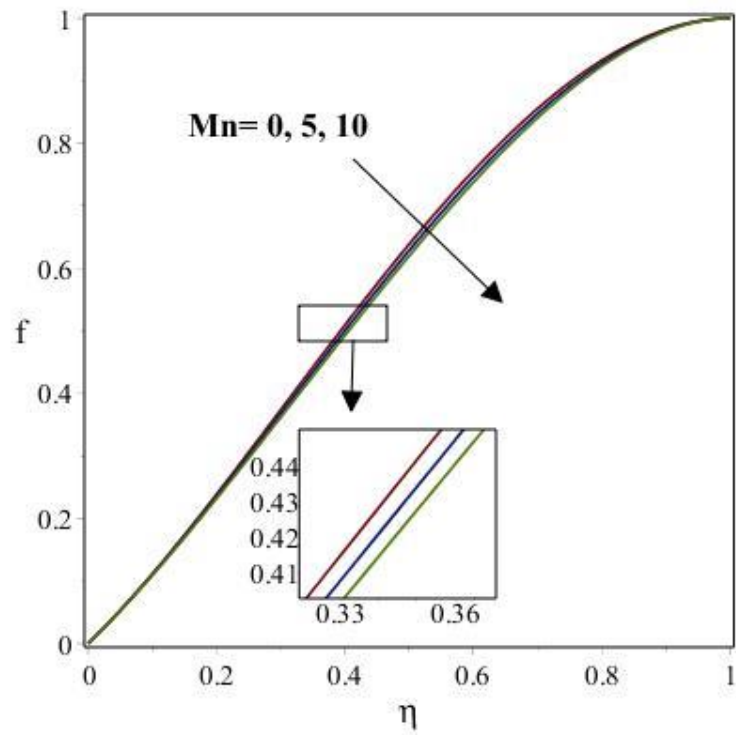


(a)

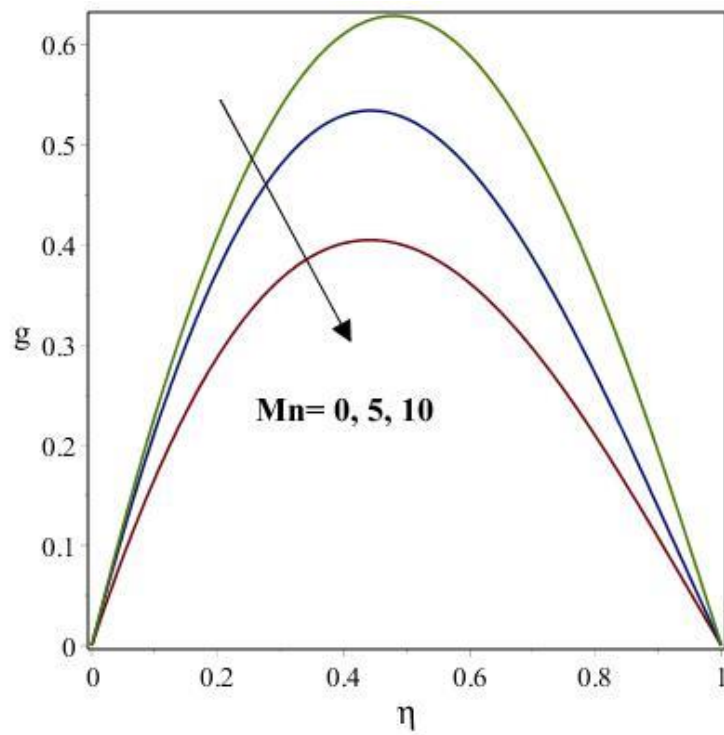


(b)

Figure. (3.5). Variation of (a) A and (b) Reynolds number with Nusselt number.

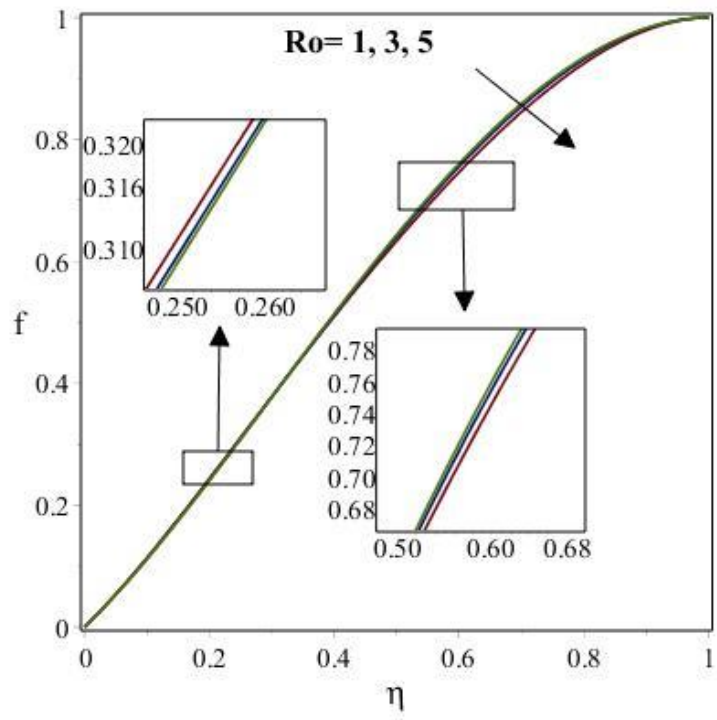


(a)

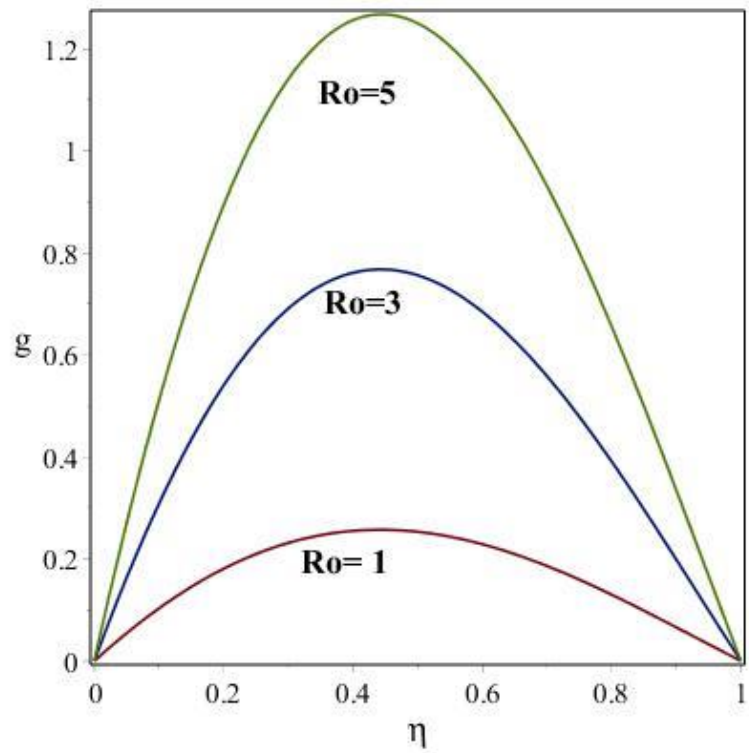


(b)

Figure.(3.6). variation of magnetic parameter with (a) $f(\eta)$ and (b) $g(\eta)$.

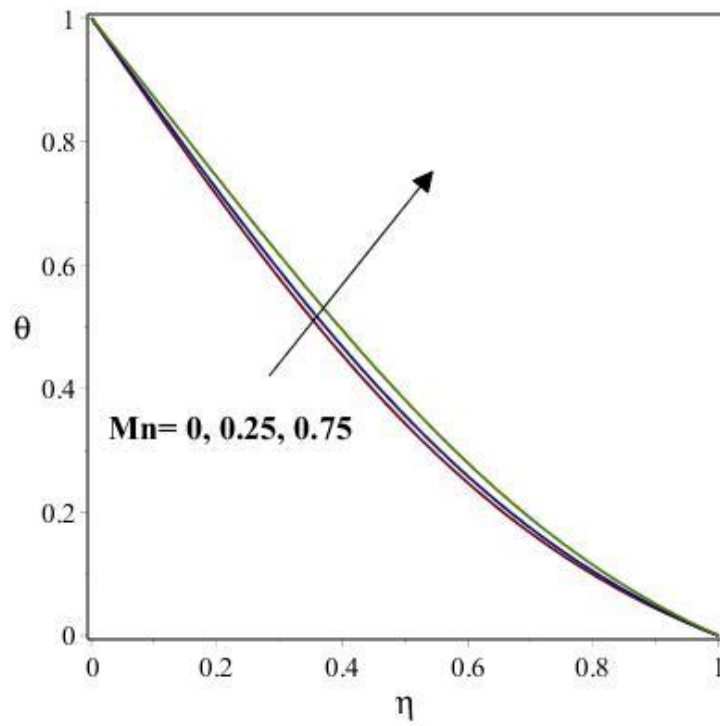


(a)

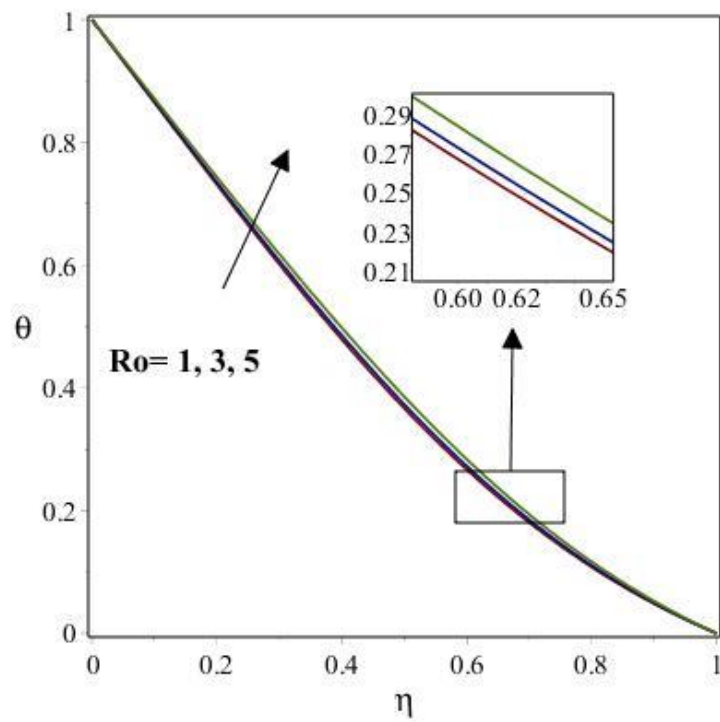


(b)

Figure.(3.7). Variation of Rotation parameter with velocity profile (a) $f(\eta)$ and (b) $g(\eta)$.

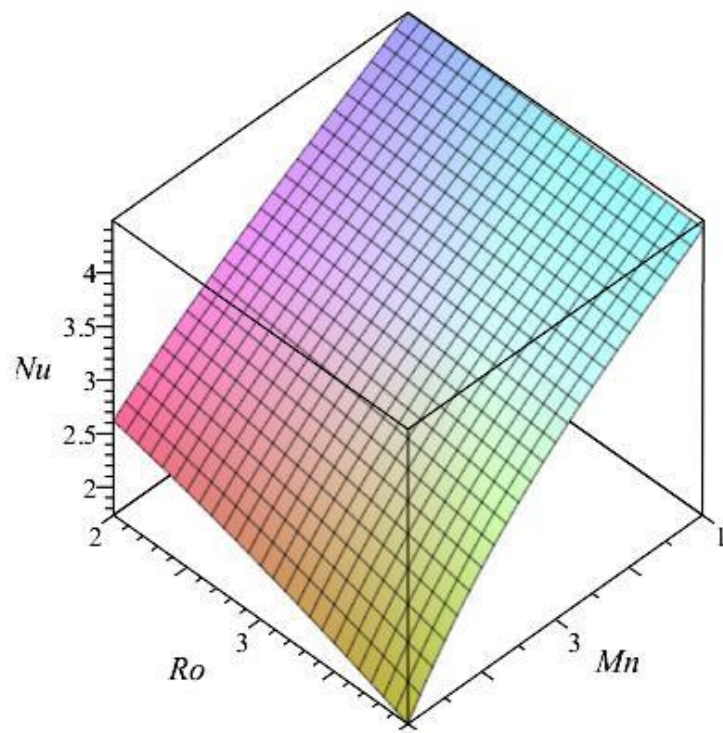


(a)

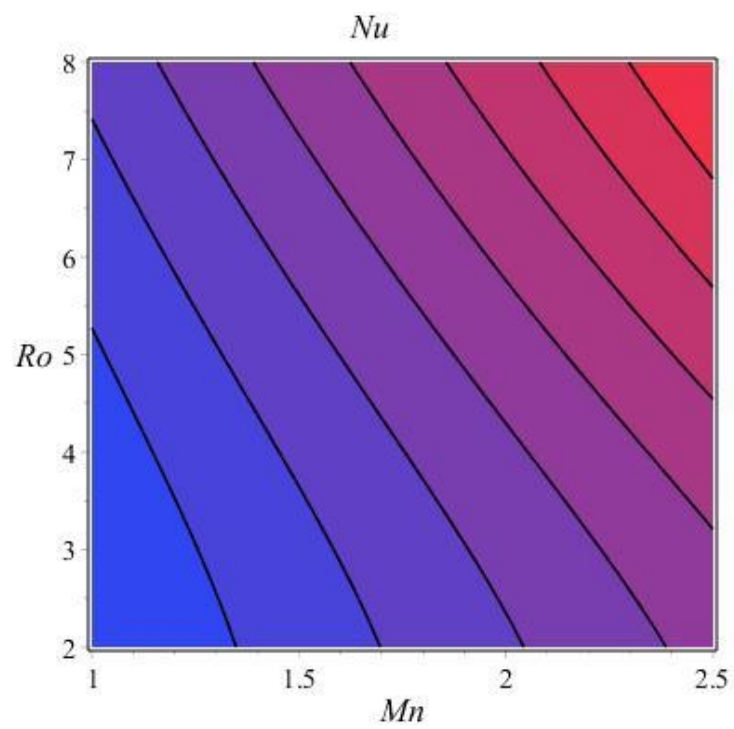


(b)

Figure. (3.8). Influence of (a) magnetic and (b) rotation parameters on the temperature profile.

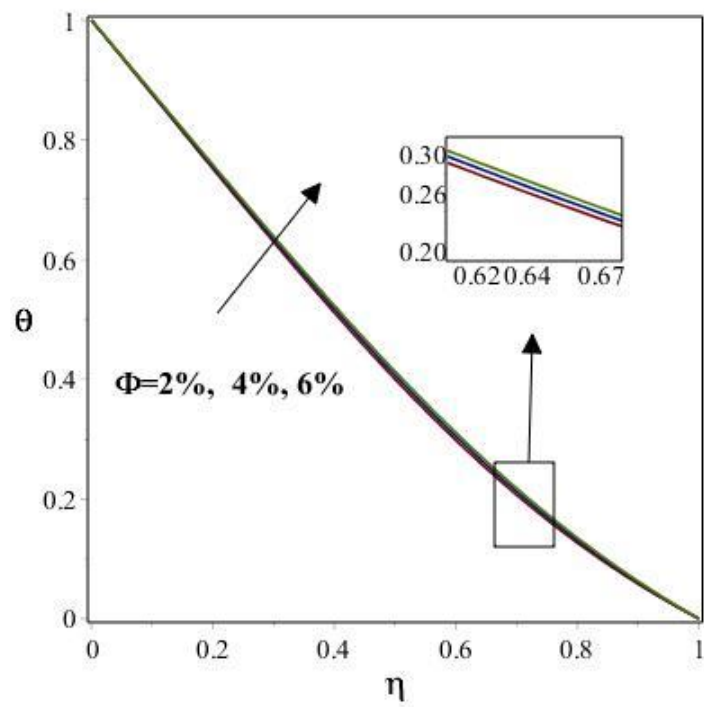


(a)

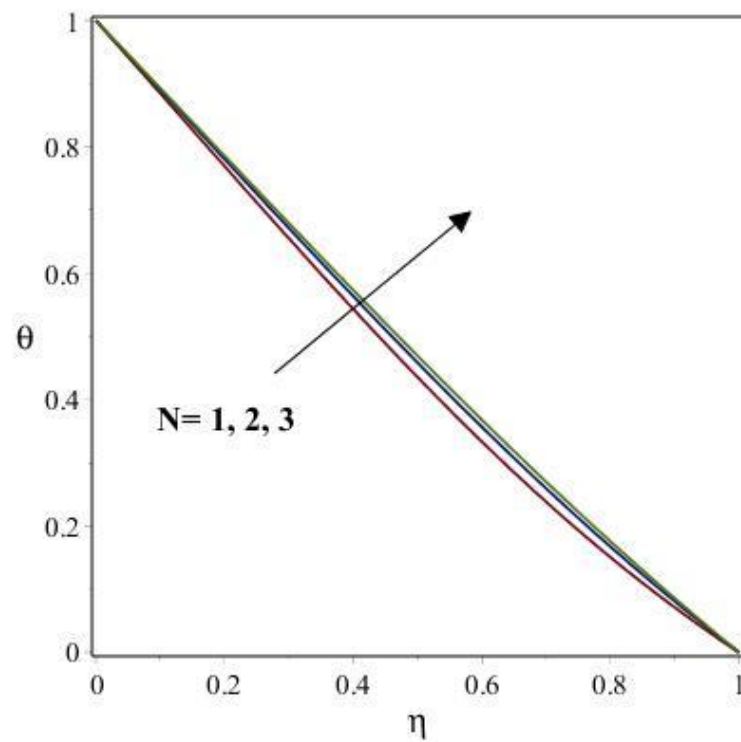


(b)

Figure. (3.9). Influence of (a) magnetic and (b) rotation parameters on the Nusselt number.

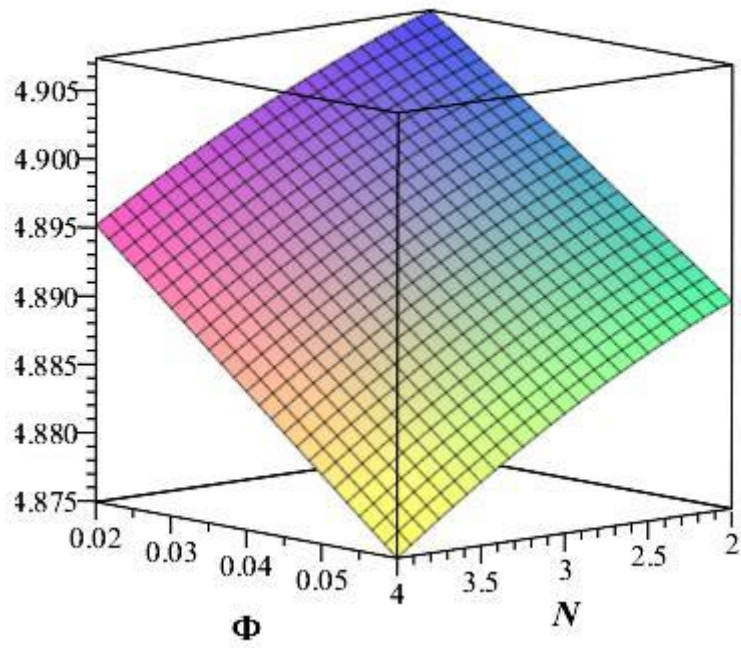


(a)

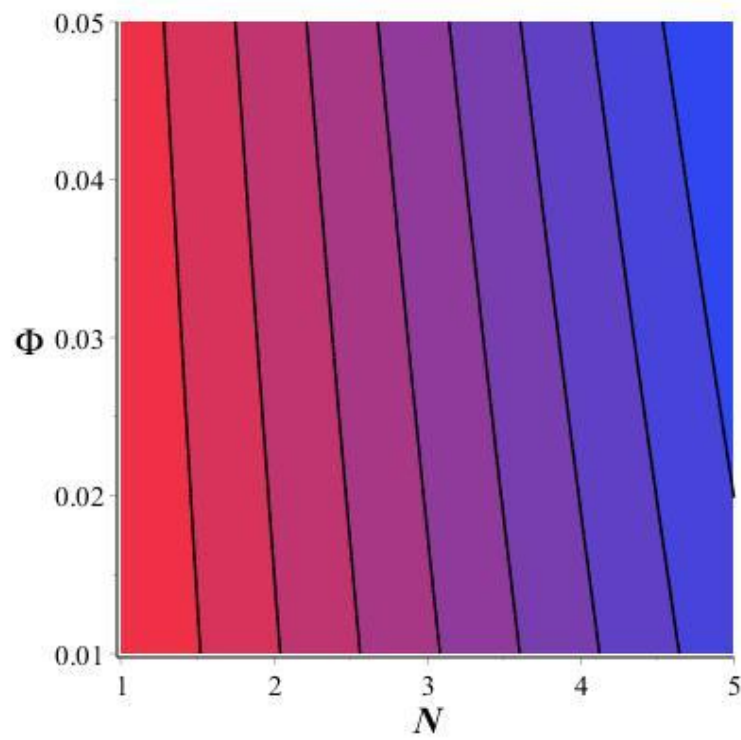


(b)

Figure. (3.10). Influence of (a) N and (b) ϕ on the temperature profile.



(a)



(b)

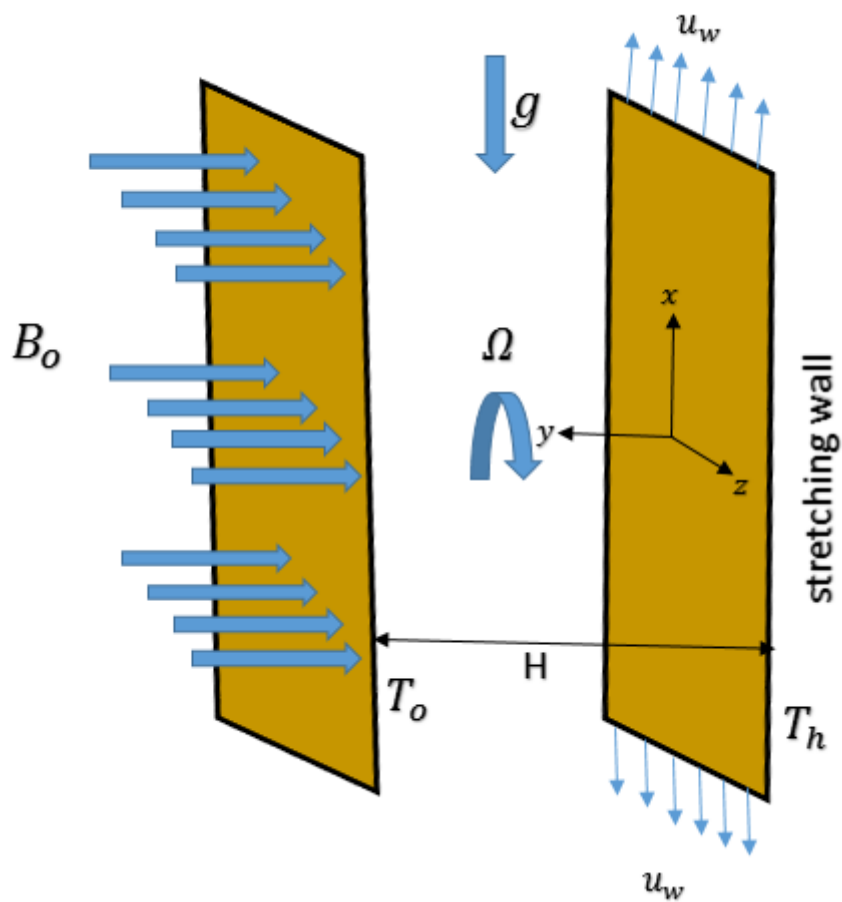
Figure. (3.11). influence of solid volume fraction on Nusselt number.

Chapter 4

Thermal performance of hybrid nanofluid in a rotating vertical channel between two plates

This chapter is extension of previous chapter by adding new terms of mixed convection and heat generation\absorption. Based upon previous chapter 3 the mathematical model rearranged and new effect has included. Results are obtained by analytical technique.

4.1 Modeling of problem



4.1: Geometry of problem

Consider steady, incompressible flow between two vertical plates. Due to rotation of channel fluid is rotating with velocity Ω . Motion of the plate is due to velocity $u^* = ax$.

The governing equation of energy and momentum are:

$$\frac{\partial v^*}{\partial y} + \frac{\partial u^*}{\partial x} = 0 \quad (4.1)$$

$$\begin{aligned} v^* \frac{\partial u^*}{\partial y} + u^* \frac{\partial u^*}{\partial x} + 2\Omega w^* \\ = -\frac{1}{\rho_{hnf}} \frac{\partial P}{\partial x} + \frac{\mu_{hnf}}{\rho_{hnf}} \left(\frac{\partial^2 u^*}{\partial x^2} + \frac{\partial^2 u^*}{\partial y^2} \right) - \frac{\bar{\sigma}_f B_o^2}{\rho_{hnf}} u^* + \frac{g(\rho\beta)_{hnf}(T^* - T_o^*)}{(\rho C_p)_{hnf}}, \end{aligned} \quad (4.2)$$

$$v^* \frac{\partial v^*}{\partial y} + u^* \frac{\partial v^*}{\partial x} = -\frac{1}{\rho_{hnf}} \frac{\partial P}{\partial y} + \frac{\mu_{hnf}}{\rho_{hnf}} \left(\frac{\partial^2 v^*}{\partial x^2} + \frac{\partial^2 v^*}{\partial y^2} \right), \quad (4.3)$$

$$v^* \frac{\partial w^*}{\partial y} + u^* \frac{\partial w^*}{\partial x} - 2\Omega u^* = \frac{\mu_{hnf}}{\rho_{hnf}} \left(\frac{\partial^2 u^*}{\partial x^2} + \frac{\partial^2 u^*}{\partial y^2} \right) - \frac{\bar{\sigma}_f B_o^2}{\rho_{hnf}} w^*, \quad (4.4)$$

$$\begin{aligned} v^* \frac{\partial T^*}{\partial y} + u^* \frac{\partial T^*}{\partial x} \\ = \frac{k_{hnf}}{(\rho C_p)_{hnf}} \left(\frac{\partial^2 T^*}{\partial x^2} + \frac{\partial^2 T^*}{\partial y^2} \right) - \frac{1}{(\rho C_p)_{hnf}} \frac{\partial q_{rad}^*}{\partial y} + \frac{\bar{\sigma}_f B_o^2}{(\rho C_p)_{hnf}} (u^{*2} + w^{*2}) \\ + \frac{Q(T^* - T_o)}{(\rho C_p)_{hnf}}, \end{aligned} \quad (4.5)$$

In equations Ω is angular velocity, u^* , v^* and w^* are velocities in x , y and z directions, B_o is magnetic field, P is pressure, T^* is temperature, $\bar{\sigma}_f$ is electrical conductivity and q_{rad}^* demonstrate radiative heat flux.

For radiation

$$q_{rad}^* = - \left(\frac{4\sigma^*}{3k_{hnf}^*} \right) \frac{\partial T^{*4}}{\partial y}, \quad (4.6)$$

We can expand T^{*4} in a Taylor series and by this expansion we get

$$T^{*4} \cong -3T_{\infty}^{*4} + 4T_{\infty}^{*3} T^*. \quad (4.7)$$

So the equation (4.5) become

$$\begin{aligned}
& v^* \frac{\partial T^*}{\partial y} + u^* \frac{\partial T^*}{\partial x} + w^* \frac{\partial T^*}{\partial z} \\
&= \frac{k_{hnf}}{(\rho C_p)_{hnf}} \left(\frac{\partial^2 T^*}{\partial x^2} + \frac{\partial^2 T^*}{\partial y^2} + \frac{\partial^2 T^*}{\partial z^2} \right) + \frac{16\sigma^* T_\infty^{*3}}{3k_{nf}^* (\rho C_p)_{nf}} \frac{\partial^2 T^*}{\partial y^2} + \frac{\bar{\sigma}_f B_o^2}{(\rho C_p)_{hnf}} (u^{*2} + w^{*2}) \\
&+ \frac{Q(T^* - T_o^*)}{(\rho C_p)_{hnf}}.
\end{aligned} \tag{4.8}$$

Effective dynamic viscosity, heat capacity and thermal conductivity are define as:

$$\rho_{hnf} = (1 - \phi_{Cu} - \phi_{Go})\rho_f + \phi_{Cu}\rho_{Cu} + \phi_{Go}\rho_{Go}, \tag{4.9}$$

$$(\rho C_p)_{hnf} = (1 - \phi_{Cu} - \phi_{Go})(\rho C_p)_f + \phi_{Cu}(\rho C_p)_{Cu} + \phi_{Go}(\rho C_p)_{Go}, \tag{4.10}$$

$$\mu_{nf} = \mu_f (1 - \phi_{Cu} - \phi_{Go})^{-2.5}, \tag{4.11}$$

$$\begin{aligned}
\frac{k_{hnf}}{k_f} = & \left\{ \frac{k_{Cu}\phi_{Cu} + k_{Go}\phi_{Go}}{\phi_{Cu} + \phi_{Go}} + 2k_f + 2(k_{Cu}\phi_{Cu} + k_{Go}\phi_{Go}) \right. \\
& - 2(\phi_{Cu} + \phi_{Go})k_f \left. \right\} \left\{ \frac{k_{Cu}\phi_{Cu} + k_{Go}\phi_{Go}}{\phi_{Cu} + \phi_{Go}} + 2k_f - (k_{Cu}\phi_{Cu} + k_{Go}\phi_{Go}) \right. \\
& \left. + (\phi_{Cu} + \phi_{Go})k_f \right\}^{-1},
\end{aligned} \tag{4.12}$$

$$(\rho\beta)_{hnf} = (1 - \phi_{Cu} - \phi_{Go})(\rho\beta)_f + \phi_{Cu}(\rho\beta)_{Cu} + \phi_{Go}(\rho\beta)_{Go}. \tag{4.13}$$

Table1. Thermo physical properties of hybrid nanofluid and water.

	(kg/m ³)	C _p (J/kg K)	k(W/m k)
Graphene Oxide (Go)	1800	717	5000
Copper (Cu)	8933	385	401
Pure water	997.1	4179	0.613

Boundary conditions at lower and upper surfaces are:

$$u^* = u_w^* = ax, \quad v^* = 0, \quad w^* = 0, \quad T^* = T_H^* \quad \text{at } y = 0 \tag{4.14}$$

$$u^* = 0, \quad v^* = v_o, \quad w^* = 0, \quad T^* = T_o^* \quad \text{at } y = h \tag{4.15}$$

Using similarity variables:

$$\eta = \frac{y}{h}, \quad v^* = -ahf(\eta), \quad u^* = axf'(\eta) \quad w^* = axg(\eta) \quad \theta = \frac{T^* - T_H^*}{T_o^* - T_H^*}. \quad (4.16)$$

By using similarity variables the given PDE's transformed in to dimensionless ODE's.

$$f^{iv} + \mathbb{B}_1(1 - \phi_{Cu} - \phi_{Go})^{2.5} Re(ff'''' - f'f''') - 2\mathbb{B}_1 R_o((1 - \phi_{Cu} - \phi_{Go})^{2.5} g' - Mn((1 - \phi_{Cu} - \phi_{Go})^{2.5} f'' + GrRe\mathbb{B}'_1(1 - \phi_{Cu} - \phi_{Go})^{2.5} \theta' = 0, \quad (4.17)$$

$$g'' + \mathbb{B}_1(1 - \phi_{Cu} - \phi_{Go})^{2.5} Re(fg' - f'g) + 2\mathbb{B}_1 R_o((1 - \phi_{Cu} - \phi_{Go})^{2.5} f' - Mn((1 - \phi_{Cu} - \phi_{Go})^{2.5} g = 0, \quad (4.18)$$

$$\theta'' + \mathbb{B}_2 PrRe \left(\frac{3}{3 + 4N} \right) \frac{k_f}{k_{hnf}} f\theta' + MnPrEc \left(\frac{3}{3 + 4N} \right) \frac{k_f}{k_{hnf}} (f'^2 + g^2) + Q_o PrRe \left(\frac{3}{3 + 4N} \right) \frac{k_f}{k_{hnf}} \theta = 0. \quad (4.19)$$

\mathbb{B}_1 , \mathbb{B}_1^* and \mathbb{B}_2 are constant and given as:

$$\mathbb{B}_1 = (1 - \phi_{Cu} - \phi_{Go}) + \frac{\phi_{Cu}\rho_{Cu} + \phi_{Go}\rho_{Go}}{\rho_f}$$

$$\mathbb{B}_1^* = (1 - \phi_{Cu} - \phi_{Go})(\rho\beta)_f + \frac{\phi_{Cu}(\rho\beta)_{Cu} + \phi_{Go}(\rho\beta)_{Go}}{(\rho\beta)_f}$$

$$\mathbb{B}_2 = (1 - \phi_{Cu} - \phi_{Go}) + \frac{\phi_{Cu}(\rho C_p)_{Cu} + \phi_{Go}(\rho C_p)_{Go}}{(\rho C_p)_f}$$

Dimensionless parameter are:

$$N = \frac{4\sigma^* T_\infty^3}{k_{nf} k_{hnf}^*}, \quad Pr = \frac{\mu_f(\rho C_p)_f}{\rho_f k_f}, \quad Mn = \frac{\bar{\sigma}_f B_o^2 h^2}{\rho_f \vartheta_f}, \quad (4.20)$$

$$Re = \frac{ah^2}{\nu}, \quad R_o = \frac{\Omega h^2}{\vartheta_f}, \quad Ec = \frac{\rho_f ah^2}{(\rho C_p)_f (T_o^* - T_H^*)}. \quad (4.21)$$

Relevant surface constrain for model are

$$f = 0, \quad f' = 1, \quad g = 0, \quad \theta = 1 \quad \text{at } \eta = 0, \quad (4.22)$$

$$f = A, \quad f' = 0, \quad g = 0, \quad \theta = 0 \quad \text{at } \eta = 1. \quad (4.23)$$

Skin friction coefficient is defined as

$$C_f = \frac{\mu_{hnf}}{\rho_f v_o^2} \left. \frac{\partial u}{\partial y} \right|_{y=0}, \quad (4.24)$$

And also Nusselt number is

$$Nu = \left[\frac{h}{k_f(T_o - T_H)} \right] \left(k_{hnf} + \frac{16\sigma^* T_\infty^3}{3k_{hnf}^*} \right) \left. \frac{\partial T^*}{\partial y} \right|_{y=0}. \quad (4.25)$$

We gain:

$$C_f^* = |(1 - \phi_{Cu} - \phi_{Go})^{-2.5} f''(0)|, \quad (4.26)$$

$$Nu^* = \left| \frac{k_{hnf}}{k_f} \left(1 + \frac{4}{3} N \right) \theta'(0) \right|. \quad (4.27)$$

(4.2) Methodology

In this section, same method (ADM) is adopted as we have discussed in chapter 3. In order to avoid the repetition of method, we just mentioned the initial guess of modified model for velocities and temperature and then define the operators that is used to solve the given system of equations (4.17)-(4.19) with boundary conditions (4.22) and (4.23).

Simplifying the fourth order ODE's by using the similar technique (ADM) we get.

Let

$$f^{iv} = -B_1(1 - \phi_{Cu} - \phi_{Go})^{2.5} Re(ff'''' - f'f'') - 2B_1Ro((1 - \phi_{Cu} - \phi_{Go})^{2.5}g' - Mn((1 - \phi_{Cu} - \phi_{Go})^{2.5}f'' + GrReB_1'(1 - \phi_{Cu} - \phi_{Go})^{2.5}\theta' = 0, \quad (4.28)$$

$$g'' = -B_1(1 - \phi_{Cu} - \phi_{Go})^{2.5} Re(fg' - f'g) - 2B_1Ro((1 - \phi_{Cu} - \phi_{Go})^{2.5}f' + Mn((1 - \phi_{Cu} - \phi_{Go})^{2.5}g), \quad (4.29)$$

$$\theta'' = -B_2PrRe \left(\frac{3}{3 + 4N} \right) \frac{k_f}{k_{hnf}} f\theta' - MnPrEc \left(\frac{3}{3 + 4N} \right) \frac{k_f}{k_{hnf}} (f'^2 + g^2) - Q_oPrRe \left(\frac{3}{3 + 4N} \right) \frac{k_f}{k_{hnf}} \theta = 0. \quad (4.30)$$

Operators for f , g and θ ,

$$f^{iv} = L_4f = \frac{d^4}{d\eta^4} f, \quad g'' = L_2g = \frac{d^2}{d\eta^2} g, \quad \text{and} \quad \theta'' = L_2\theta = \frac{d^2}{d\eta^2} \theta.$$

And inverse operators are $L_4^{-1}(\cdot) = \int_0^\eta \int_0^\eta \int_0^\eta \int_0^\eta (\cdot) d\eta d\eta d\eta d\eta$ and $L_3^{-1}(\cdot) = \int_0^\eta \int_0^\eta \int_0^\eta (\cdot) d\eta d\eta d\eta$

Now the initial guess are

$$f_o(\eta) = -(1 - 2A)\eta^3 + \eta + (3A - 2)\eta^2,$$

$$\begin{aligned} f_{n+1}(\eta) &= [L_4^{-1}(N_1'u^*)] + (2\eta^3 - 3\eta^2)[L_4^{-1}(N_1'u^*)]_{\eta=1} \\ &+ (\eta^2 - \eta^3)[L_3^{-1}(N_1'u^*)]_{\eta=1}, \end{aligned} \quad (4.31)$$

$$g_o(\eta) = 0,$$

$$g_{n+1}(\eta) = [L_2^{-1}(N_2'u^*)] - \eta[L_2^{-1}(N_2'u^*)]_{\eta=1}, \quad (4.32)$$

$$\theta_o(\eta) = 1 - \eta,$$

$$\theta_{n+1}(\eta)[L_2^{-1}(N_3'u^*)] - \eta[L_2^{-1}(N_3'u^*)]_{\eta=1}. \quad (4.33)$$

where

$$\begin{aligned} N_1'u^* &= -B_1(1 - \phi_{Cu} - \phi_{Go})^{2.5}Re(ff''' - f'f'') + 2B_1Ro((1 - \phi_{Cu} - \phi_{Go})^{2.5}g' \\ &+ Mn((1 - \phi_{Cu} - \phi_{Go})^{2.5}f'' + GrReB_1'(1 - \phi_{Cu} - \phi_{Go})^{2.5}\theta'), \end{aligned} \quad (4.34)$$

$$\begin{aligned} N_2'u^* &= -B_1(1 - \phi_{Cu} - \phi_{Go})^{2.5}Re(fg' - f'g) - 2B_1Ro((1 - \phi_{Cu} - \phi_{Go})^{2.5}f' \\ &+ Mn((1 - \phi_{Cu} - \phi_{Go})^{2.5}g), \end{aligned} \quad (4.35)$$

$$\begin{aligned} N_3'u^* &= -B_2PrRe\left(\frac{3}{3 + 4N}\right)\frac{k_f}{k_{hnf}}f\theta' - MnPrEc\left(\frac{3}{3 + 4N}\right)\frac{k_f}{k_{hnf}}(f'^2 + g^2) \\ &+ Q_oPrRe\left(\frac{3}{3 + 4N}\right)\frac{k_f}{k_{hnf}}\theta. \end{aligned} \quad (4.36)$$

Using Maple to solve the problem

4.3 Results and discussion

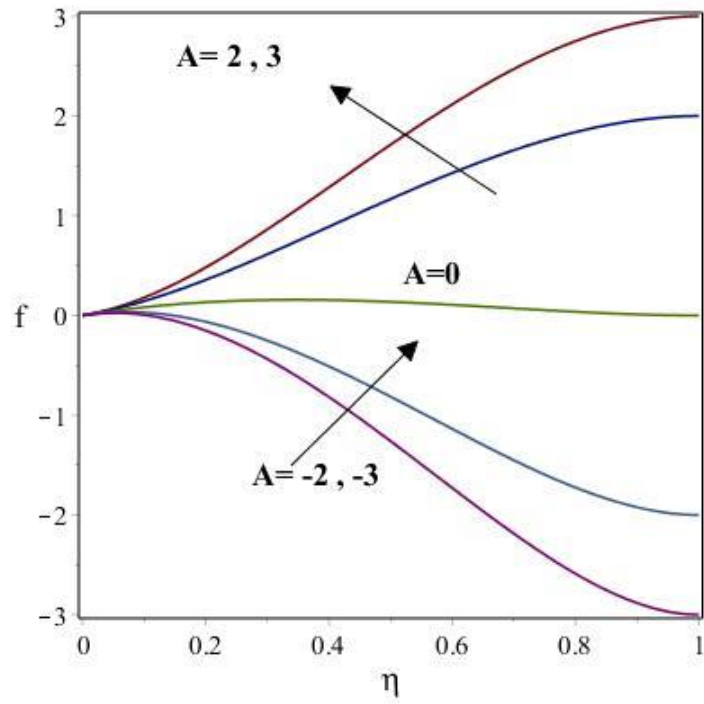
Former, the nonlinear PDE's are reconstructed in to ODE's and analytical technique is use for the solution of problem. Impact of magnetic parameter, suction/injection parameter, Reynolds number, and Rotation parameter on velocity profile, temperature profile and Nusselt number examined. The effect of A and Re on velocity profile f and g are shown in Figure. (4.2) and (4.3). It is mention earlier that $A > 0$ shows the injection flow and $A < 0$ shows the suction flow. If values of injection parameter goes up then velocity profile also rises in x and y -direction. While for suction parameter, increase in value of suction parameter causes decrease in velocity profile. For injection

process g decreases and f increases when Re number increases. Moreover, for small value of Re , the g decreases while at larger value of Re , higher velocity point moves.

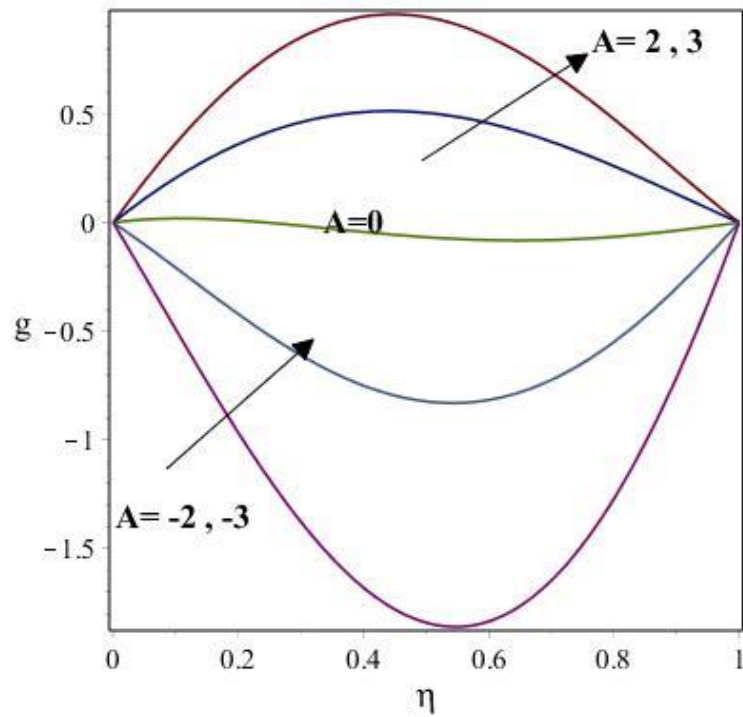
Figure. (4.4) and (4.5) indicate the impact of Re and injection parameter on temperature profile and Nusselt number. For injection process temperature profile decreases and Nusselt number increases while for suction process Nusselt number goes down. With ascending Re , θ will diminish. The results also indicate that shear stress increases and Nusselt number goes up with an increase in Reynolds number. Although, this is valid for any value of injection parameter and for small value of suction parameter. Also Nusselt number become decreasing function of Re for larger value of suction parameter.

In Figure. (4.6) and (4.7) the impact of Mn and R_o on velocity profile are discussed. Experienced that, by increasing Mn , the Lorentz force also rises and resist more effectively to the flow. In this manner, one can see that velocity profile will be degraded by increasing Mn . This is introduced in Figure. (4.6). It tends to be additionally concluded that climbing upside of rotation parameter causes increase in g and decrease in f . In any case, this is valid for variety of f for rotation parameter at $\eta > 0.3$. But for $\eta < 0.3$ the value of f become increases. Figure. (4.8) and (4.9) depict that, the rising qualities of magnetic and rotation parameter cause the thermal boundary layer to be condense, bringing about the temperature profile's increases with an expanding in the magnetic and rotation parameter. In addition, in light of the fact that the Nusselt number and the thermal boundary layer thickness have a rearranged relationship, the Nusselt number increases with increasing Mn and R_o . Figure. (4.10) and (4.11). Demonstrate the effect of N and solid volume fraction on temperature profile and Nusselt number. An increment in value of N and solid volume fraction cause increase in temperature profile. Nusselt number will also increase with increasing the value of N and solid volume fraction.

The influence of Grashaf number on velocity profile and temperature are shown in Figure.(4.12) and (4.13). It is clear from graphical representation that when Grashaf number rises the velocity in x -direction also rises. While velocity profile in z -direction decreases with increasing the value of Grashaf number. The relation of Grashaf number with temperature profile are shown in figure, (4.13). It demonstrate that temperature profile will also increase with increasing Grashaf number.

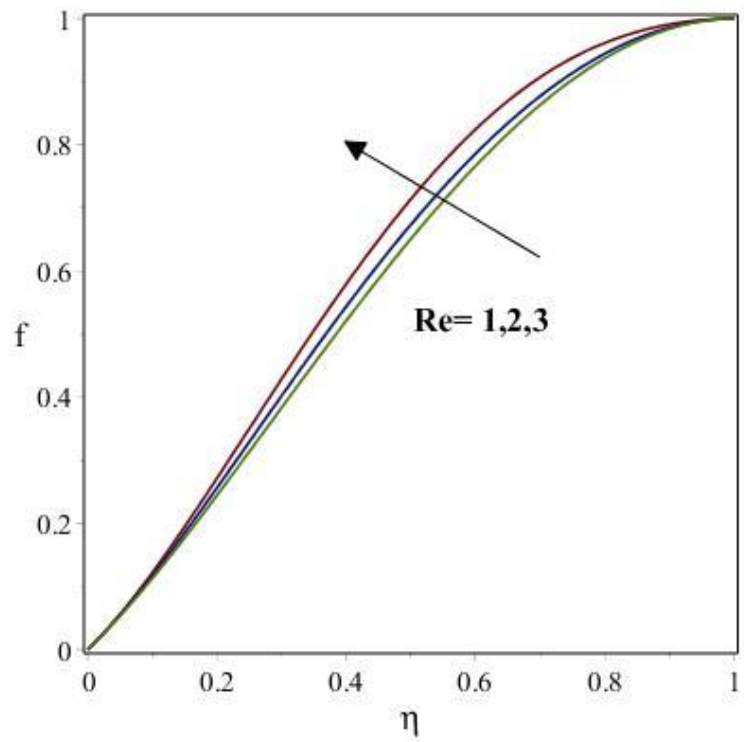


(a)

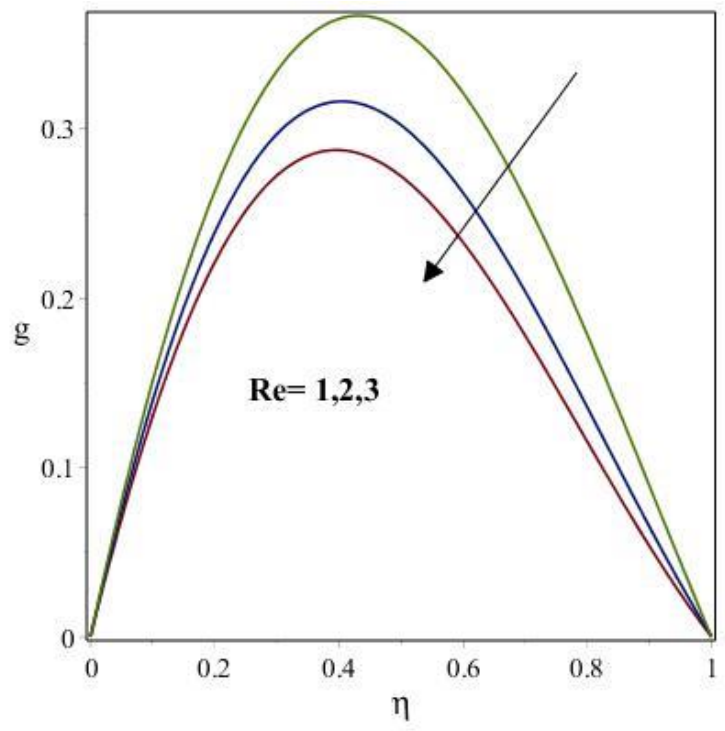


(b)

Figure.(4.2). variation of suction/injection parameter with velocity profile (a) $f(\eta)$ and (b) $g(\eta)$.

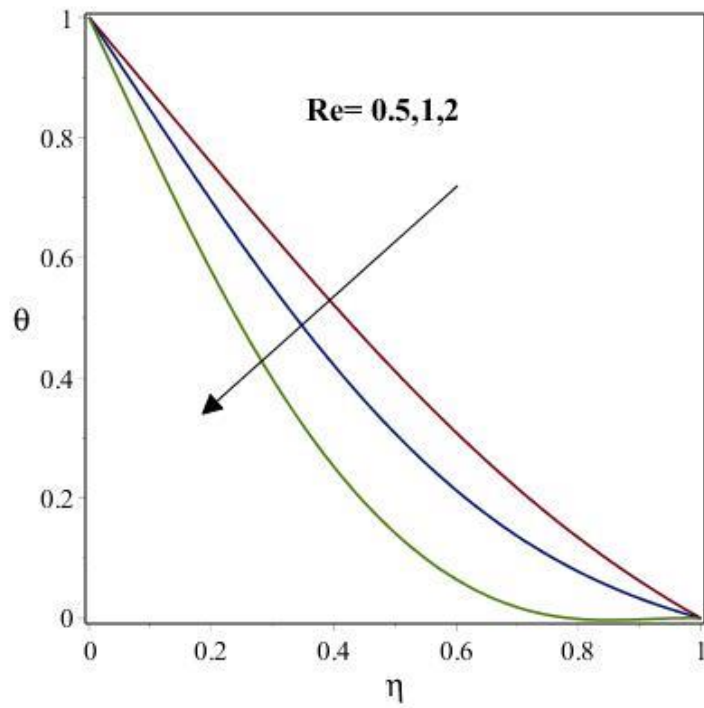


(a)

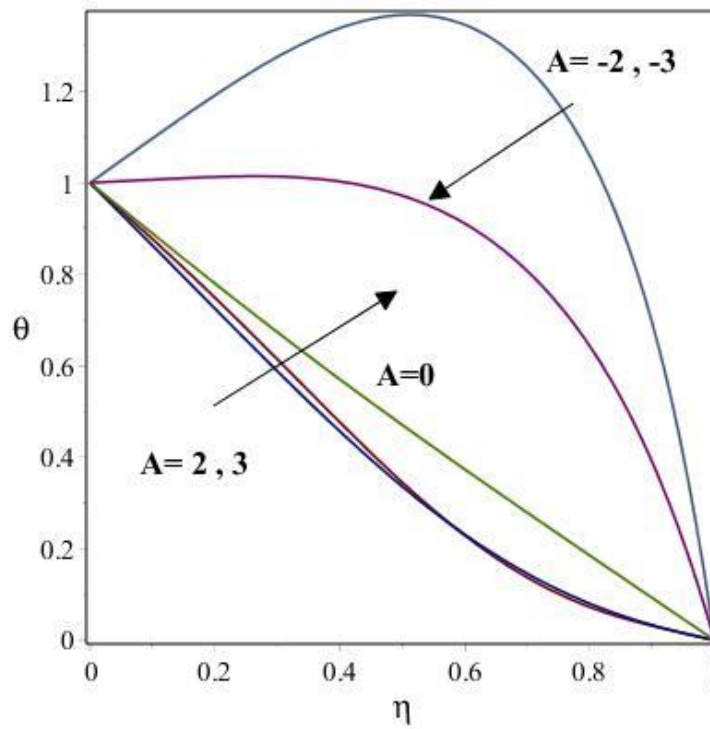


(b)

Figure.(4.3).Variation of Reynolds number with velocity profile (a) $f(\eta)$ and (b) $g(\eta)$.

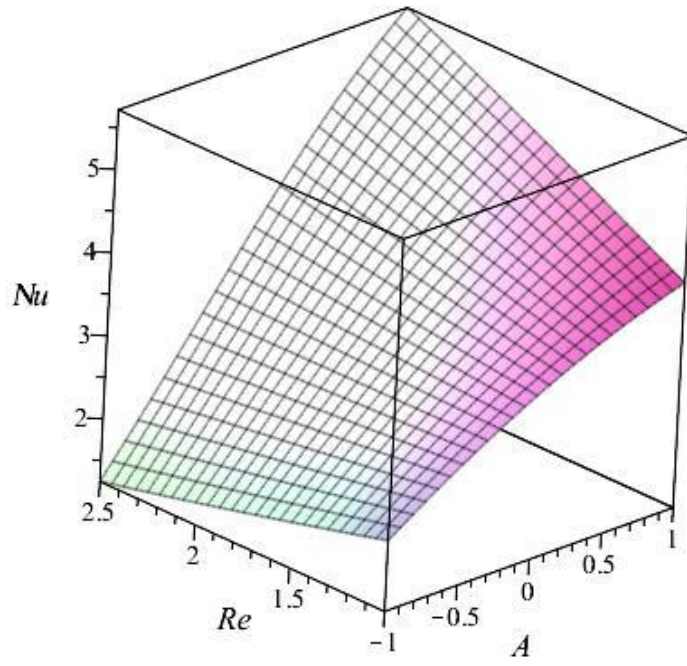


(a)

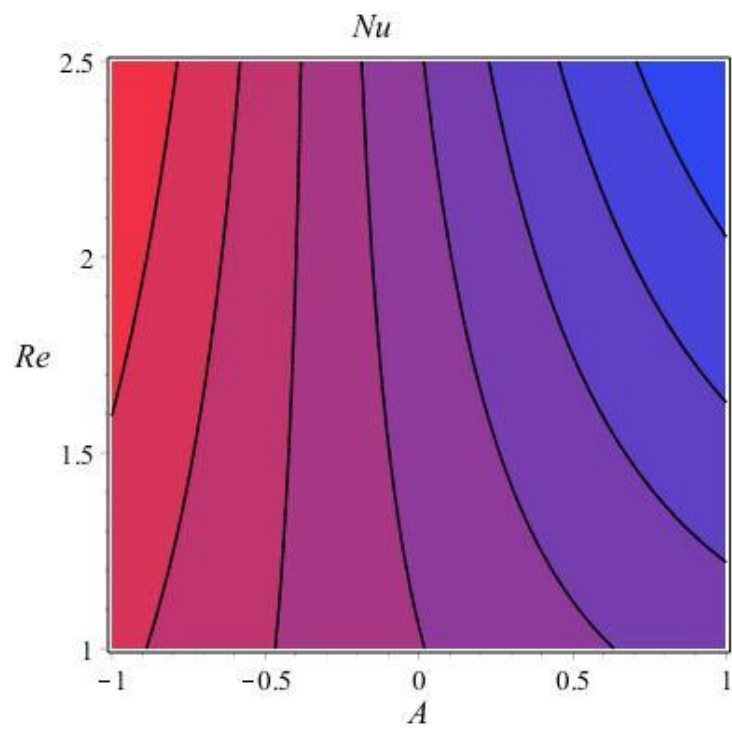


(b)

Figure. (4.4) Influence of (a) A and (b) Re on the temperature profile..

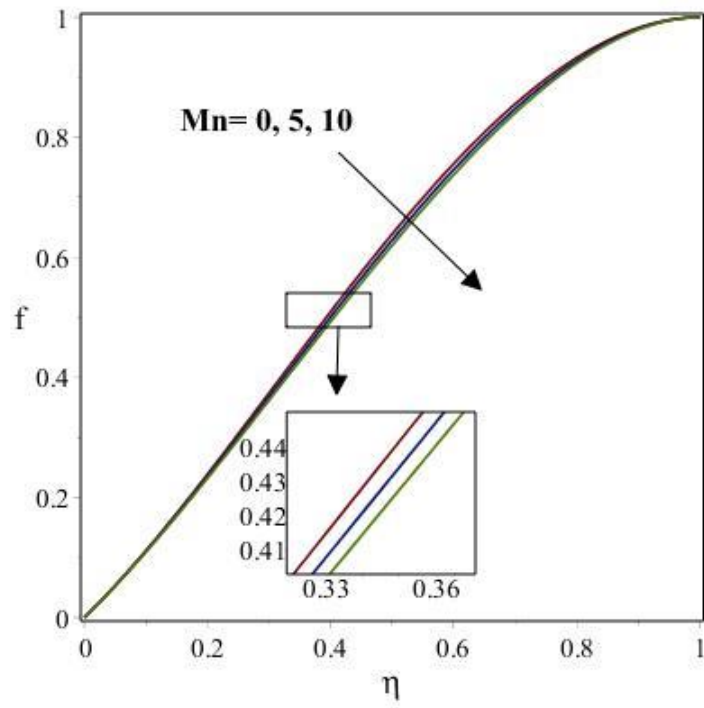


(a)

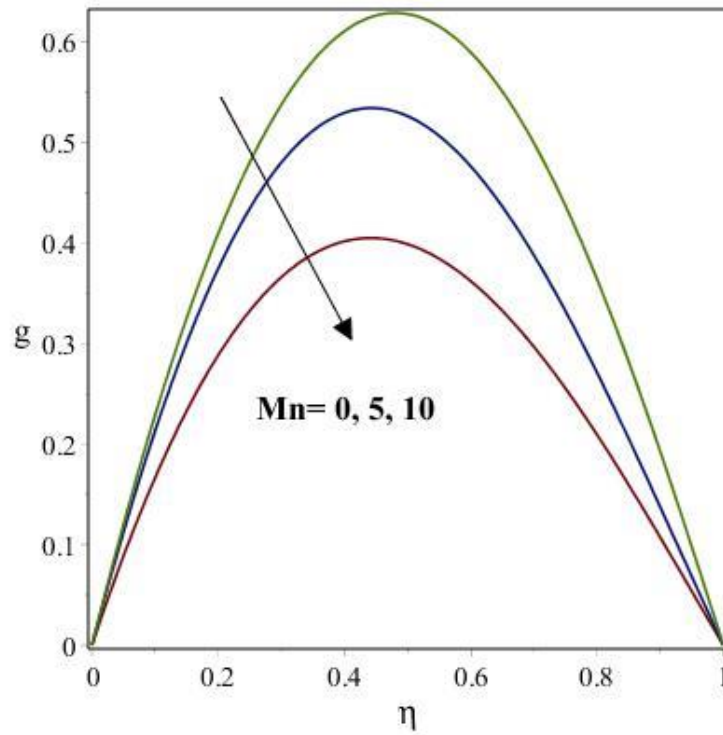


(b)

Figure. (4.5). Variation of (a) A and (b) Reynolds number with Nusselt number.

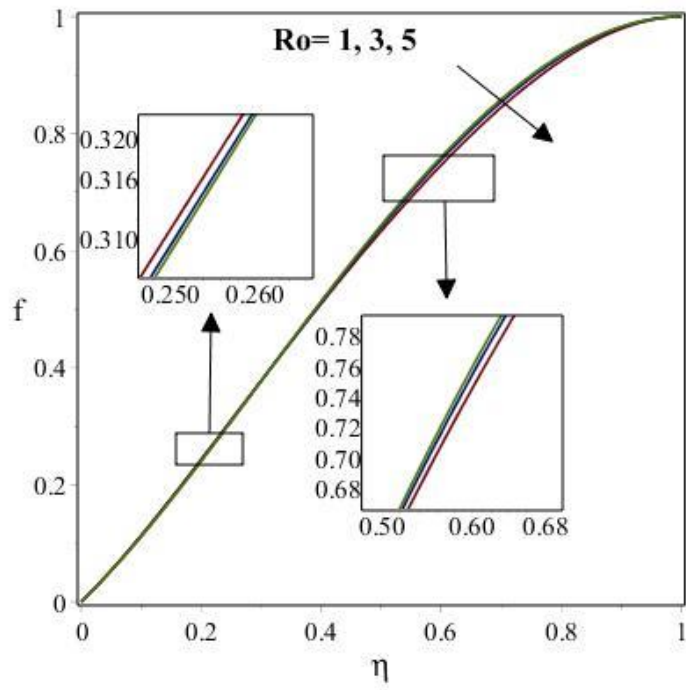


(a)

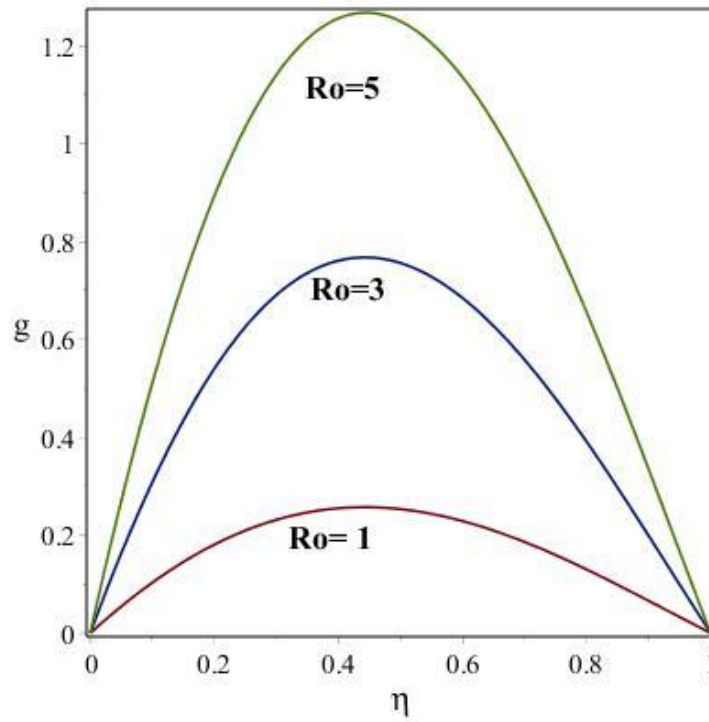


(b)

Figure.(4.6). Variation of magnetic parameter with velocity profile (a) $f(\eta)$ and (b) $g(\eta)$.

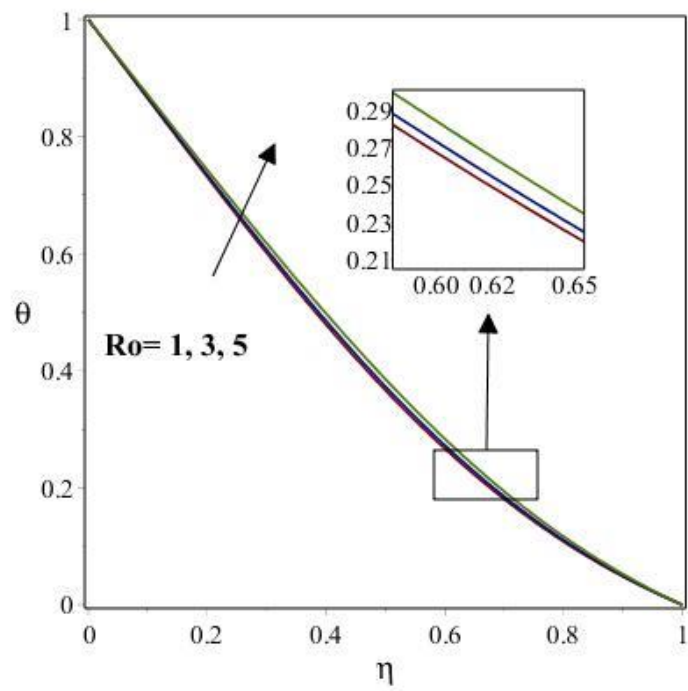


(a)

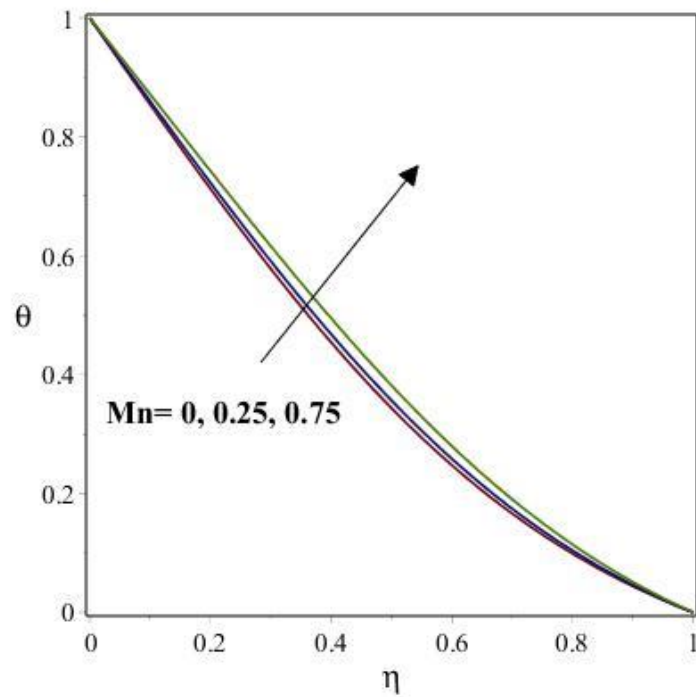


(b)

Figure.(4.7). Variation of Ro with velocity profile (a) $f(\eta)$ and (b) $g(\eta)$.

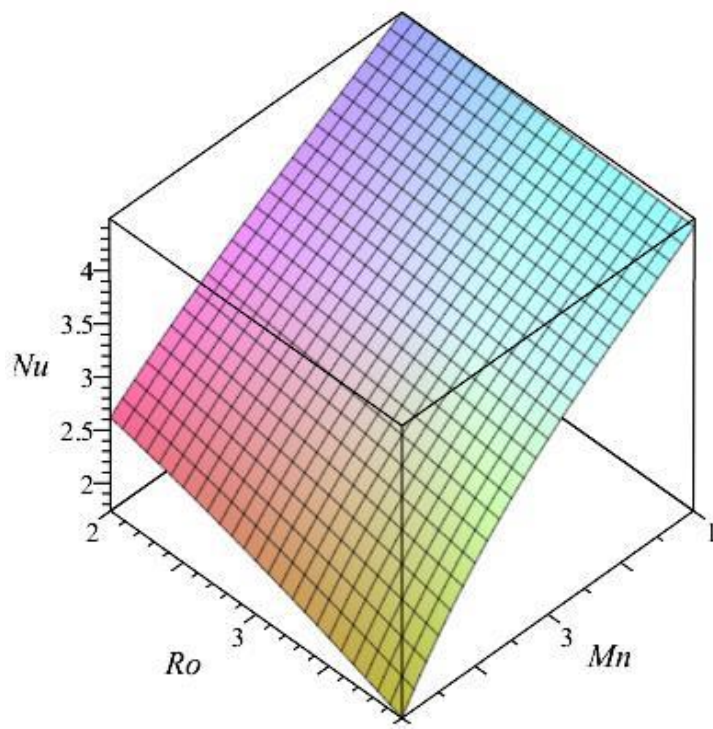


(a)

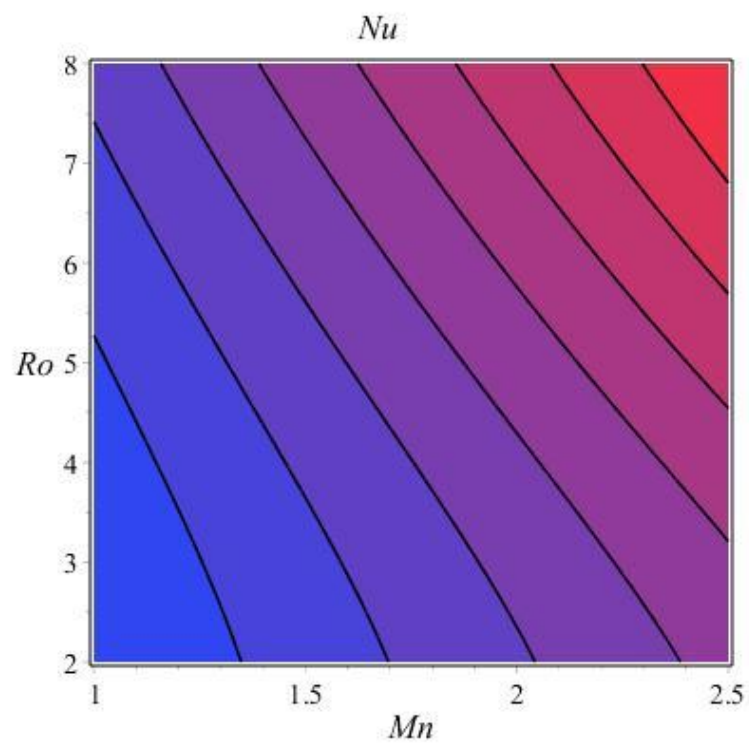


(b)

Figure. (4.8). Influence of (a) rotation and (b) magnetic parameters on the temperature profile.

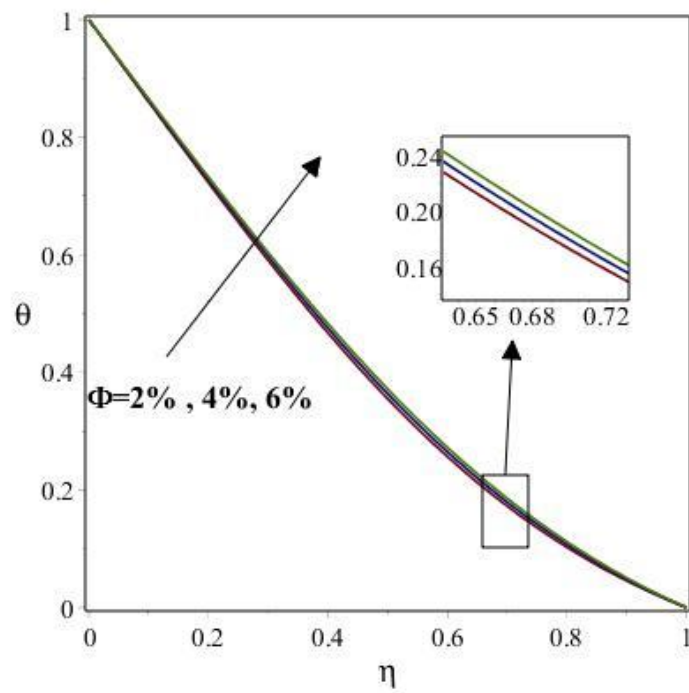


(a)

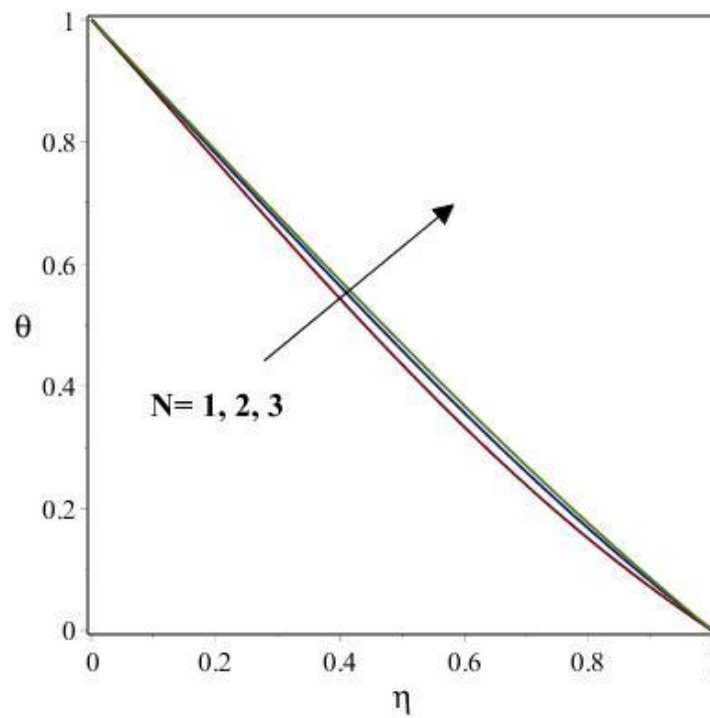


(b)

Figure. (4.9). Influence of (a) magnetic and (b) rotation parameters on the Nusselt number.

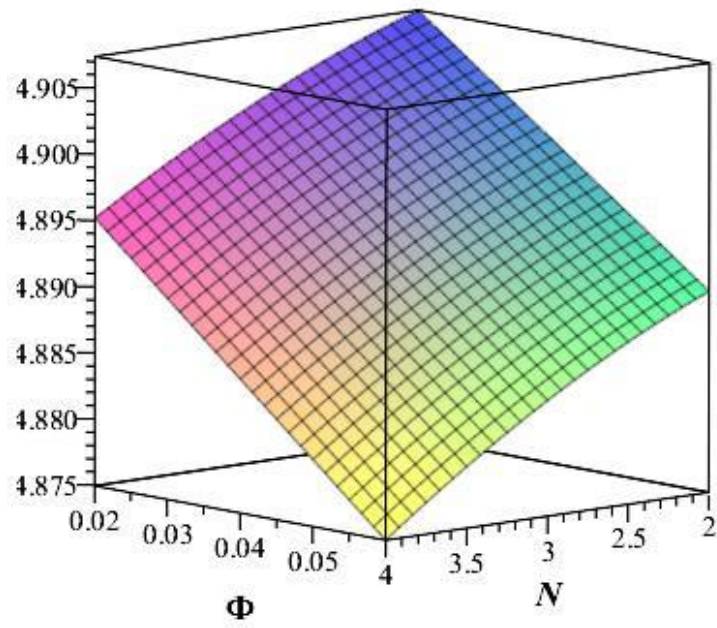


(a)

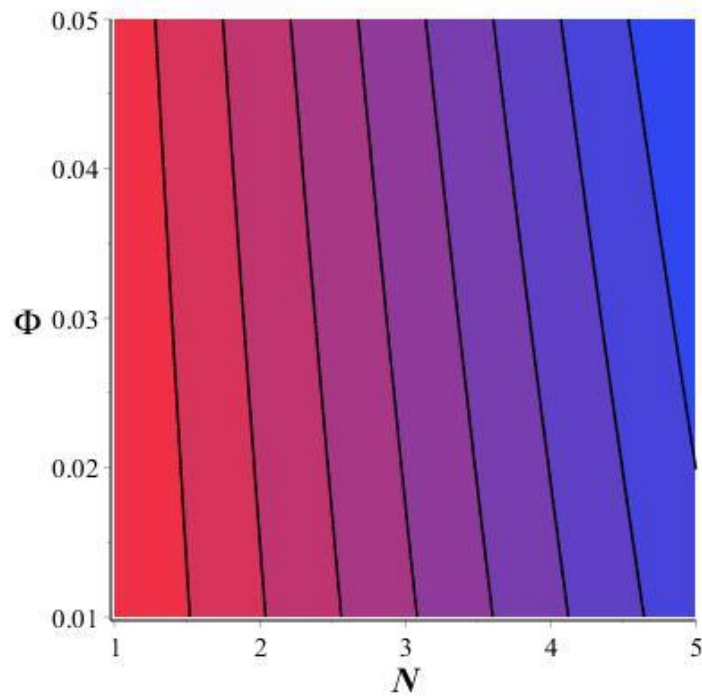


(b)

Figure. (4.10). Effect of (a) N and (b) ϕ on the temperature profile.



(a)



(b)

Figure. (4.11). Variation of (a) radiation parameter and (b) volume fraction with Nusselt number.

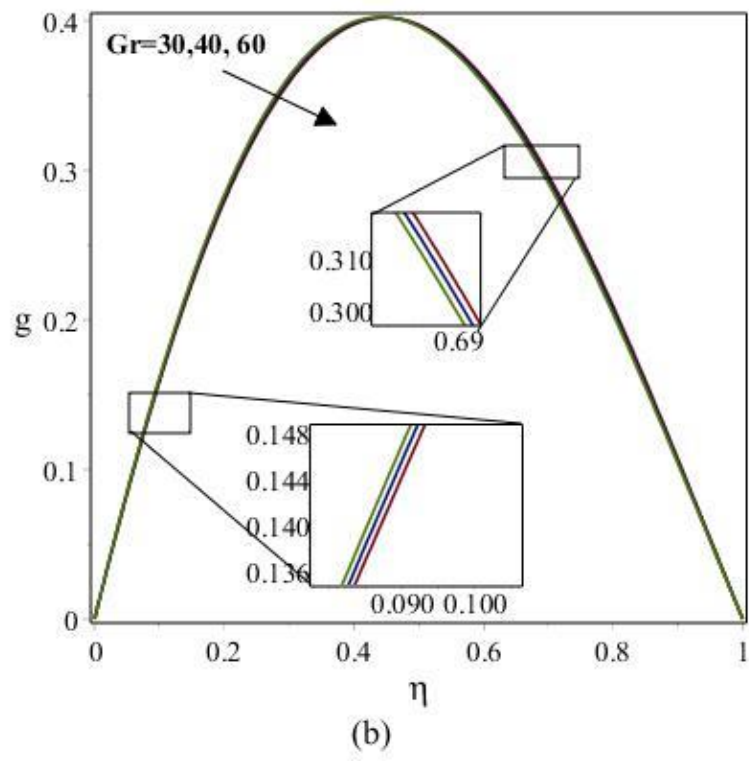
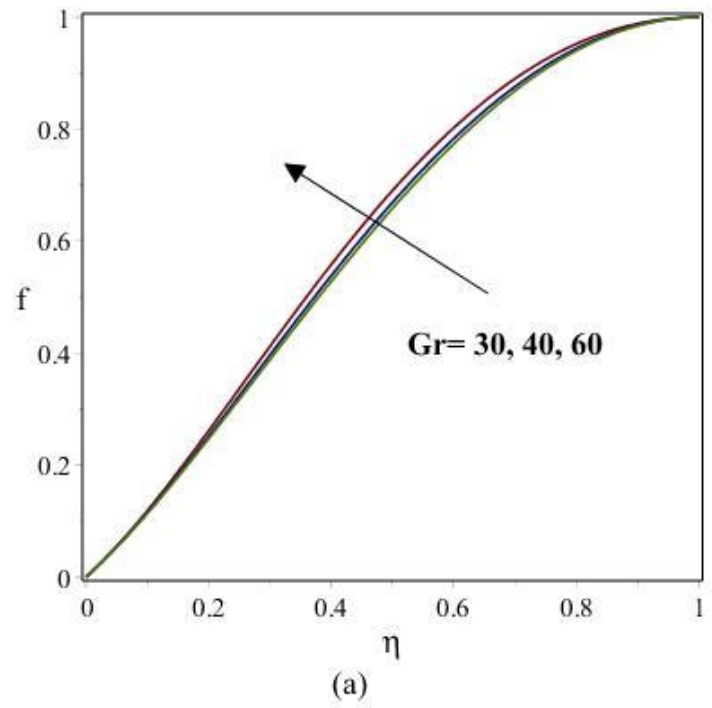


Figure. (4.12). variation of Grashaf number with velocity profile (a) $f(\eta)$ and (b) $g(\eta)$.

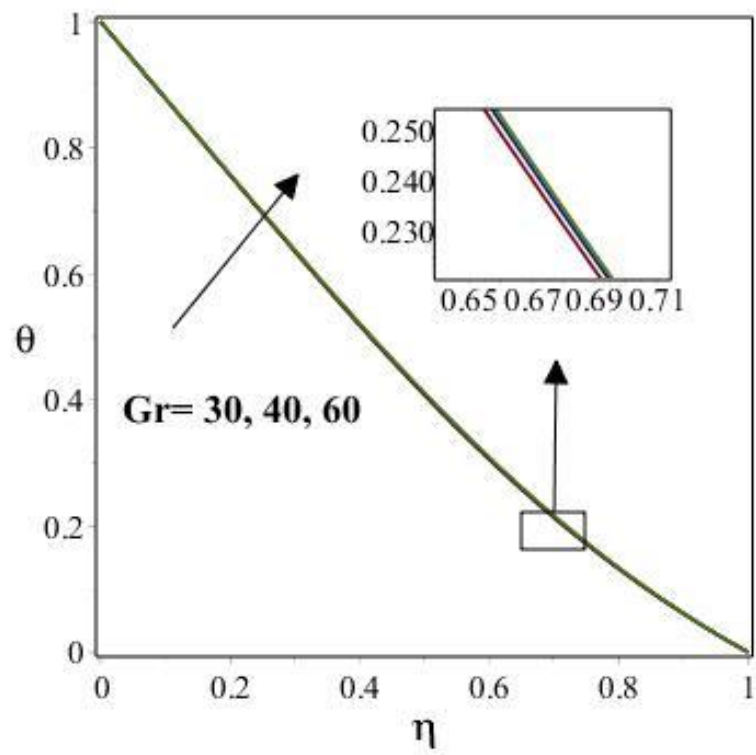


Figure.(4.13). variation of Grashaf number with temperature profile.

Chapter 5

Conclusion

Hybrid nanofluid flow in a vertical channel and heat transfer on a stretchable surface between two plates are examined. The nonlinear PDE's are converted in to ODE's and then solve by using (DRA) Approach. Physical parameter are graphically determined. The obtaining results of this study are

- $A > 0$ shows injection and $A < 0$ shows suction with wall.
- Both velocities $f(\eta)$ and $g(\eta)$ in x and z -direction increases with increasing injection parameter but suction parameter shows converse behavior.
- Temperature shows decreasing behavior with injection parameter.
- Velocity $f(\eta)$ in x -direction increases with increasing Reynolds number.
- Velocity $g(\eta)$ in z -direction decreases with increasing Reynolds number.
- Nusselt number goes up with raising injection parameter and Reynolds number and also increase for low value of suction parameter.
- Both velocities $f(\eta)$ and $g(\eta)$ in x and z -direction decreasing with increasing magnetic parameter.
- Magnetic and rotation parameter have direct relation with temperature profile.
- Velocity profile $f(\eta)$ clearly goes up and $g(\eta)$ diminish with ascending Rotation parameter.
- Nusselt number diminish with increasing Mn and Ro .
- With Grashaf number velocity increases in x -direction and decreases in z -direction.
- Temperature profile also increases with Grashaf number.

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